

FEM for Vibration Problem

- Governing equation and weak form
- Space discretization
- Mass matrix and damping matrix
- Direct integration

Governing Equation & Weak Form (1)

$$\begin{cases} \frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + b_x = 0 \\ \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + b_y = 0 \end{cases} \oplus (\text{inertia force}) \begin{cases} B_x = -\rho \frac{\partial^2 u}{\partial t^2} \\ B_y = -\rho \frac{\partial^2 v}{\partial t^2} \end{cases}$$

$$(\text{equations of motion}) \begin{cases} \frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + b_x + B_x = 0 \\ \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + b_y + B_y = 0 \end{cases}$$

$$\begin{aligned} & \int_{\Omega} \left\{ u^* \left(\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + b_x + B_x \right) + v^* \left(\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + b_y + B_y \right) \right\} h dA = 0 \\ & - \int_{\Omega} (u^* B_x + v^* B_y) h dA + \int_{\Omega} \left\{ \frac{\partial u^*}{\partial x} \sigma_x + \frac{\partial v^*}{\partial y} \sigma_y + \left(\frac{\partial u^*}{\partial y} + \frac{\partial v^*}{\partial x} \right) \tau_{xy} \right\} h dA \\ & = \int_{\Omega} (u^* b_x + v^* b_y) h dA + \int_{\Omega} \left\{ \frac{\partial}{\partial x} (u^* \sigma_x) + \frac{\partial}{\partial y} (u^* \tau_{xy}) + \frac{\partial}{\partial y} (v^* \sigma_y) + \frac{\partial}{\partial x} (v^* \tau_{xy}) \right\} h dA \end{aligned}$$

Governing Equation & Weak Form (2)

$$\begin{aligned}
 & \left[\varepsilon_x^* = \frac{\partial u^*}{\partial x}, \varepsilon_y^* = \frac{\partial v^*}{\partial y}, \tau_{xy}^* = \frac{\partial u^*}{\partial y} + \frac{\partial v^*}{\partial x} \right] \\
 & - \int_{\Omega} (u^* B_x + v^* B_y) h dA + \int_{\Omega} (\varepsilon_x^* \sigma_x + \varepsilon_y^* \sigma_y + \tau_{xy}^* \tau_{xy}) h dA \\
 & = \int_{\Omega} (u^* b_x + v^* b_y) h dA + \int_{\Gamma} \left\{ u^* (\sigma_x n_x + \tau_{xy} n_y) + v^* (\sigma_y n_y + \tau_{xy} n_x) \right\} h ds \\
 & \left[\begin{array}{l} t_x = \bar{t}_x \\ t_y = \bar{t}_y \end{array} \right\} \text{ on } \Gamma_{\sigma} \\
 & \left[u^* = v^* = 0 \text{ on } \Gamma_u \right] \\
 & - \int_{\Omega} (u^* B_x + v^* B_y) h dA + \int_{\Omega} (\varepsilon_x^* \sigma_x + \varepsilon_y^* \sigma_y + \tau_{xy}^* \tau_{xy}) h dA \\
 & = \int_{\Omega} (u^* b_x + v^* b_y) h dA + \int_{\Gamma_{\sigma}} (u^* \bar{t}_x + v^* \bar{t}_y) h ds
 \end{aligned}$$

Discretization: Space

$$-\int_{\Omega_e} (u^* B_x + v^* B_y) h_e dA = \int_{\Omega_e} \rho_e \left(u^* \frac{\partial^2 u}{\partial t^2} + v^* \frac{\partial^2 v}{\partial t^2} \right) h_e dA$$

$$\begin{cases} u \approx N_1^e u_1^e + N_2^e u_2^e + N_3^e u_3^e = \mathbf{N}_e \mathbf{u}_e \\ v \approx N_1^e v_1^e + N_2^e v_2^e + N_3^e v_3^e = \mathbf{N}_e \mathbf{v}_e \end{cases}$$

$$\begin{cases} u^* \approx N_1^e u_1^{*e} + N_2^e u_2^{*e} + N_3^e u_3^{*e} = \mathbf{N}_e \mathbf{u}_e^* \\ v^* \approx N_1^e v_1^{*e} + N_2^e v_2^{*e} + N_3^e v_3^{*e} = \mathbf{N}_e \mathbf{v}_e^* \end{cases}$$

$$\int_{\Omega_e} \rho_e \left(u^* \frac{\partial^2 u}{\partial t^2} + v^* \frac{\partial^2 v}{\partial t^2} \right) h_e dA \approx \mathbf{u}_e^{*T} \left[\int_{\Omega_e} \rho_e (\mathbf{N}_e^T \mathbf{N}_e) h_e dA \right] \ddot{\mathbf{u}}_e + \mathbf{v}_e^{*T} \left[\int_{\Omega_e} \rho_e (\mathbf{N}_e^T \mathbf{N}_e) h_e dA \right] \ddot{\mathbf{v}}_e$$

$$\mathbf{u} = \begin{Bmatrix} u \\ v \end{Bmatrix} \approx \begin{bmatrix} N_1^e & 0 & N_2^e & 0 & N_3^e & 0 \\ 0 & N_1^e & 0 & N_2^e & 0 & N_3^e \end{bmatrix} \begin{Bmatrix} u_1^e \\ v_1^e \\ u_2^e \\ v_2^e \\ u_3^e \\ v_3^e \end{Bmatrix} = \mathbf{N}_e \mathbf{d}_e \quad \text{where} \quad \begin{cases} \mathbf{N}_e : \text{shape function matrix} \\ \mathbf{d}_e : \text{element nodal displacement vector} \end{cases}$$

$$\int_{\Omega_e} \rho_e \left(u^* \frac{\partial^2 u}{\partial t^2} + v^* \frac{\partial^2 v}{\partial t^2} \right) h_e dA \approx \mathbf{d}_e^{*T} \mathbf{M}_e \ddot{\mathbf{d}}_e \quad \text{where} \quad \mathbf{M}_e = \int_{\Omega_e} \rho_e (\mathbf{N}_e^T \mathbf{N}_e) h_e dA \quad (\text{mass matrix})$$

$$\mathbf{M}_e \ddot{\mathbf{d}}_e + \mathbf{K}_e \mathbf{d}_e = \mathbf{F}_e \Rightarrow \mathbf{M} \ddot{\mathbf{d}} + \mathbf{K} \mathbf{d} = \mathbf{F} \Rightarrow \mathbf{M} \ddot{\mathbf{d}} + \mathbf{C} \dot{\mathbf{d}} + \mathbf{K} \mathbf{d} = \mathbf{F}$$

Mass Matrix

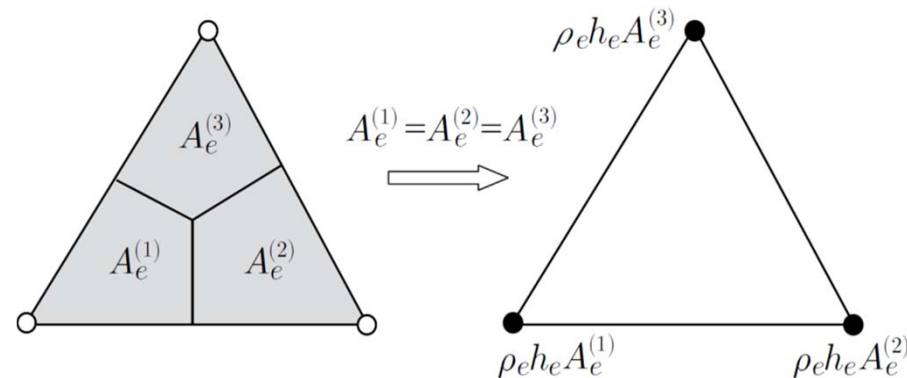
$$\mathbf{M}_e = \int_{\Omega_e} \rho_e \begin{Bmatrix} N_1^e \\ N_2^e \\ N_3^e \end{Bmatrix} \begin{Bmatrix} N_1^e & N_2^e & N_3^e \end{Bmatrix} h_e dA = \frac{\rho_e V_e}{12} \begin{bmatrix} 2 & 1 & 1 \\ 1 & 2 & 1 \\ 1 & 1 & 2 \end{bmatrix} \quad \text{where} \quad \begin{cases} V_e = A_e h_e \\ \rho_e V_e \text{ (element mass)} \end{cases}$$

$$2D: \mathbf{d}_e = \{u_1^e \quad u_2^e \quad u_3^e \quad u_4^e \quad u_5^e \quad u_6^e\}^T$$

consistent mass matrix: (1st order element) lumped mass matrix: (0th order element)

$$\mathbf{M}_e = \frac{\rho_e V_e}{12} \begin{bmatrix} 2 & 0 & 1 & 0 & 1 & 0 \\ 0 & 2 & 0 & 1 & 0 & 1 \\ 1 & 0 & 2 & 0 & 1 & 0 \\ 0 & 1 & 0 & 2 & 0 & 1 \\ 1 & 0 & 1 & 0 & 2 & 0 \\ 0 & 1 & 0 & 1 & 0 & 2 \end{bmatrix}$$

$$\mathbf{M}_e = \frac{\rho_e V_e}{3} \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$



Damping Matrix

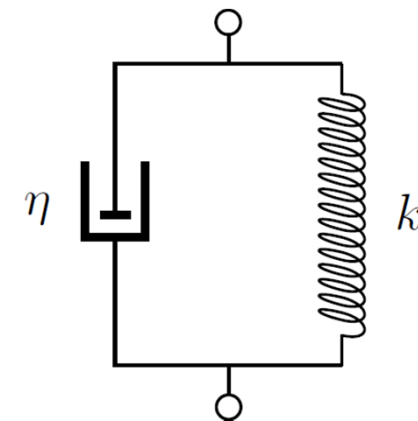
- Structural damping: inside the structure
- Viscous damping: outside the structure

if the damping coefficient η of the specimen is obtained through the dynamic material test,

$$\sigma = \underbrace{\sigma_k}_{\text{elasticity}} + \underbrace{\sigma_\eta}_{\text{viscosity}} = k\varepsilon + \eta\dot{\varepsilon} \rightarrow \sigma = \mathbf{D}_e \varepsilon + \mathbf{H}_e \dot{\varepsilon} \xrightarrow{H_e = \alpha \mathbf{D}_e} \sigma = \mathbf{D}_e (\varepsilon + \alpha \dot{\varepsilon})$$

$$\xrightarrow{\text{FEM}} \left\{ \begin{array}{l} \mathbf{C}_e = \alpha \mathbf{K}_e \text{ (proportional damping)} \\ \mathbf{C}_e = \beta \mathbf{M}_e \end{array} \right\} \rightarrow \mathbf{C}_e = \beta \mathbf{M}_e + \alpha \mathbf{K}_e \text{ (Rayleigh damping)}$$

$$\left\{ \begin{array}{l} \alpha = 2 \frac{h_2 \omega_2 - h_1 \omega_1}{\omega_2^2 - \omega_1^2} \\ \beta = 2 \omega_1 \omega_2 \frac{h_1 \omega_2 - h_2 \omega_1}{\omega_2^2 - \omega_1^2} \end{array} \right. \quad \text{where} \quad \left\{ \begin{array}{l} \omega_i : i\text{-th natural frequency} \\ h_i : i\text{-th damping coefficient} \end{array} \right.$$



Solution Method

$$\begin{cases} \mathbf{M}\ddot{\mathbf{d}} + \mathbf{K}\mathbf{d} = \mathbf{F} & (\text{no damping}) \\ \mathbf{M}\ddot{\mathbf{d}} + \mathbf{C}\dot{\mathbf{d}} + \mathbf{K}\mathbf{d} = \mathbf{F} & (\text{damping}) \end{cases}$$

- Linear problem
 - Direction integration method (sequential integration)
 - Mode analysis method
 - Frequency response method
 - Response spectral method
- Nonlinear problem
 - Direction integration method

Direct Integration Method

- Central difference: $O((\Delta t)^2)$

$$\ddot{d}^n \approx \frac{1}{2\Delta t} (d^{n+1} - d^{n-1})$$

$$\ddot{d}^n \approx \frac{\frac{(d^{n+1} - d^n)}{\Delta t} - \frac{(d^n - d^{n-1})}{\Delta t}}{\Delta t} = \frac{1}{\Delta t^2} (d^{n+1} - 2d^n + d^{n-1})$$

$$M\ddot{d} + C\dot{d} + Kd = F \rightarrow \left(\frac{1}{\Delta t^2} M + \frac{1}{2\Delta t} C \right) d^{n+1} = F^n - \left(K - \frac{2}{\Delta t^2} M \right) d^n - \left(\frac{1}{\Delta t^2} M - \frac{1}{2\Delta t} C \right) d^{n-1}$$

$d^n, d^{n-1} \rightarrow d^{n+1}$, lumped mass + no damping $\rightarrow$ explicit method

$d^n, d^{n-1} \rightarrow d^{n+1} \rightarrow \ddot{d}^n, \dot{d}^n$: sequential integration method (step-by-step method)

- Linear acceleration method
- Newmark's β method
- Wilson θ method

Linear Acceleration Method

$$\begin{cases} d^{n+1} = d^n + \Delta t \dot{d}^n + \frac{\Delta t^2}{3} \ddot{d}^n + \frac{\Delta t^2}{6} \ddot{d}^{n+1} \\ \dot{d}^{n+1} = \dot{d}^n + \frac{\Delta t}{2} (\ddot{d}^n + \ddot{d}^{n+1}) \end{cases}$$

[unknown: acceleration]

$$M\ddot{d}^{n+1} + C\dot{d}^{n+1} + Kd^{n+1} = F^{n+1} \rightarrow$$

$$\left(M + \frac{\Delta t}{2} C + \frac{\Delta t^2}{3} K \right) \ddot{d}^{n+1} = F^{n+1} - C \left(\dot{d}^n + \frac{\Delta t}{2} \ddot{d}^n \right) - K \left(d^n + \Delta t \dot{d}^n + \frac{\Delta t^2}{3} \ddot{d}^n \right)$$

$$\ddot{d}^{n+1} \rightarrow \dot{d}^{n+1}, d^{n+1}$$

[unknown: displacement]

$$\begin{cases} d^{n+1} = d^n + \Delta t \dot{d}^n + \frac{\Delta t^2}{3} \ddot{d}^n + \frac{\Delta t^2}{6} \ddot{d}^{n+1} \\ \dot{d}^{n+1} = \dot{d}^n + \frac{\Delta t}{2} (\ddot{d}^n + \ddot{d}^{n+1}) \end{cases} \rightarrow \begin{cases} \ddot{d}^{n+1} = \frac{6}{\Delta t^2} (d^{n+1} - d^n) - \frac{6}{\Delta t} \dot{d}^n - 2\ddot{d}^n \\ \dot{d}^{n+1} = \frac{3}{\Delta t} (d^{n+1} - d^n) - 2\dot{d}^n - \frac{\Delta t}{2} \ddot{d}^n \end{cases}$$

$$M\ddot{d}^{n+1} + C\dot{d}^{n+1} + Kd^{n+1} = F^{n+1} \rightarrow$$

$$\left(\frac{6}{\Delta t^2} M + \frac{3}{\Delta t} C + K \right) d^{n+1} = F^{n+1} + M \left(2\ddot{d}^n + \frac{6}{\Delta t} \dot{d}^n + \frac{6}{\Delta t^2} d^n \right) + C \left(\frac{\Delta t}{2} \ddot{d}^n + 2\dot{d}^n + \frac{3}{\Delta t} d^n \right)$$

$$d^{n+1} \rightarrow \dot{d}^{n+1}, \ddot{d}^{n+1}$$

Newmark's β method (1)

$$\begin{cases} \mathbf{d}^{n+1} = \mathbf{d}^n + \Delta t \dot{\mathbf{d}}^n + \Delta t^2 \left(\frac{1}{2} - \beta \right) \ddot{\mathbf{d}}^n + \Delta t^2 \beta \ddot{\mathbf{d}}^{n+1} \\ \dot{\mathbf{d}}^{n+1} = \dot{\mathbf{d}}^n + \Delta t (1 - \gamma) \ddot{\mathbf{d}}^n + \Delta t \gamma \ddot{\mathbf{d}}^{n+1} \end{cases}$$

if $\gamma = \frac{1}{2}$, then $\dot{\mathbf{d}}^{n+1} = \dot{\mathbf{d}}^n + \frac{\Delta t}{2} (\ddot{\mathbf{d}}^n + \ddot{\mathbf{d}}^{n+1}) \rightarrow$ linear acceleration method

$$0 \leq \beta \leq \frac{1}{2}$$

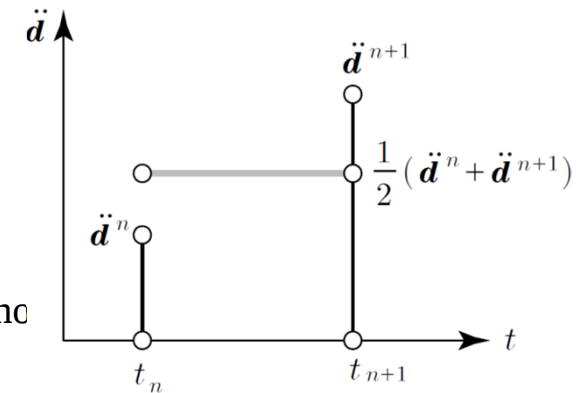
(1) $\beta = 0 : \mathbf{d}^{n+1} = \mathbf{d}^n + \Delta t \dot{\mathbf{d}}^n + \frac{\Delta t^2}{2} \ddot{\mathbf{d}}^n \rightarrow$ unconditionally unstable

(2) $\beta = \frac{1}{4} : \mathbf{d}^{n+1} = \mathbf{d}^n + \Delta t \dot{\mathbf{d}}^n + \frac{\Delta t^2}{2} \left(\frac{\ddot{\mathbf{d}}^n + \ddot{\mathbf{d}}^{n+1}}{2} \right) \rightarrow$ average acceleration method

(3) $\beta = \frac{1}{6} : \mathbf{d}^{n+1} = \mathbf{d}^n + \Delta t \dot{\mathbf{d}}^n + \frac{\Delta t^2}{3} \ddot{\mathbf{d}}^n + \frac{\Delta t^2}{6} \ddot{\mathbf{d}}^{n+1} \rightarrow$ linear acceleration method

Newmark's β method $\left(\gamma = \frac{1}{2}, \beta = \frac{1}{6} \right) \Leftrightarrow$ linear acceleration method

Newmark's β method is proposed for unconditionally stable integration scheme.



Newmark's β method (2)

[unknown: acceleration]($\gamma = 1/2$)

$$\mathbf{M}\ddot{\mathbf{d}}^{n+1} + \mathbf{C}\dot{\mathbf{d}}^{n+1} + \mathbf{K}\mathbf{d}^{n+1} = \mathbf{F}^{n+1} \rightarrow$$

$$\left(\mathbf{M} + \frac{\Delta t}{2} \mathbf{C} + \beta \Delta t^2 \mathbf{K} \right) \ddot{\mathbf{d}}^{n+1} = \mathbf{F}^{n+1} - \mathbf{C} \left(\dot{\mathbf{d}}^n + \frac{\Delta t}{2} \ddot{\mathbf{d}}^n \right) - \mathbf{K} \left\{ \mathbf{d}^n + \Delta t \dot{\mathbf{d}}^n + \left(\frac{1}{2} - \beta \right) \Delta t^2 \ddot{\mathbf{d}}^n \right\}$$

$$\ddot{\mathbf{d}}^{n+1} \rightarrow \dot{\mathbf{d}}^{n+1}, \mathbf{d}^{n+1}$$

[unknown: displacement]($\gamma = 1/2$)

$$\begin{cases} \mathbf{d}^{n+1} = \mathbf{d}^n + \Delta t \dot{\mathbf{d}}^n + \Delta t^2 \left(\frac{1}{2} - \beta \right) \ddot{\mathbf{d}}^n + \Delta t^2 \beta \ddot{\mathbf{d}}^{n+1} \\ \dot{\mathbf{d}}^{n+1} = \dot{\mathbf{d}}^n + \Delta t (1 - \gamma) \ddot{\mathbf{d}}^n + \Delta t \gamma \ddot{\mathbf{d}}^{n+1} \end{cases} \rightarrow \begin{cases} \ddot{\mathbf{d}}^{n+1} = \frac{1}{\beta \Delta t^2} (\mathbf{d}^{n+1} - \mathbf{d}^n) - \frac{1}{\beta \Delta t} \dot{\mathbf{d}}^n - \left(\frac{1}{2\beta} - 1 \right) \ddot{\mathbf{d}}^n \\ \dot{\mathbf{d}}^{n+1} = \frac{1}{2\beta \Delta t} (\mathbf{d}^{n+1} - \mathbf{d}^n) - \left(\frac{1}{2\beta} - 1 \right) \dot{\mathbf{d}}^n - \left(\frac{1}{4\beta} - 1 \right) \Delta t \ddot{\mathbf{d}}^n \end{cases}$$

$$\mathbf{M}\ddot{\mathbf{d}}^{n+1} + \mathbf{C}\dot{\mathbf{d}}^{n+1} + \mathbf{K}\mathbf{d}^{n+1} = \mathbf{F}^{n+1} \rightarrow$$

$$\left(\frac{1}{\beta \Delta t^2} \mathbf{M} + \frac{1}{2\beta \Delta t} \mathbf{C} + \mathbf{K} \right) \mathbf{d}^{n+1} = \mathbf{F}^{n+1} + \mathbf{M} \left\{ \left(\frac{1}{2\beta} - 1 \right) \ddot{\mathbf{d}}^n + \frac{1}{\beta \Delta t} \dot{\mathbf{d}}^n + \frac{1}{\beta \Delta t^2} \mathbf{d}^n \right\}$$

$$+ \mathbf{C} \left\{ \left(\frac{1}{4\beta} - 1 \right) \Delta t \ddot{\mathbf{d}}^n + \left(\frac{1}{2\beta} - 1 \right) \dot{\mathbf{d}}^n + \frac{1}{2\beta \Delta t} \mathbf{d}^n \right\}$$

$$\mathbf{d}^{n+1} \rightarrow \dot{\mathbf{d}}^{n+1}, \ddot{\mathbf{d}}^{n+1}$$

Wilson θ method (1)

- Extension of linear acceleration method
 - Newmark β method: linear between t_n and t_{n+1}
 - Wilson θ method: linear between t_n and $t_{n+\theta}$

$$\begin{cases} d^{n+\theta} = d^n + \theta \Delta t \dot{d}^n + \frac{(\theta \Delta t)^2}{6} (\ddot{d}^{n+\theta} + 2\ddot{d}^n) \\ \dot{d}^{n+\theta} = \dot{d}^n + \frac{\theta \Delta t}{2} (\ddot{d}^{n+\theta} + \ddot{d}^n) \end{cases}$$

$\theta = 1 \rightarrow$ linear acceleration method

$\theta \geq 1.37 \rightarrow$ unconditionally stable, but inaccurate solution for too large θ

$$\begin{cases} \ddot{d}^{n+1} = \frac{(\theta - 1)\ddot{d}^n + \ddot{d}^{n+\theta}}{\theta} \\ \dot{d}^{n+1} = \dot{d}^n + \frac{\Delta t}{2} (\ddot{d}^{n+1} + \ddot{d}^n) \\ d^{n+1} = d^n + \Delta t \dot{d}^n + \frac{\Delta t^2}{6} (\ddot{d}^{n+1} + 2\ddot{d}^n) \end{cases}$$

Wilson θ method (2)

[unknown: acceleration]

$$M\ddot{d}^{n+\theta} + C\dot{d}^{n+\theta} + Kd^{n+\theta} = F^{n+\theta} \rightarrow$$

$$\left(M + \frac{\theta\Delta t}{2}C + \frac{(\theta\Delta t)^2}{6}K \right) \ddot{d}^{n+\theta} = F^{n+\theta} - C \left(\dot{d}^n + \frac{\theta\Delta t}{2}\ddot{d}^n \right) - K \left\{ d^n + \theta\Delta t\dot{d}^n + \frac{(\theta\Delta t)^2}{3}\ddot{d}^n \right\}$$

$$\ddot{d}^{n+\theta} \rightarrow \ddot{d}^{n+1} \rightarrow \dot{d}^{n+1}, d^{n+1}$$

[unknown: displacement]

$$\begin{cases} d^{n+\theta} = d^n + \theta\Delta t\dot{d}^n + \frac{(\theta\Delta t)^2}{6}(\ddot{d}^{n+\theta} + 2\ddot{d}^n) \\ \dot{d}^{n+\theta} = \dot{d}^n + \frac{\theta\Delta t}{2}(\ddot{d}^{n+\theta} + \ddot{d}^n) \end{cases} \rightarrow \begin{cases} \ddot{d}^{n+\theta} = \frac{6}{(\theta\Delta t)^2}(d^{n+\theta} - d^n) - \frac{6}{\theta\Delta t}\dot{d}^n - 2\ddot{d}^n \\ \dot{d}^{n+\theta} = \frac{3}{\theta\Delta t}(d^{n+\theta} - d^n) - 2\dot{d}^n - \frac{\theta\Delta t}{2}\ddot{d}^n \end{cases}$$

$$M\ddot{d}^{n+\theta} + C\dot{d}^{n+\theta} + Kd^{n+\theta} = F^{n+\theta} \rightarrow$$

$$\left(\frac{6}{(\theta\Delta t)^2}M + \frac{3}{\theta\Delta t}C + K \right) d^{n+\theta} = F^{n+\theta} + M \left\{ 2\ddot{d}^n + \frac{6}{\theta\Delta t}\dot{d}^n + \frac{6}{(\theta\Delta t)^2}d^n \right\} + C \left(\frac{\theta\Delta t}{2}\ddot{d}^n + 2\dot{d}^n + \frac{3}{\theta\Delta t}d^n \right)$$

$$d^{n+\theta} \rightarrow \ddot{d}^{n+\theta} \rightarrow d^{n+1} \rightarrow \dot{d}^{n+1}, \ddot{d}^{n+1}$$