SAFETY SAFETY



SEMINARS

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Tables & Graphs Summarizing all Important Rules & Regulations in Vehicle Safety

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2017

Simulation & Engineering

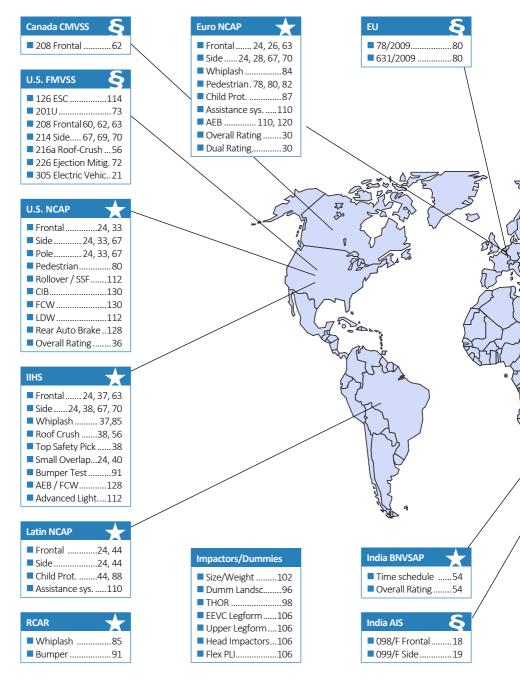


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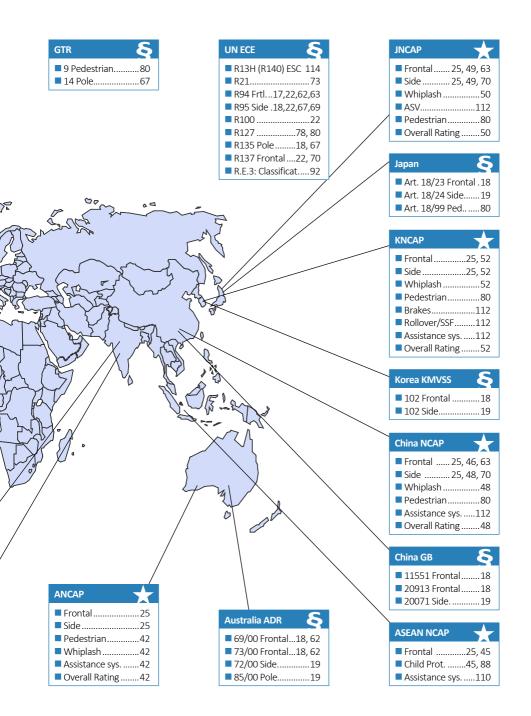


SafetyWissen Navigator











Seminar Guide

Here you find the courses you need to get your job done!

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***** +49-6023-964060

Legend

- Seminar/Event that focusses on this topic
- Seminar/Event that deals with this topic (among others)

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The Importance of Continuous Learning

The change in the automotive industry is ubiquitous. New technologies profoundly alter the business and established corporations are suddenly facing the competition of start-ups. Development processes that have been meticulously optimized need further acceleration and totally new development steps are suddenly required.

The possibilities, but also the necessities that result from new business models and a continuously increasing degree of digitalization, are enormous.

These big challenges are mastered best by those companies that systematically prepare their employees for the new developments and those that invest into the capabilities of their personnel.

We are not born with capabilities; we are trained for capabilities. And this exactly enables engineers to constantly adapt to changing requirements and to actively create the future.

With the SafetyCompanion we have compiled an attractive program of seminars and events, that covers the whole breadth of automotive safety: from passive safety to accident avoidance and safety for automated driving.

In addition to the offerings in the SafetyCompanion, we also cater for your individual needs for customized trainings, e.g. training on your premises. Use our experience and the expertise of our trainers to achieve your goals.

Our knowledge services have again been expanded significantly. Five new knowledge pages have been added to the SafetyCompanion; more than 40 pages have been updated. Our web portal www.safetywissen.com continues to be popular with engineers worldwide. Daily news from the world of automotive safety and thousands of global requirements documents make it a valuable resource for automotive engineers.

Now is the best time for your company and your associates to embrace the tremendous changes in the automobile industry for your benefit. We are happy to support you.

For the whole team of carhs.training

Rainer Hoffmann President & CEO

alf but

Ralf Reuter Executive Vice President



Safety**Wissen** on more than 60 pages more than 140 seminars & events



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References

ACTS, Adam Opel, Audi, AZOS, Bentley Motors, Bertrandt, BMW, Bosch, Brose, CATARC, Continental, CSI, Daimler, Dalphimetal, Delphi, Dura Automotive, EDAG, Faurecia, Ford, Global NCAP, Grammer, HAITEC, Honda, IAV, Idiada, IEE, JCI, IVM, Lear, Magna, Mahindra & Mahindra, MBtech, Messring, Open Air Systems, PATAC, P+Z, SAIC, SMP, SMSC, Seat, Siemens, TAKATA, TASS, Tecosim, TRW, TTTech, VIF, Volkswagen.

Attractive Prices

With reference to our regular seminar fees we offer attractive discounts on our in-house seminars:

1 Day Seminar								
Discount	for the							
30%	5 th - 8 th Participant							
60%	9 th - 12 th Participant							
70%	13 th - 16 th Participant							
75%	17 th - 20 th Participant							
80%	from the 21 st Participant							

2 Day Seminar								
Discount	for the							
50%	5 th - 8 th Participant							
70%	9 th - 12 th Participant							
75%	13 th - 16 th Participant							
80%	17 th - 20 th Participant							
85%	from the 21 st Participant							

Passive Safety

carhs

THE FUTURE OF AUTOMOTIVE SAFETY

Supporting automotive development engineers to further improve automotive safety, that is the essence of SafetyWeek.

In a unique combination of knowledge congress, events and exhibition, SafetyWeek offers participants and visitors the opportunity, to bring their expertise up-to-date and to learn about the latest developments and technologies in product development and product verification.

In 2017 SafetyWeek will feature numerous highlights:

- The Knowledge Congress SafetyUpDate +active with the most current updates on requirements and solutions in active and passive safety. And again in 2017: presentations of the safety strategies and equipment of recently launched automobiles by OEMs ⊃ page 14
- The **SafetyTesting** *+active* with the innovations from the Leaders in Testing and Simulation of components and systems in active and passive safety.
- The Cooperation Forum Driver Assistance Systems with a view into the future of mobility, organized by Bayern Innovativ
- The accompanying exhibition SafetyExpo, the meeting point for suppliers and decision makers in automotive safety.



SafetyWeek: Overview Topics and Products







Who should attend?

SafetyWeek is the meeting point for everyone involved in vehicle safety. This includes developers as well as test and simulation engineers from OEMs and suppliers, manufacturers of test systems, representatives of governments and consumer protection organizations and researchers from universities and research institutes.

	DATE	16 18. May 2017
	HOMEPAGE	www.carhs.de/safetyweek
Facts	VENUE	Stadthalle Aschaffenburg, Schloßplatz 1, 63736 Aschaffenburg
	LANGUAGE	German with simultaneous translation into English
	PRICE	from 420 EUR (single event)



SAFETYUPDATE +active

The concept is familiar: To keep software up-to-date you regularly make an update. The same is true for automotive safety engineering: To keep yourself up-to-date you have to attend the SafetyUpDate on a regular basis. Here you get a comprehensive overview of all relevant news in automotive safety.

Active + Passive Safety = SafetyUpDate +active

The SafetyUpDate reflects the close integration of active and passive safety and combines both topics in one event. General topics such as the NCAP consumer tests are dealt with in plenary presentations, whereas specific topics such as testing are presented in parallel session on active respectively passive safety.

Conference topics include:

- Regulations for active and passive safety
- NCAP consumer protection tests
- Development tools: Test & Simulation
- Development strategies & solutions
- Biomechanics & accident research

From Experts for Experts

The speakers are leading experts from government agencies, consumer protection organizations, industry and universities. We consider it important that the UpDate presentations are product-neutral and practical.

Meeting Point: Expert Dialog

In addition to the presentations the SafetyUpDate encourages the communication among experts. After the presentations the speakers are available for discussions at the Meeting-Point.

Who should attend?

The SafetyUpDate is aimed at automotive developers who are interested in active or passive vehicle safety and want to bring their knowledge up-to-date. In addition to the knowledge update, SafetyUpDate offers excellent opportunities to build and maintain contacts in the safety community.

	DATE	1617. May 2017	2627. September 2017
	HOMEPAGE	www.carhs.de/asu	www.carhs.de/gsu
Facts	VENUE	Stadthalle Aschaffenburg	Technische Universität Graz
	LANGUAGE	German with translation into English	German with translation into English
	PRICE	1.450,- EUR till 18.04.2017, thereafter 1.690,- EUR	1.450,- EUR till 29.08.2017, thereafter 1.690,- EUR









carhs

Introduction to Passive Safety of Vehicles

Course Description

Ever increasing requirements regarding vehicle safety have led to rapid developments, with major innovations in the field of Active and Passive Safety. Especially legal requirements in the USA (FMVSS 208, 214), the consumer information tests U.S. NCAP, Euro NCAP and IIHS, as well as pedestrian protection should be mentioned here. So far an end of this development is not in sight.

The seminar provides an introduction to Passive Safety of Vehicles. Passive Safety is about initiatives and legal provisions for the limitation of injuries following an accident. All important topics are covered in the seminar, from accident statistics and injury-biomechanics, which are decisive parts of accident research, to the crash-rules and regulations that are derived from the latter, and also to consumer information-tests with protection criteria and test procedures, and eventually to crash tests, where the compliance with the compulsory limits is tested and proven in test procedures. Specific attention is given to dummies, with which the potential loads on a person in an accident can be measured. Finally the basic principles of occupant protection are explained, and the components of occupant protection systems, respectively restraint-systems in motor vehicles such as airbags, belt-system, steering wheel, seat, interior, stiff passenger compartment and others, as well as their increasingly complex interaction, also in terms of new systems, will be discussed.

Course Objectives

It is the primary objective of this seminar to communicate an understanding for the entire field of Passive Safety with all its facets and correlations, but also for its limits and trends. In the seminar you are going to learn about and understand the most important topics and can then judge their importance for your work. With the extensive, up-to-date documentation you obtain a valuable and unique reference book for your daily work.

Who should attend?

The seminar addresses everybody who wants to obtain an upto-date overview of this wide area. It is suited for novices in the field of Passive Safety of Vehicles such as university graduates, career changers, project assistants, internal service providers, but also for highly qualified technicians from the crash-test lab.

Course Contents

- Introduction to vehicle safety
 - Overview active and passive safety
 - Crash physics
 - Accident research
 - General accident research
 - Classification
 - Statistics
- Biomechanics
 - Human anatomy
 - Injury mechanisms & injury criteria
- Dummy technology
- Crash testing
 - Crash test systems and components
 - Test methods
- Crash rules and regulations
 - Institutions
 - Rules and regulations
 - NCAP tests
 - Latest trends
- Protection principles, occupant protection systems
- Protection principles of passive safety
- Occupant protection systems
- Passenger compartment, interior
- OOP, pre crash, post crash, sensor system, vehicle body
- Optimization of restraint systems, adaptive systems
- Integrated safety



Rainer Hoffmann (carhs.training gmbh) has been involved in automotive safety throughout his career. After graduating from Wayne State University, he joined Porsche as a research associate in passive safety. Mr. Hoffmann advanced safety simulation during his subsequent tenure at ESI Group where he introduced new techniques like airbag simulation, numerical airbag folding and FE dummy modeling. As the head of the simulation department of PARS (now Continental Safety Engineering), Mr. Hoffmann led the R&D efforts for some of the first series production side airbag developments. In 1994 Mr. Hoffmann founded EASi Engineering GmbH, which in 2006 was renamed to carhs GmbH. He has authored numerous technical papers and has been granted German and international patents in the automotive safety field.

	DATE	COURSE ID	VENUE	DURATION	I PRICE	LANGUAGE
	1517.02.2017	3016	Tianjin	3 Days	6.900,- RMB	
Venues	2526.04.2017	2917	Landsberg am Lech	2 Days	1.290,- EUR till 28.03.2017, thereafter 1.540,- EUR	
త	1314.06.2017	2904	Alzenau	2 Days	1.290,- EUR till 16.05.2017, thereafter 1.540,- EUR	
Dates	0607.09.2017	2936	Tappenbeck	2 Days	1.290,- EUR till 09.08.2017, thereafter 1.540,- EUR	
	30.1001.11.2017	3017	Tianjin	3 Days	6.900,- RMB	
	2021.11.2017	2916	Alzenau	2 Days	1.290,- EUR till 23.10.2017, thereafter 1.540,- EUR	



International Safety and Crash-Test Regulations: Current Status and Future Developments

Course Description

Since the 1960's, the regulation of vehicle safety performance has had a major impact on vehicle and system design. As automotive manufacturing has evolved into an integrated global system, understanding and anticipating legal requirements has become an immense challenge. Regulators collaborate and diverge in how they address road-safety policy goals. Regulatory changes in a single market can translate into global customer requirements. And these requirements are continuously evolving. In a compact program, this two-day seminar provides a worldwide update on the passive safety landscape, covering local, national, regional, and international policy and rulemaking developments.

The first segment of the seminar focuses on regulatory institutions and processes. By understanding the regulatory environment, including the trend towards an integrated global regulatory system, businesses can better prepare for changes that impact competitiveness and customer satisfaction.

The second segment applies this knowledge to current and future regulatory requirements. The seminar covers crashworthiness (frontal, side, rear impact, etc.) as well as pedestrian protection and new technologies.

Course Objectives

This course informs participants of recent developments and discussions within the global regulatory community concerning passive safety. The seminar explores differences in regulatory systems and philosophies, in compliance and enforcement, and in the forces behind the regulation of vehicle safety. The course provides participants with a broad understanding current regulatory directions and guidance on how to follow, and even influence, future requirements.

Who should attend?

This seminar should be of interest to anyone involved with meeting and anticipating legal requirements for vehicle safety performance across international markets. The course provides a compact review of changes in passive safety requirements and current priorities across the international regulatory community. Moreover, the course provides knowledge critical to understanding differences in the way regulators establish and enforce these legal requirements.

Course Contents

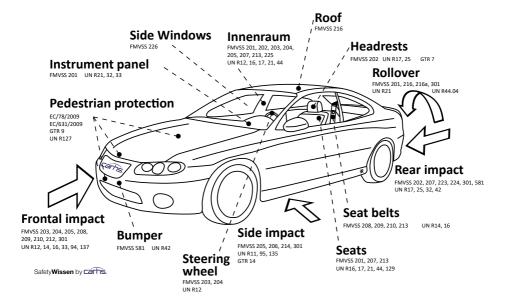
- History of safety regulation and development of legal regimes (e.g., self-certification, type approval, product liability, in-use surveillance
- Regulatory agencies and rulemaking processes (e.g., UN World Forum for the Harmonization of Vehicle Regulations, European Commission, U.S. National Highway Traffic Safety Administration, etc.)
- Regulatory drivers and priorities (e.g., accident data, injury dynamics, injury assessment criteria, test tools, harmonization, whole vehicle approval, competitiveness, etc.)
- Types and purposes of regulations (UN Regulations, Global Technical Regulations, Federal Motor Vehicle Safety Standards, EU Regulations and Directives, etc.)
- Developments in crashworthiness and occupant protection requirements (frontal impact, side impact, pole-side impact, full width barrier, offset deformable barrier, mobile barrier, etc.)
- Vulnerable road user (VRU) protection (e.g., pedestrian safety, cyclist safety)
- Safety of new propulsion technologies (electric vehicles, hydrogen fuel-cells, minimum vehicle noise levels)
- Passive safety implications of new safety technologies (e.g., emergency call systems, collision avoidance, VRU detection, automated driving)

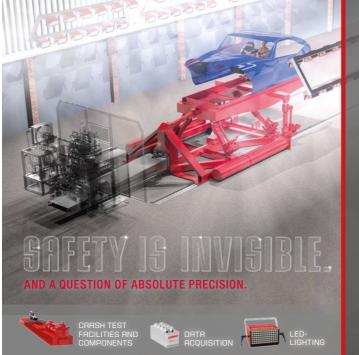


John Creamer (GlobalAutoRegs.com) is the founder of GlobalAutoRegs.com and a partner in The Potomac Alliance, a Washington-based international regulatory affairs consultancy. In his client advisory role, Mr. Creamer is regularly involved with meetings of the UN World Forum for the Harmonization of Vehicle Regulations (WP.29). Previously, he has held positions with the US International Trade Commission and the Motor & Equipment Manufacturers Association (representing the US automotive supplier industry), as the representative of the US auto parts industry in Japan, and with TRW Inc. (a leading global automotive safety systems supplier).

S	DATE	COURSE ID	VENUE	DURATION	N PRICE	LANGUAGE
Venu	0910.03.2017	2908	Alzenau	2 Days	1.290,- EUR till 09.02.2017, thereafter 1.540,- EUR	
es &	2829.06.2017	2865	Alzenau	2 Days	1.290,- EUR till 31.05.2017, thereafter 1.540,- EUR	
Dat	1415.09.2017	2871	Alzenau	2 Days	1.290,- EUR till 17.08.2017, thereafter 1.540,- EUR	

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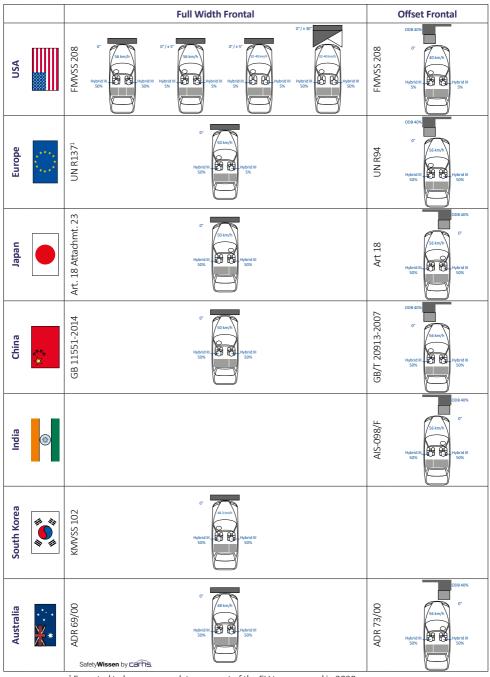
WWW.MESSRING.COM







Rules and Regulations on Occupant Protection



¹ Expected to become mandatory as part of the EU type appoval in 2020.





Side Barrier	Side Pole	Pedestrian	Rear	Head Impact	Rollover
FMVSS214	500k/ 0-335kh		FMVSS 202a FMVSS 301	FMVSS 201	Roof crush: FMVSS 216a Ejection Mitigation: FMVSS 226
	NS SS S	R (EC) 78/2009 R (EC) 631/2009 UN R127	UN R32	UN R21	
Art. 18 Attachmt. 24		Article 18 Attachment 99	Article 18 Attachment 34		
GB 20071-2006		GB/T 24550-2009	GB 20072-2006	GB11552-2009	Roof crush: GB26134-2010
4/660-SIV		AIS-100	AIS-101		
KMVVSS 102		KMVSS 102-2	Fin	d all detail <mark>SAFETY</mark> WISSEN	s in:
ADR 72/00 ADR 72/00 ADR 72/00 ADR 72/00	00 32 km/h 75 Rigd 254 mm Pole			Download @ carhs.c	com/app

¹ Expected to become mandatory as part of the EU type appoval in 2020.



Crash Safety of Alternative Propulsion Vehicles

Course Description

During recent years, vehicles with alternative propulsion systems have achieved an ever-increasing importance for the automotive market. In addition to gas-powered vehicles, which have already been existing for many years on the manufacturer and retrofit market, a wide range of hybrid vehicles has also established meanwhile. Even for pure electric vehicles, the first acquirable products are already on the market. Worldwide over 1 million electrified vehicles were on the streets in 2015. By decision of the German government, one million electric vehicles should be found driving on German roads by the year 2020. It is clear, however, that the automotive electrification cannot be stopped anymore.

With this new technology, new challenges for vehicle safety arise.

Electric shock risks on high-voltages systems, fire hazards in case of lithium-ion batteries and risks of rupture in case of gas tanks are the most important issues here. For every mode of drive, specific drive components and their particular safety requirements are described. In addition to common rules and standards, specific needs based on real-life accidents are being discussed.

For all relevant vehicle components the respective safety requirements, safety concepts and exemplary safety initiatives will be discussed. The state of the art concerning test standards, verification methods and possibilities for virtual safety will be shown. Future trends will be presented with the help of current research projects and results. Practical experience of rescuing, recovering and towing of electric vehicles complete the spectrum of accident safety.

Course Objectives

Participants will get an overview about automotive safety for alternative drive systems and will learn the special challenges and solutions which come along. Participants will be able to apply test methods and safeguarding concepts and to pursue development strategies in a target-oriented way.

Who should attend?

The seminar addresses development and research engineers as well technicians in the fields of testing and engineering. Due to its current relevance the course suits young professionals as well as experienced engineers who want to deepen their knowledge in this field.

Course Contents

- Overview alternative propulsion systems: gas, hybrid, electric and fuel cell vehicles
- Challenges for vehicle safety
- Legal requirements and standards for safety
- Safety requirements for real-world accidents
- Safety of high voltage systems
- Battery safety
- Gas tank safety
- Fuel cell safety
- Structural safety
- Safety concepts
- Rescuing, recovering and towing of electric vehicles



Rainer Justen (Daimler AG) has more than 25 years of experience in the field of vehicle safety. After his studies in mechanical engineering with a focus on automotive engineering he started his career in 1987 in the automotive development for Mercedes-Benz at Daimler AG. Several career milestones in the fields of vehicle safety, project management, safety concepts and active safety / driver assistance systems made him an expert on all relevant topics of automotive safety. Since 2008 he is working in the field of safety for alternative drive systems. Rainer Justen is author of numerous publications and papers on this topic. In 2015 Rainer Justen received the SAE Automotive Safety Award from the American Society of Automotive Engineers (SAE) for his work on the safety of Li-lon batteries in electric vehicles.

S	DATE	COURSE ID	VENUE	DURATION	I PRICE	LANGUAGE
Venu	2223.03.2017	2869	Alzenau	2 Days	1.290,- EUR till 22.02.2017, thereafter 1.540,- EUR	
tes &	2627.06.2017	2907	Alzenau	2 Days	1.290,- EUR till 29.05.2017, thereafter 1.540,- EUR	
Dat	0607.11.2017	2906	Alzenau	2 Days	1.290,- EUR till 09.10.2017, thereafter 1.540,- EUR	

nstructor

FMVSS 305: Safety Requirements for Electric Vehicles

Scope:

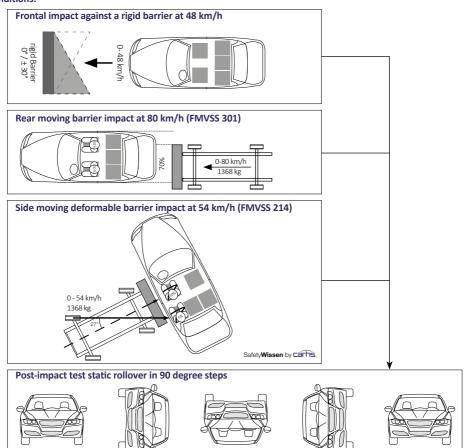
Cars, busses, trucks with a GVWR of 4536 kg or less that use electrical components with working voltages higher than 60 volts direct current (VDC) or 30 volts alternating current (VAC), and whose speed attainable is more than 40 km/h.

Requirements:

Under the test conditions described below (impact test and subsequent static rollover)

- max. 5 litres of electrolyte may spill from the batteries,
- there shall be no evidence of electrolyte leakage into the passenger compartments,
- all components of the electric energy storage/conversion system must be anchored to the vehicle,
- no battery system component that is located outside the passenger compartment shall enter the passenger compartment,
- electrical isolation must be greater than or equal to:
 - 500 ohms/V for all DC high voltage sources without isolation monitoring and for all AC high voltage sources,
 - 100 ohms/V for all DC high voltage sources with continuous monitoring of electrical isolation,
- the voltage of the voltage source (Vb, V1, V2) must be less than or equal to 30 VAC for AC components or 60 VDC for DC components.

Test Conditions:



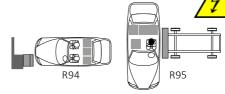






UN ECE: Safety Requirements for Electric Vehicles

Extension of UN R94 / R95:

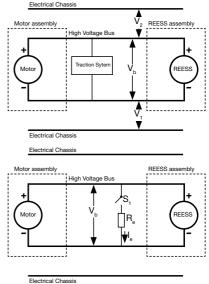


After crash tests according to UN R94 and R95 vehicles with a high voltage electrical powertrain (> 60 V DC or > 30 V AC) must meet the following requirements:

1. Protection against electrical shock

at least one of the four criteria specified below shall be met:

■ Absence of high voltage: The voltages V_{b} , V_1 and V_2 shall be \leq 30 V AC or \leq 60 V DC :



Low electrical energy:

The total energy (TE) on the high voltage buses shall < 2.0 J. Prior to the impact a switch S_1 and a known discharge resistor R_e is connected in parallel to the relevant capacitance . Not earlier than 5 s and not later than 60 s after impact S_1 shall be closed while the voltage V_b and the current I_e are recorded. From this TE is caluclated as follows:

$$TE = \int_{tc}^{th} V_{b} \times I_{e} dt$$

with $tc = time of closing S_1$

th = time when voltage drops below 60 V DC

Physical protection:

For protection against direct contact with high voltage live parts, the protection IPXXB shall be provided.

- Isolation resistance:
 - If the AC HV buses and the DC high voltage buses are galvanically isolated from each other, isolation resistance between the HV bus and the electrical chassis shall be ≥ 100 Ω/V of the working voltage for DC buses, and ≥ 500 Ω/V of the working voltage for AC buses.
 - If the AC HV buses and the DC HV buses are galvanically connected isolation resistance between the HV bus and the electrical chassis shall be \geq 500 Ω /V of the working voltage. (if the protection IPXXB is satisfied for all AC HV buses or the AC voltage is \leq 30 V after the vehicle impact, the isolation resistance shall be R_i \geq 100 Ohm/V)

2. Electrolyte spillage

In the period from the impact until 30 minutes after no electrolyte from the REESS (Rechargeable Electrical Energy Storage System) shall spill into the passenger compartment and no more than 7 % of electrolyte shall spill from the REESS.

3. REESS retention

REESS located inside the passenger compartment shall remain in the location in which they are installed and REESS components shall remain inside REESS boundaries. No part of any REESS that is located outside the passenger compartment for electric safety assessment shall enter the passenger compartment during or after the impact test.

UN R100:

M and N class vehicles with a maximum speed > 25 km/h must also comply with UN R100 Rev. 2



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NCAP-Tests in Europe and America

2017 2018

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	Euro NCAP	U.S. NCAP	IIHS	Latin NCAP
Full Width	V Hybrid III 5%	0' Hybrid III TACR Sofs Sofs Hybrid III SS Hybrid III SS Hybrid III SS Hybrid III SS Hybrid III SS	Get familiar with all NCA our seminar: NCAP - New Car Assessm Tests, Assessment Meth learn more on ⊃ page 11	ods, Ratings
ODB / SOB	ODB 40%	THOR SOX	ODB 40% Flat 150 500 2% 0"	ODB 404 0" Hybrid III Soros C3 10 10 10 10 10 10 10 10 10 10
MDB	Solumber Solumber Marcal Solution Solut	ES 3 M STORE STORE STOR	SD By SO By/// Mos Het, 1500 kg SD By	ES 2 Solarin By Mos Erv, Soly Q3
Pole	WS S05 Rgid 254 mm Pole	SD 15 VS 50%		Rigd 234 mm Pole
Rollover		■ SSF	■ Roof Crush	
Pedestrian	 Flex PLI Upper Legform Headforms AEB VRU Pedestrian AEB VRU Cyclist 	 Flex PLI Upper Legfom Headforms AEB Pedestrian Rear Automatic Braking 		Award
Child Safety	 Frontal ODB Side MDB CRS-Installation Vehicle based assessment 		 LATCH (Lower Anchors and Tethers for Children) 	 Frontal ODB Side MDB CRS- Installation Vehicle based assessment
Whiplash	 static front / rear dynamic (3 pulses) AEB City 		■ static ■ dynamic (1 pulse)	Safety Wissen by carfis .
Other	Assistance systems: SBR, SAS, AEB, LDW, LKA	 FCW, LDW, Rear View Cameras, AEB, DBS, BSD 	AEB, FCWHeadlights	 SBR, ABS (prerequisite for ≥ 3 star rating) ESC (prereq. f. ≥ 4 star)
24	page 26	⊃ page 33	⊃ page 37	⊃ page 44

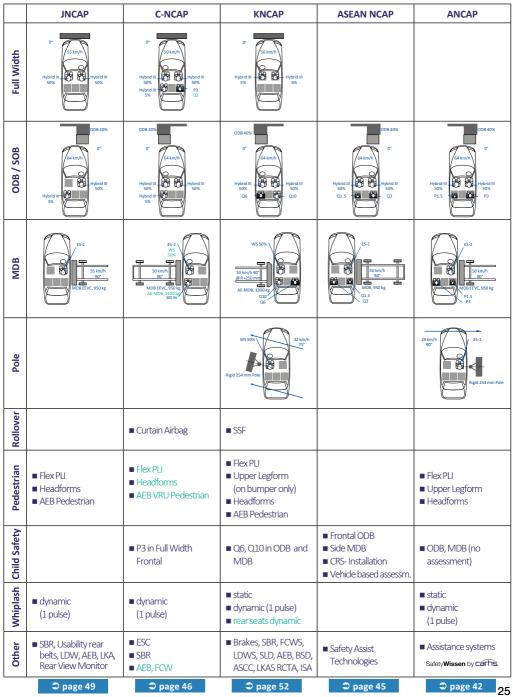


NCAP-Tests in Asia and Australia

2017 2018

UPDATE

SAFETY WISSEN



SAFETY WISSEN UPDATE

Euro NCAP





Assessment Protocol Version 7.0.3



Protection Criteria in Frontal Impact

Dummy	Region	Criteria	4 Points	0 Points	Modifiers		
Fronta	l-Impac	t on ODB with	40 % overlap	@ 64 km/h			
FIUITA		HIC15	< 500	> 700			
		a _{3ms} (g)	< 72	> 80			
		My,extension (Nm)	< 42	> 57	Unstable airbag/steering wheel		
	11		< 2.7 @ 0 ms	> 3.3 @ 0 ms	contact (-1 pt)		
	Head ¹ Neck	F _{z,tension} (kN)	< 2.3 @ 35 ms	> 2.9 @ 35 ms	Hazardous airbag deployment (-1 pt)		
	NECK		< 1.1 @ 60 ms	> 1.1 @ 60 ms	Incorrect airbag deployment (-1 pt)		
			< 1.9 @ 0 ms	> 3.1 @ 0 ms	Steering column displacement (-1 pt)		
		F _{x,shear} (kN)	< 1.2 @ 25-35 ms	> 1.5 @ 25-35 ms			
			< 1.1 @ 45 ms	> 1.1 @ 45 ms			
Hybrid III 50 %	Chast	Deflection (mm)	< 22	> 42	A-pillar displacement (-2 pt) Compartment deformed (-1 pt)		
	Chest	VC (m/s)	< 0.5	> 1.0	Steering wheel contact (-1 pt) Incorrect airbag deployment (-1 pt) Shoulder belt load > 6 kN (-2 pt)		
	Femur Knee	Axial Force (kN)	< 3.8	> 9.07 > 7.56 @ 10 ms	Variable contact (-1 pt) Concentrated loading (-1 pt)		
	halee	Displacement (mm)	< 6	>15	Incorrect airbag deployment (-1 pt)		
		Tibia Index	< 0.4	> 1.3	Z–displacement of worst pedal (-1 pt)		
	Tibia	Axial Force (kN)	< 2	> 8			
	Foot	x–Displacement pedal (mm)	< 100	> 200	Footwell rupture (-1 pt) Pedal blocking (-1 pt)		
Fronta	l-Impac	t on Rigid Wall	with 100 % o	verlap @ 50	km/h		
	Head ¹	HIC ₁₅	< 500	> 700	Unstable airbag/steering wheel		
	пеац-	a _{3ms} (g)	< 72	> 80	contact (-1 pt)		
		My,extension (Nm)	< 36	> 49	Hazardous airbag deployment (-1 pt)		
	Neck	F _{z,tension} (kN)	< 1.7	> 2.62	Incorrect airbag deployment (-1 pt) Steering column displacement (-1 pt)		
Hybrid III 5 %	Neck	F _{x,shear} (kN)	< 1.2	> 1.95	Rear seat: head forward excursion (-4 pt)		
	Chest	Deflection (mm)	< 18	> 42	Steering wheel contact (-1 pt) Incorrect airbag deployment (-1 pt)		
	Chest	VC (m/s)	< 0.5	> 1.0	Shoulder belt load > 6.0 kN (-2 pt)		
	Femur	Axial Force (kN)	< 2.6	> 6.2	Submarining (-4 pt)		

¹ If there is no hard contact (i.e. a_{res, peak} < 80 g and no other evidence of hard contact) a score of 4 points is awarded.



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- Tests of driver assistance and full auto brake systems for the prevention of rear-end collisions, protection of pedestrians and cyclists, prevention of accidents at intersections



SAFETY WISSEN UPDATE Euro NCAP Euro NCAP Protection Criteria in Side Impact (MDB and Pole)												
Protection Criteria in Side Impact (MDB and Pole)												
		Criteria npact (AE-MDE act under 75° (0 Points	Modifiers							
		HIC ₁₅	< 500	> 700								
	Head ²	a _{3ms} (g)	< 72	> 80	incorrect airbag deployment (-1 point) door opening (- 1 point/door) lateral shoulder force > 3.0 kN							
World SID 50 %	Chest	Deflection (mm)	< 28	> 50	(deduction of all chest points) VC > 1.0 m/s (deduction of all chest/							
	Abdomen	Deflection (mm)	< 47	> 65	abdomen points) head protection device assessment (-4 points)							
					(-4 points)							

¹ Pole: no sliding scale, only capping if $HIC_{15} > 700$ or $a_{res, peak} > 80$ g or direct head contact with the pole.

< 1.7

Modifier Side Head Protection Device

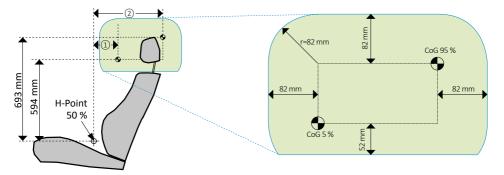
Pelvis

Pubic Symphysis

Peak Force (kN)

Inside the ,Head Protection Device Assessment Zone' (green) the head protection system's coverage is assessed. If the coverage is insufficient a 4 point modifier is applied the overall pole impact score. Areas outside the Daylight Opening (FMVSS 201) are excluded from assessment. Seams are not penalized if the un-inflated area is no wider than 15 mm. Any other un-inflated areas that are no larger than 50 mm in diameter (or equivalent area) are not penalized.

> 2.8



The head protection device (HPD) evaluation zone (green) is defined as a rounded rectangle around the head CoG box (defined by the head CoGs of the 5 % female and 95 % male occupants) at a distance of 82 mm from the upper and fore/aft edges and 52 mm below the bottom edge. The x-position of the CoG is defined relative to the H-Point of the 50 % male: Front seats:

(1) = H-Point(x) + 126 mm - seat travel(5th%ile- 50th%ile)

(2) = H-Point(x) + 147 mm + seat travel(50th%ile-95th%ile)

Rear seats:

1 = H-Point(x) + 126 mm - seat travel

(2) = H-Point(x) + 147 mm



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- Crash and structure computations, passenger simulation
- Subsystem safety testing

- Predictive, active and passive pedestrian protection
- Integration of new NCAP requirements
- Sensor selection for active and passive systems
- Crash and catapult testing, pre-crash testing

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UPDATE

SAFETY WISSEN





Euro NCAP Rating: 2017 - 2020

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Adult Occup	ant P	rotec	tion	Child Occup	ant Pi	otect	ion	Pedestrian Protection				Safety Assist			
Addit Occup		2018		cinia occup		2018		reacstriant		2018	2020	Surcey Assist	2017	2018	2020
		ax. poi				ax. poir				ax. poii				ax. poii	
Offset Frontal impact ⊃ Page 26	8	8	8	Dyn. Tests Frontal Degree 87	16	16	16	Head Impact ● Page 78	24	24	24	Seat Belt Reminder ⊃ Page 110	3	3	3
Full-width Frontal impact ⊃ Page 26	8	8	8	Dyn. Tests Side ⊃ Page 87	8	8	8	Leg Impact ● Page 78	6	6	6	Speed Assis- tance Syst. ● Page 110	3	3	3
Side impact (MDB) ⊃ Page 28	8	8	8	CRS Installation Page 87	12	12	12	Upper Leg Impact ⊃ Page 78	6	6	6	LDW / LKD / LSS ⊃ Page 110	3	4	4
Side impact (Pole) ⊃ Page 28	8	8	8	Vehicle based ⊃ Page 87	13	13	13	AEB VRU-Pe Page 122	6	6	6	AEB Inter- Urban ⊃ Page 126	3	3	4
Whiplash Front seats ⇒ Page 85	2	1.5	1.5					AEB VRU-Cy Page 124	-	6	6	Junction Assist			2
Whiplash Rear seats ⊃ Page 84	1	0.5	0.5												
AEB City ⇒ Page 120	3	4	4												
max. points (1)	38	38	38	max. points (1)	49	49	49	max. points (1)	42	48	48	max. points (1)	12	13	16
normalised score (2)	actua	I point	s / (1)	normalised score (2)	actual points / (1)		normalised score (2)	actual points / (1)		s / (1)	normalised score (2)	actual points / (1)			
weighting (3)		40 %		weighting (3)		20 %		weighting (3)		20 %		weighting (3)		20 %	
weighted score (4)		(2)x(3))	weighted score (4)		(2)x(3)		weighted score (4)		(2)x(3)		weighted score (4)		(2)x(3)	
			Bala	ncing: minimun	n norm	alised	score	(2) by box for th	ie resp	ective	star rat	ing:			
	80 %	80 %	80 %		75 %	80 %	80 %		60 %	60 %	60 %		50 %	70 %	70 %
	70 %	70 %	70 %		60 %	70 %	70 %		50 %	50 %	50 %		40 %	60 %	60 %
	60 %	60 %	60 %	-	30 %	60 %	60 %	-	40 %	40 %	40 %	-	25 %	50 %	50 %
	50 %	50 %	50 %		25 %	50 %		•	30 %	30 %	30 %	•	15 %	40 %	40 %
*	40 %	40 %	40 %		15 %				20 %	20 %	20 %		10 %	30 %	30 %
								re (5) = ∑(4)							
Rold figures in dis-	to ob o					only fo	r rankir	ng the results wi	thin ve	hicle ca	ategorie	es.			
Bold figures indicat	re cuant	ges with	respect	to the previous yea	at,							Euro NCAP Log	go Gu	idelin	es

VSSTR Protocol Version 7.0

Dual Rating

Euro NCAP issues a base rating for standard equipment only. Fitments rates for safety assist technologies are no longer considered. Optionally manufacturers of cars that have achieved at least 3 stars can apply for a secondary rating of a model equipped with an optional safety package that meets a certain market installation rate (an average of 25 % in the first 3 years and of 55 % in the subsequent 3 years). The safety package must be actively promoted by the manufacturer. The safety package must be available, at least as an option, on all variants in the model range.





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Knee Mapping Workshop: The Euro NCAP Test Procedure

Course Description

Euro NCAP plays a leading role among the tests assessing the passive safety of vehicles in Europe. Its influence now also extends to other countries. Recently the knee impact test procedure within the Euro NCAP frontal impact test was modified, the goal being a less subjective assessment. A hard contact or a sharp edge in the knee area implies the danger for a car manufacturer to be punished with a so-called knee modifier (reduction in points). The knee modifier is the most frequent penalty within the Euro NCAP and impairs some vehicles' otherwise 5-star ratings. The allocation of a knee modifier often is a controversial decision. If a knee modifier has been allocated by the Euro NCAP inspector the car manufacturer has the possibility of proving - by means of a complex sled test procedure - that the modifier was not justified.

After a short introduction the main focus of the workshop is on the current Euro NCAP assessment procedure for frontal impact in the knee area (knee mapping). The current requirements will be explained in detail, in particular the knee modifiers 'Variable Contact' and 'Concentrated Loading', the areas of inspection and the threshold values. Positive / negative examples will facilitate the participants' understanding of the requirements and the assessment procedure. Participants will learn how to avoid a modifier. The sled test procedure will also be explained and discussed in detail.

In the afternoon a demo vehicle, which can be provided by participants, will be analyzed. Ralf Ambos, a trained Euro NCAP inspector, can give valuable hints here.

A perspective regarding the future development of the test procedure will be given at the end of the seminar.



The seminar addresses specialists from the field of crash, engineers and technicians from numerical simulation and testing, project engineers and managers who want to have a firsthand, up-to-date information and hints on how to avoid knee modifiers in Euro NCAP.

Course Contents

- Overview of Euro NCAP crash tests
- Euro NCAP requirements in the knee area
- Knee modifier, knee mapping test procedure
- Sled test procedure for knee impact
- Discussion of the assessment procedure and possibilities of interpretation
- Workshop with analysis of test vehicles, which can be provided by participants
- Future development of the test procedure



The workshop was very informative and relevant. The final analysis of a test vehicle was very helpful."

Ray Longbottom, SAIC Motor UK Technical Centre Ltd., UK



Ralf Ambos (DEKRA Automobil GmbH) studied automotive technology at the university for technology and economy in Dresden, Germany. He has worked as a project manager in passive vehicle safety for eight years. In 2004 he was trained as an inspector for Euro NCAP. In 2009 he joined DEKRA Automobil GmbH.

Date	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
	11.09.2017	2861	Alzenau	1 Day	740,- EUR till 14.08.2017, thereafter 890,- EUR	





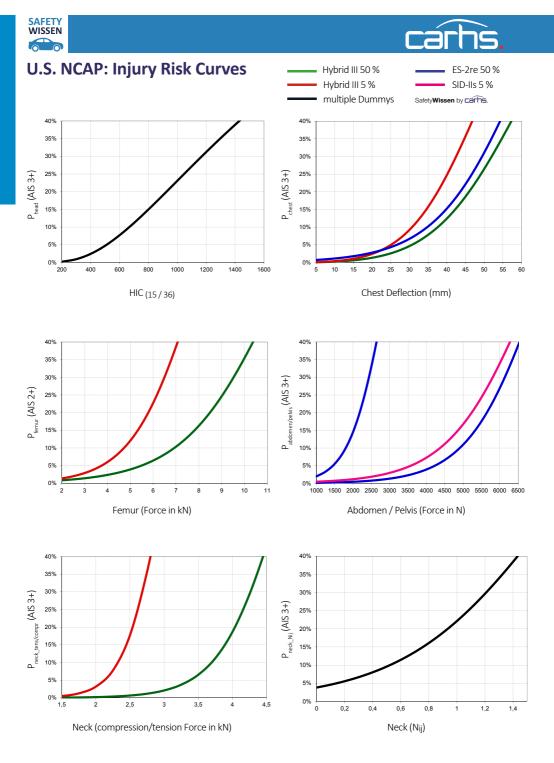
U.S. NCAP



Docket No. NHTSA-2006-26555 **Tests and Criteria** 32 km/h 75° ES-2 r SG km 62 km/h Hybrid III 50 % Hybrid III 5 % 55 km/h T. Rigid 254 mm Pole MDB, 1368 kg SID IIs Injury Risk Curves Injury Criteria SafetyWissen by Carhs Frontal Impact Rigid Wall 100 % Overlap / 56 km/h Hybrid III 50 % (Driver) Dummy Hybrid III 5 % (Passenger) $P_{head}(AIS3+) = \Phi\left(\frac{\ln(HIC15) - 7.45231}{0.72005}\right)$ P_{head} (AIS 3+) = $\Phi\left(\frac{\ln(HIC15) - 7.45231}{0.73998}\right)$ Head (HIC15) where Φ = cumulative normal distribution where Φ = cumulative normal distribution $P_{chest_defl}(AIS3+) = \frac{1}{1 + e^{10.5456 - 1.568*(ChestDefl)^{0.4612}}}$ $P_{chest_defl}(AIS3+) = \frac{1}{1 + e^{10.5456 - 1.7212*(ChestDefl)^{0.4612}}}$ Chest (Deflection in mm) $P(AIS \ 2+) = \frac{1}{1 + e^{5.795 - 0.5196 Femur_Force}}$ $P(AIS \ 2+) = \frac{1}{1 + e^{5.7949 - 0.7619 Femur_Force}}$ Femur (Force in kN) $P_{\text{neck}_Nij}(\text{AIS3+}) = \frac{1}{1 + e^{3.2269 - 1.9688Nij}}$ $P_{\text{neck}_Nij}(\text{AIS 3+}) = \frac{1}{1 + e^{3.2269 - 1.9688Nij}}$ $P_{neck_Tens}(AIS3+) = \frac{1}{1+e^{10.9745-2.375Neck_Tension}}$ $P_{neck_Tens}(AIS3+) = \frac{1}{1+e^{10.958-3.770Neck_Tension}}$ Neck (N_{ij} and Tension/ Compression in kN) $P_{neck_Comp}(AIS3+) = \frac{1}{1 + e^{10.9745 - 2.375 Neck_Compression}}$ $P_{neck_Comp}(AIS3+) = \frac{1}{1 + e^{10.958 - 3.770 Neck_Compression}}$ Pneck = max imum(Pneck_Nij, Pneck_Tens, Pneck_Comp) Pneck = max imum(Pneck Nij, Pneck Tens, Pneck Comp) $P_{ioint} = 1 - (1-P_{head}) \times (1-P_{neck}) \times (1-P_{chest}) \times (1-P_{femur})$ Overall

Side Impact (MDB & Pole Test)

	ES-2re 50 %	SID-IIs 5 %		
Head (HIC ₃₆)	$P_{head}(AIS3+) = \Phi\left(\frac{\ln(HIC36) - 7.45231}{0.73998}\right)$ where Φ = cumulative normal distribution	$P_{head}(AIS 3+) = \Phi\left(\frac{\ln(HIC 36) - 7.45231}{0.73998}\right)$ where Φ = cumulative normal distribution		
Chest (Rib Deflection in mm)	$P_{chest}(AIS3+) = \frac{1}{1 + e^{5.3895 - 0.0919*\text{max. rib deflection}}}$			
Abdomen (Abdominal Force in N)	$P_{abdomen}(AIS3+) = \frac{1}{1+e^{6.04044-0.002133*F}}$ where F =total abdominal force (N) in ES-2re			
Pelvis (Force in N)	$P_{pelvis}(AIS3+) = \frac{1}{1 + e^{7.5969 - 0.0011*F}}$ where F is the public force in the ES-2re in Newtons	$p_{pelvis}(AIS2+) = \frac{1}{1 + e^{6.3055 - 0.00094 * F}}$ where F is the sum of acetabular and iliac force in the SID – IIs dummy in Newtons		
Overall	$P_{joint} = 1 - (1-P_{head}) \times (1-P_{chest}) \times (1-P_{abdomen}) \times (1-P_{pelvis})$	$P_{joint} = 1 - (1 - P_{head}) \times (1 - P_{pelvis})$		



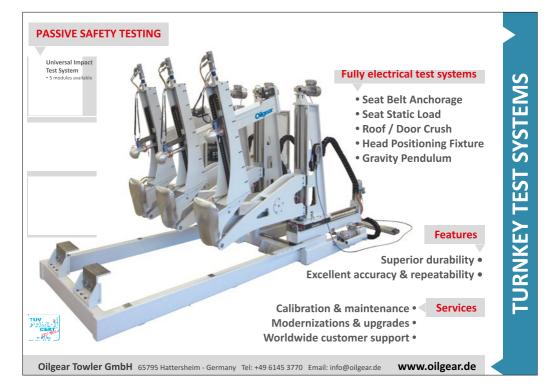


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U.S. NCAP: Rating Scheme

Frontal C	Frontal Crash Test		Side Pole Test Side M		Rollover Test			
Driver	Passenger	Front Seat	Front Seat	Rear Seat				
Injury Criteria								
▼ Probabilty of In- jury (Risk Curves) P _{joint}	Probabilty of Rollover P _{roll}							
RR*=P _{joint} /base**	RR*=P _{roll} /base**							
Driver Stars (50 %)	▼ Passenger Stars (50 %)	Stars Stars (20 %) (80 %) Front Seat Stars (50 %)		Rear Seat Stars (50 %)	Overall Rollover Star Rating			
	▼ al Star Rating (12)	▼ Verall Side Star Rating (4/12)			(3/12) Safety Wissen by Cartis.			
Vehicle Safety Score (VSS)								

*RR = relative risk; **base = baseline risk = 15 %

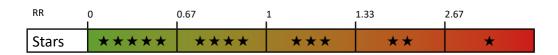
Rating procedure

Using the Injury Risk Curves on \bigcirc page 33 and page 34, the risk of a serious injury (AIS 3+) can be calculated from the injury criteria measured in the crash test. The joint risk for an occupant can be determined using the following formulae:

Frontal Impact: $P_{joint} = 1 - (1 - P_{head}) \times (1 - P_{neck}) \times (1 - P_{chest}) \times (1 - P_{femur})$

Side Impact: $P_{joint} = 1 - (1 - P_{head}) \times (1 - P_{chest}) \times (1 - P_{abdomen}) \times (1 - P_{pelvis})$

This risk is compared to a so called baseline risk which was set to 15 %. This ratio is called relative risk (RR) from which the star rating is determined using the following table:





UPDATE



IIHS Rating

Testing Protocol Version XVII (Nov 2016)

Rating Guidelines September 20	14
rating Guidennes September 20.	14

Dummy	Region	Criteria	Good	Acceptable	Marginal	Poor
Fronta	al Impa	ct with 40 % Overlap (@ 64 km/h			
		HIC ₁₅	≤ 560	≤ 700	≤840	>840
		N _{ij}	≤0.80	≤ 1.00	≤ 1.20	> 1.20
	Head & Neck	F _{z,tension} (kN)	≤ 2.6	≤ 3.3	≤ 4.0	> 4.0
C NCCK		Fz,compression (kN)	≤ 3.2	≤ 4.0	≤ 4.8	> 4.8
		ares peak (g)		Values > 70 resul		
		a _{3ms} (g)	≤ 60	≤ 75	≤ 90	> 90
	Charal	Deflection (mm)	≤ 50	≤ 60	≤ 75	> 75
H III 50 %	Chest	Deflection rate (m/s)	≤ 6.6	≤ 8.2	≤9.8	> 9.8
		VC (m/s)	≤ 0.8	≤ 1.0	≤ 1.2	> 1.2
		Femur Axial Force (kN) (Force duration corridors)	≤ 7.3 @ 0 ms ≤ 6.1 @ 10 ms	≤ 9.1 @ 0 ms ≤ 7.6 @ 10 ms	≤ 10.9 @ 0 ms ≤ 9.1 @ 10 ms	> 10.9 @ 0 ms > 9.1 @ 10 ms
	Legs &	Knee Displacement (mm)	≤ 12	≤ 15	≤ 18	> 18
	Feet	TI (upper, lower)	≤0.80	≤ 1.00	≤ 1.20	> 1.20
		Tibia Axial Force (kN)	≤ 4.0	≤ 6.0	≤ 8.0	> 8.0
		Foot acceleration (g)	≤ 150	≤ 200	≤260	> 260

Testing Protocol Version IV (Feb 2016)

Dummy	Region	Criteria	Good	Acceptable	Marginal	Poor	
Seat/Head Restraints: Static Assessment (🗢 page 85)							
	thead	Backset (mm)	≤ 70	≤ 90	≤110	> 110	
HRMD	HRMD Head & Neck	Distance from top of head (mm)	≤ 60	≤ 80	≤100	> 100	
Seat/Head Restraints: Dynamic Assessment							
BioRID	Head	Vector sum of the standardized shear (FX) and tension (FZ) values $(F_x / 315)^2 + ((F_z - 234) / 1131)^2$	< {0.450} ²	≤ {0.825}²	> {0.825}²		
llg	& Neck	Time to head restraint contact (ms)	for value	es > 70 ms the ratir	ng is reduced by o	ne level*	
		T1 acceleration (g)	for valu	ues > 9.5 the rating	g is reduced by on	e level*	
				* only if both exce	ed the given level		

The overall rating equals the static or dynamic rating. whichever is worse. Exceptions:

If the static rating is "acceptable" but the backset is sufficient for a "good" rating and the dynamic rating is "good" then the overall rating is also "good". If the static rating is "marginal" or "poor" no dynamic test is made and the overall rating is "poor".

SAFETY WISSEN	UPD	ATE			car	hs.
IIHS R	ating	ting Protocol Versio	n IX (Nov 2016)			
Dummy	Region	Criteria	Good	Acceptabl	e Marginal	Poor
Barrie	r Side	Impact (IIHS MDB) @ !	50 km/h			
		HIC ₁₅	≤ 623	≤ 779	≤ 935	> 935
	Head/ Neck	F _{z,tension} (kN)	≤ 2.1	≤ 2.5	≤ 2.9	> 2.9
		F _{z,compression} (kN)	≤ 2.5	≤ 3.0	≤ 3.5	> 3.5
		Shoulder deflection (mm)		Values > 60 re	esult in downgrading	
	Chest/ Torso	Ø Rib deflection (mm)	≤ 34	≤42	≤ 50	> 50
		Worst Rib deflection (mm)			51 - 55	> 55
		Deflection rate (m/s)	≤ 8.20	≤ 9.84	≤11.48	> 11.48
SID-IIs		VC (m/s)	≤ 1.00	≤ 1.20	≤ 1.40	> 1.40
5 %		Acetabulum force (kN)	≤ 4.0	≤ 4.8	≤ 5.6	> 5.6
		Ilium force (kN)	≤ 4.0	≤4.8	≤ 5.6	> 5.6
		Combined acetabulum and ilium force (kN)	≤ 5.1	≤ 6.1	≤7.1	> 7.1
	Pelvis/ Left	Femur A-P force (3 ms clip, kN)	≤ 2.8	≤ 3.4	≤ 3.9	> 3.9
	Femur	Femur L-M force (3 ms clip, kN)	≤ 2.8	≤ 3.4	≤ 3.9	> 3.9
		Femur A-P bending moment (3 ms clip, Nm)	≤254	≤ 305	≤356	> 356
		Femur L-M bending moment (3 ms clip, Nm)	≤254	≤ 305	≤356	> 356
Structure	2	Intrusion: B-pillar to driver seat centerline distance (mm)	≥125	≥ 50	≥0	<0

Testing Protocol Version III (July 2016)

Criteria	Good	Acceptable	Marginal	Poor
Roof Crush (⊃ page 56)				
Stiffness to weight ratio (SWR) F _{max} / m x g	≥ 4.00	≥ 3.25	≥ 2.50	< 2.5

IIHS TOP SAFETY *PICK* **IIHS TOP SAFETY** *PICK*+

Year	TSP Criteria	TSP+ Criteria
2017	 "Good" rating in all crash tests at least "advanced" rating in front crash prevention ⇒ Page 112 	 "Good" rating in all crash tests at least "advanced" rating in front crash prevention Page 112 at least "acceptable" rating for advanced headlights

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IIHS Rating: Small Overlap



Testing Protocol Version V (Nov 2016)

Rating Protocol Version IV (Nov 2014)

Dummy	Region	Criteria	Good	Acceptable	Marginal	Poor
Small	Overla	p Frontal Impact with	25 % Overla	p @ 64 km/	′h	
	int	lower hinge pillar (resultant)				
	artme	footrest (resultant)				
ل ا	Comp	left toepan (resultant)	≤ 150	≤ 225	≤ 300	> 300
ns (mr	cupant	brake pedal (resultant)				
ıtrusio	Lower Occupant Compartment	parking brake pedal (resultant)				
Structure Rating: Intrusions (mm) O	Γον	rocker panel (lateral)	≤ 50	≤ 100	≤ 150	> 150
ture Ra	th	steering column (longitutinal)	≤ 50	≤ 100	≤ 150	> 150
Struc ccupar tment	Jpper Occupant Compartment	upper hinge pillar (resultant)				
	oper O compai	upper dash (resultant)	≤ 75	≤ 125	≤175	> 175
	50	left instrument panel (resultant)				
		HIC ₁₅	≤ 560	≤ 700	≤ 840	> 840
	Head	N _{ij}	≤ 0.80	≤ 1.00	≤ 1.20	> 1.20
	& Neck Ø	F _{z,tension} (kN)	≤2.6	≤3.3	≤4.0	>4.0
		Fz,compression (kN)	≤ 3.2	≤4.0	≤4.8	> 4.8
		a3ms (g)	≤ 60	≤ 75	≤ 90	> 90
	Chest/	Deflection (mm)	≤ 50	≤ 60	≤ 75	> 75
H III 50 %	Torso	Deflection rate (m/s)	≤ 6.6	≤8.2	≤ 9.8	> 9.8
		VC (m/s)	≤ 0.8	≤ 1.0	≤1.2	> 1.2
	Femur	KTH Injury Risk (%)	≤5	≤15	≤25	> 25
		Knee Displacement (mm)	≤ 12	≤15	≤18	> 18
	Leg & Foot	TI (upper, lower)	≤ 0.80	≤ 1.00	≤ 1.20	> 1.20
	9	Tibia Axial Force (kN)	≤ 4.0	≤ 6.0	≤ 8.0	> 8.0
		Foot Acceleration (g)	≤ 150	≤ 200	≤ 260	> 260

carhs.



IIHS Rating: Small Overlap

Small Overlap Frontal Impact with 25 % Overlap @ 64 km/h

Restraints & Dummy Kinematics Rating	SafetyWissen by Carhs.
Rating system based on a demerit system	Demerits
Frontal Head Protection	
Partial frontal airbag interaction	1
Minimal frontal airbag interaction	2
Excessive lateral steering wheel movement (>100 mm)	1
Two or more head contacts with structure	1
Late deployment or non deployment of frontal airbag	automatic Poor
Lateral Head Protection	
Side head protection airbag deployment with limited forward coverage	1
No side head protection airbag deployment	2
Excessive head lateral movement	1
Front Chest Protection	
Excessive vertical steering wheel movement (>100 mm)	1
Excessive lateral steering wheel movement (>150 mm)	1
Occupant containment and miscellaneous	
Excessive occupant forward excursion (>250 mm)	1
Occupant burn risk	1
Seat instability	1
Seat attachment failure	automatic Poor
Vehicle door opening	automatic Poor
Restraints & Kinematics @ Good Acceptable Marginal	Poor

Restraints & Kinematics O	Good	Acceptable	Marginal	Poor
Sum of Demerits	≤1	≤3	≤ 5	> 5

Small Overlap Overall Rating

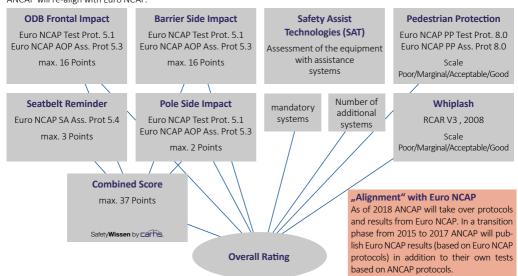
Rating system based on a demerit system. Demerits result from the injury, structure and restraints & kinematics ratings.

Component Rating	Good	Acceptable	Marginal	Poor			
Vehicle Structure Rating O	0	2	6	10			
Head/Neck Injury Rating 🛛	0	2	10	20			
Chest Injury Rating	0	2	10	20			
Thigh and Hip Injury Rating 4	0	2	6	10			
Leg and Foot Injury Rating 🖲	0	1	2	4			
Restraints / Kinematics Rating 🗿	0	2	6	10			
The overall rating depends on the sum of demerits: Safety Wissen by Caffred							
Overall Rating	Good	Acceptable	Marginal	Poor			
Sum of demerits	≤3	≤9	≤ 19	> 19			

Australasian NCAP (ANCAP)

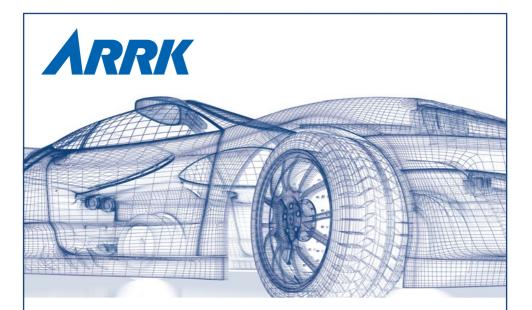
ANCAP was harmonized with Euro NCAP until 2009. The harmonization ended with the introduction of Euro NCAP's overall rating in 2009. ANCAP has now developed a new overall rating scheme that will be introduced in the period from 2011 -2017. As of 2018 ANCAP will re-align with Euro NCAP.

Roadmap Update 23. April 2014



Points required for the respective star rating	Frontal- and Barrier- Side-Impact each	Pole-Side-Impact	Combinied points	Pedestrian Protection	Whiplash	mandatory SAT			additional SAT (count)			
						ESC	3PSB	HPT	SBR	EBA	TT	
****	12.5	1	32.5	Acceptable	Good	•	•	● ²	● ¹⁺³	•	•	6
****	8.5	1	24.5	Acceptable	Good	•	•	● ²	● ¹⁺³	•	•	5
***	4.5	-	16.5	Acceptable	Acceptable	•	•	\bullet^1	\bullet^1	•	•	4
**	1.5	-	8.5	Marginal	Acceptable	•	•	\bullet^1	$ullet^1$		•	3
*	-	-	0.5	Marginal	Acceptable	•	•		$ullet^1$		•	2
¹ front (1 st row of se	eats)		ESC: Elect	tronic Stabilit	y Control			3PSB: 3-	Point Se	eat Belts		
$^{\rm 2}2^{\rm nd}rowofseats$			SBR: Seat Belt Reminder				EBA: Emergency Brake Assist					
$^{\scriptscriptstyle 3}$ fixed seats in 2^{nd} r	ow of seats	5	HPT: Head	d-protecting	technology - :	side airb	bags	TT: Top	Tether			

More details, including a list of additional SAT, are available in the "ANCAP RATING ROAD MAP 2011-2017" which can be downloaded from http://www.ancap.com.au/media or can be found on **SafetyWissen.com**



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- Passive safety concepts
- Robustness evaluation
- Material models
- Optimisation & form finding methods

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Latin NCAP Rating in Adult- and Child-Occupant Protection

Adult Occupant Protection

UPDATE

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Assessn	nent Pr	otoco	Versio	n 3.

	Require	d Score	Additional Requirements			
	Frontal ODB + Side MDB (max. 16+16=32 Pt.) ¹	Seat Belt Reminder SBR (max 2 Bt)	ABS	ESC acc. GTR 8	Pole-Side Impact acc. Euro NCAP Protocol 5.2	
Star Rating	(max. 16+16=32 Pt.) ²	(max. 2 Pt.)			Protocol 5.2	
*****	≥ 27	≥1		\checkmark	\checkmark	
****	≥ 22	≥1		~		
***	≥ 16	≥ 0.5	\checkmark			
**	≥ 10					
*	≥ 4				SafetyWissen by Carhs.	

¹ If the scores for frontal and side impact differ more than 35% the rating will be reduced by 1 star.

Child Occupant Protection (page 88)

Assessment	Protocol	Version 3.1

Star Rating	Required Score (out of max. 49 points)
****	≥ 41
****	≥ 35
***	≥ 27
**	≥ 18
*	≥ 9 Safety Wissen by carhs.

Frontal Impact with 40 % Overlap @ 64 km/h

	Head,	4	HlC15 < 500; a _{3ms} < 72 g M _{y,extension} < 42 Nm F _{z,tension} < 2.7 kN @ 0 ms / < 2.3 kN @ 35 ms / < 1.1 kN @ 60 ms F _{x,shear} < 1.9 kN @ 0 ms / < 1.2 kN @ 25 – 35 ms / < 1.1 kN @ 45 ms	
H III 50 % front	Neck	0	HlC15 > 700; a3ms > 88 g M _{y,extension} > 57 Nm F _{z,tension} > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms F _{x,shear} > 3.1 kN @ 0 ms / > 1.5 kN @ 25 – 35 ms / > 1.1 kN @ 45 ms	16 points
	Chest	4	Deflection < 22 mm; VC < 0.5 m/s	max.
	Chest	0	Deflection > 42 mm; VC > 1.0 m/s	E
	Femur,	4	Axial Force _{compr} < 3.8 kN; Knee Displacement < 6 mm	
	Knee	0	Axial Force _{compr} > 9.07 kN @ 0 ms / > 7.56 @ 10 ms; Knee Displacement > 15 mm	
	Tibia,	4	TI < 0.4, Axial Force _{compression} < 2 kN; x–Displacement Pedals < 100 mm	
	Foot	0	TI > 1.3, Axial Force _{compression} > 8 kN; x–Displacement Pedals > 200 mm	

Barrier Side Impact (MDB) @ 50 km/h

lload	Head	4	$HIC_{15} < 500; a_{3ms} < 72 g$	
	neau	0	HIC ₁₅ > 700; a _{3ms} > 88 g	
	Chest	4	Deflection < 22 mm; VC < 0.32 m/s	points
ES-2 front	Chest	0	Deflection > 42 mm; VC > 1.0 m/s	
	A la al a una a un	4	Force _{compression} < 1.0 kN	<. 16
	Abdomen	0	Force _{compression} > 2.5 kN	max.
	Pelvis	4	PSPF < 3.0 kN	
	Pelvis	0	PSPF > 6.0 kN	

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UPDATE Overall Assessment Protocol Version 1.0

SAFETY WISSEN

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ASEAN NCAP Overall Rating 2017

	Adult Occupa	nt Protection	Child Occupa	nt Protection	Safety	Assist	
	Offset Frontal Impact	16	Dynamic Assessment	Frontal 16	Effective Braking & Av	voidance 8	
	Side Impact (MDB)	16	Dynamic Assessment	Side 8	Seat Belt Reminder	6	
	Head Protection Tech	nology 4	CRS Installation		Blind Spot Technology	/ 2	
			Vehicle-based Assess	ment 13	Advanced SATs	2	
max. points (1)		36	⇒ Page 88	49	Page 110	18	
normalized score (2)	actual po	oints / (1)	actual po	oints / (1)	actual po	oints / (1)	
weighting (3)	50	%	25	%	25 %		Overall score (5)
weighted score (4)	(2)	(3)	(2)>	x(3)	(2)>	(3)	∑(4)
Rating	Balancing	: minimum norm	alized score (2) pe	er box required fo	r the respective s	tar rating:	min. overall score (5)
	score	points	score	points	score	points	Score
*****	75 %	27.00	75 %	36.75	60 %	10.80	75 %
****	65 %	23.40	60 %	29.40	40 %	7.20	65 %
***	45 %	16.20	30 %	14.70	30 %	5.40	50 %
**	30 %	10.80	25 %	12.25	20 %	3.60	40 %
*	20 %	7.20	15 %	7.35	10 %	1.80	30 %

Adult Occupant Protection

Dummy Region

AOP Assessment Protocol Version 1.0

Fronta	l Impact wi	th 40 %	6 Overlap @ 64 km/h	
Head, Neck	4	$ \begin{array}{l} HIC_{15} < 500; a_{3ms} < 72g \\ M_{y,extension} < 42Nm \\ F_{z,tension} < 2.7kN @ 0ms / < 2.3kN @ 35ms / < 1.1kN @ 60ms \\ F_{x,shear} < 1.9kN @ 0ms / < 1.2kN @ 25 - 35ms / < 1.1kN @ 45ms \end{array} $		
	0	HIC15 > 700; a _{3ms} > 88 g M _{y,extension} > 57 Nm F _{z,tension} > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms F _{x,shear} > 3.1 kN @ 0 ms / > 1.5 kN @ 25 – 35 ms / > 1.1 kN @ 45 ms	nts	
H III 50 %	H III 50% front Femur, Knee	4	Deflection < 22 mm; VC < 0.5 m/s	max. 16 points
front		0	Deflection > 42 mm; VC > 1.0 m/s	. 16
		4	Axial Force _{compression} < 3.8 kN Knee Displacement < 6 mm	max
Tibia	0	Axial Force _{compression} > 9.07 kN @ 0 ms / > 7.56 @ 10 ms Knee Displacement > 15 mm		
	4	TI < 0.4; Axial Force _{compression} < 2 kN Pedal rearward displacement <100 mm		
	Foot		TI > 1.3; Axial Force _{compression} > 8 kN Pedal rearward displacement > 200 mm	

Barrier Side Impact (MDB) @ 50 km/h

Points Criteria

Head	Lload	4	HIC ₃₆ < 650; a _{3ms} < 72 g	
	пеац	0	HIC ₃₆ > 1000; a _{3ms} > 88 g	
ES-2 Abdomen	Chast	4	Deflection < 22 mm; VC < 0.32 m/s	points
	Chest	0	Deflection > 42 mm; VC > 1.0 m/s	od g
	Abdomon	4	Force _{compression} < 1.0 kN	k. 16
	0	Force _{compression} > 2.5 kN	тах.	
	Pelvis	4	PSPF < 3.0 kN	
	PEIVIS	0	PSPF > 6.0 kN	

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Protocol 2015 [2018]

Values in brackets []: planned changes in 2018

Dummy	Region	Points	Criteria	
Fronta	l Impact wi	th 100	% Overlap @ 50 km/h ①	
Head	Hoad	5	HIC ₃₆ < 650; a _{3ms} < 72 g	
	пеац	0	HIC ₃₆ > 1000; a _{3ms} > 88 g	
	Neck	2	$\begin{array}{l} M_{y,extension} < 42 \ Nm \\ F_{z,tension} < 2.7 \ kN @ 0 \ ms \ / < 2.3 \ kN @ 35 \ ms \ / < 1.1 \ kN @ 60 \ ms \\ F_{x,shear} < 1.9 \ kN @ 0 \ ms \ / < 1.2 \ kN @ 25 - 35 \ ms \ / < 1.1 \ kN @ 45 \ ms \end{array}$	
H III 50 %	Neck	0	M _{y,extension} > 57 Nm F _{z,tension} > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms F _{x,shear} > 3.1 kN @ 0 ms / > 1.5 kN @ 25 – 35 ms / > 1.1 kN @ 45 ms	
front	Chest	5	Deflection < 22 mm; VC < 0.5 m/s	LS .
	Chest	0	Deflection > 50 mm; VC > 1.0 m/s	oin
	Femur Knee	2	Axial Force _{compression} < 3.8 kN; Knee Displacement < 6 mm	3 [20] p
		0	Axial Force _{compression} > 9.07 kN @ 0 ms / > 7.56 @ 10 ms; Knee Displacement > 15 mm	max. 18 [20] points
	Tibia	2	TI < 0,4; Axial Force _{compression} < 2 kN	
	ПЛА	0	TI > 1,3; Axial Force _{compression} > 8 kN	
	Head	0.8 [1.6]	HIC15 < 500	
	Tiead	0	HIC15 > 700	
H III 5 %	Neck	0.2 [0.4]	F _{x,shear} < 1200 N; F _{z,tension} < 1700 N; M _{y,extension} < 36 Nm	
rear	Neek	0	$F_{x,shear}$ > 1950 N; $F_{z,tension}$ > 2620 N; $M_{y,extension}$ > 49 Nm	
	Chest	1 [2]	Deflection < 23 mm	
	Chest	0	Deflection > 48 mm	

Frontal Impact with 40 % Overlap @ 64 km/h 2

Не Н III 50 %	Llood Nosk	4	HIC ₃₆ < 650, a_{3ms} < 72 g M _{y,extension} < 42 Nm F _{z,tension} < 2.7 kN @ 0 ms / < 2.3 kN @ 35 ms / < 1.1 kN @ 60 ms F _{x,shear} < 1.9 kN @ 0 ms / < 1.2 kN @ 25 – 35 ms / < 1.1 kN @ 45 ms		
	Head, Neck	0	HIC36 > 1000, a _{3ms} > 88 g M _{y,extension} > 57 Nm F _{z,tension} > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms F _{x,shear} > 3.1 kN @ 0 ms / > 1.5 kN @ 25 – 35 ms / > 1.1 kN @ 45 ms	its	
front	front Chest	4	Deflection < 22 mm; VC < 0.5 m/s	[20] points	
Chi	Chest	0	Deflection > 50 mm; VC < 1.0 m/s	20]	
	Femur	4	Axial Force _{compression} < 3.8 kN, Knee Displacement < 6 mm	18 [
	Knee	0	Axial Force _{compression} > 9.07 kN @ 0 ms / > 7.56 @ 10 ms, Knee Displacement > 15 mm	тах.	
	Tibia	4	TI < 0.4; Axial Force _{compression} < 2 kN		
TIDIa	0	TI > 1.3; Axial Force _{compression} > 8 kN			
	Head, Neck	1 [2]	$HIC_{15} < 500$, $F_{x,shear} < 1200$ N, $F_{z,tension} < 1700$ N, $M_{y,extension} < 36$ Nm		
H III 5 %	Head, NECK	0	$HIC_{15} > 700$, $F_{x,shear} > 1950$ N, $F_{z,tension} > 2620$ N, $M_{y,extension} > 49$ Nm		
rear	Chart	1 [2]	Deflection < 23 mm		
(Chest	0	Deflection > 48 mm		

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Verification and Validation of ADAS and Safety Systems



Validation of ADAS and Automated Drive Systems

Integrated Safety System Assessment

Human Systems Integration

Virtual - Hybrid - Real Testing



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	UP

DATE

China NCAP

Dummy	Region	Points	Criteria	Values in brackets []: planned changes in 2	2018
Barrie	r Side Impa	ct ([AE]	MDB) @ 50 km/h 3		
	Head	4	HIC ₃₆ < 650 [HIC ₁₅ < 500]; a _{3ms} < 72 g		
	пеац	0	HIC ₃₆ > 1000 [HIC ₁₅ > 700]; a _{3ms} > 88	[80]g	
ES-2	Chest	4	Deflection < 22[28] mm; VC < 0.32[-] m/	/s	
front	Chest	0	Deflection > 42 [50] mm; VC > 1.0 m/s; [[Shoulder Lateral Force > 3.0 kN]	
	[WS 50] Abdomen Pelvis	4	Axial Force _{compression} < 1.0 kN; [Deflect	ion <47 mm]	
[005 50]		0	Axial Force _{compression} > 2.5 kN; [Deflect	ion > 65 mm; VC > 1.0 m/s]]	nts
		4	PSPF < 3.0 [1.7] kN		[20] points
		0	PSPF > 6.0 [2.8] kN		20]
	Head	1	HIC ₁₅ < 500		18[
	пеац	0	HIC ₁₅ > 700		max. 1
	[chard]	[1]	[Deflection < 31 mm]		Ĕ
SID-IIs	[Chest]	0	[Deflection > 41 mm; VC > 1.0 m/s]		
rear	[4	[1]	[Deflection < 38 mm]		
	[Abdomen]	0	[Deflection > 48 mm; VC > 1.0 m/s]		
	Dolvic	1	Force < 3500 N		
	Pelvis		Force > 5500 N		

Protocol 2015 [2018]

Whiplash Test @ v = 15.65 [20.0<u>0] km/h</u> ④

	NIC	2	< 8 m²/s²	
	NIC	0	> 30 m²/s²	
BioRID II	Upper Neck	1 [1.5]	F _{x+} <340 N, F _{z+} < 475 N, M _y < 12 Nm	
BIORID II	Opper Neck	0	F _{x+} > 730 N, F _{z+} > 1130 N, M _y > 40 Nm	ts
	Lower Neck	1 [1.5]	F _{x+} <340 N, F _{z+} < 257 N, M _y < 12 Nm	points
	LOWEI NECK	0	F _{x+} > 730 N, F _{z+} > 1480 N, M _y > 40 Nm	[5] p
	max. dyn. seatback defl.	-2	> 19° [25.5°]	max.4 [
	dyn. seat displacement	-4[-5]	> 20 mm	3
	HRMD interference	-2	Y/N	

Additional Points 5

	1	Visual / Audio Signal with occupant detection	
SBR Passenger	0.5	Visual / Audio Signal without occupant detection	[5] pt.
[SBR 2 nd row]	1	[Status indicator for each 2 nd row seat]	3
Side Protection	1 [3]	Side / Curtain-Airbag	лах.
ESC	1 [-1]	acc. GTR 8 or FMVSS 126 or UN R13H (R140) 🗢 page 114	2

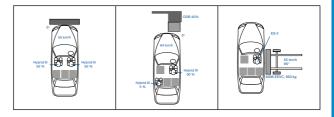
Overall Rating	2017	2018 (Weighting: Occupant Protection 70%,Pedestrian Protection + Active Safety 15% each)					
Stars	Total Points	Total score	Balancing				
	1+2+8+4+5		Occupant Prot.	Pedestrian Prot.	Active Safety		
★★★★★ ☆	≥ 60	90 %	95 %	75 %	50/55 ² /72 ³ %		
$\star \star \star \star \star$	≥ 54 < 60	82 %	85 %	65 %	26/38 ² /55 ³ %		
$\star \star \star \star$	≥ 48 < 54	72 %	75 %	50 %	26/26 ² /26 ³ %		
$\star \star \star$	≥ 36 < 48	60 %	65 %	40 %			
**	≥ 24 < 36	45 %	55 %	20 %			
*	< 24	< 45 %	< 55 %	< 20 %			

 1 As of 2018 ESC will be rated as part of the active safety category. 2 as of 2019 $^{-3}$ as of 2020





JNCAP



Dummy	Region	Weight	Points	Criteria										
Fronta	al Impact	t												
	Used	0.022	4 HIC ₃₆ < 650											
	Head	0.923	0	HIC ₃₆ > 1000	IIC ₃₆ > 1000									
	Neck	0.231	4	M _{y,extension} < 42 Nm F _{z,tension} < 2.7 kN @ 0 ms / < 2.3 kN @ F _{x,shear} < 1.9 kN @ 0 ms / < 1.2 kN @ 2				eighting)						
H III 50 %	Neck	0.231	0	M _{y,extension} > 57 Nm F _{z,tension} > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms F _{x,shear} > 3.1 kN @ 0 ms / > 1.5 kN @ 25 – 35 ms / > 1.1 kN @ 45 ms				12 points (after weighting)						
front	Chest 0.923		4	Deflection < 22 mm				oints						
	chest	0.925	0	Deflection > 42 mm; a _{3ms} > 60 g	Rating Scheme Frontal &			L2 p(
1	Femur	0.923	2	Axial Force _{compression} < 7 kN	Side	Side Impact, Whiplash:		max. 1						
	. cindi		0	Axial Force _{compression} > 10 kN		Level	Required Points	E						
	Tibia	0.923	2	TI < 0.4			Points							
		01020	0	TI > 1.3	5		≥ 10.5							
	Head	0.8	4	HIC ₁₅ < 500										
	neuu	0.0	0	HIC ₁₅ > 700	4		≥9	ing)						
	Nock	Nock	Nock	Neck	0.2	0.2	0.2	0.2	4	$\label{eq:Fx,shear} \begin{split} F_{x,shear} &< 1200 \text{ N}; F_{z,tension} < 1700 \text{ N}; \\ M_{y,extension} &< 36 \text{ Nm} \end{split}$			> 7.5	veight
H III 5 %	NECK	0.2	0	$\label{eq:Fx,shear} \begin{split} F_{x,shear} &> 1950 \text{ N}; F_{z,tension} > 2620 \text{ N}; \\ M_{y,extension} &> 49 \text{ Nm} \end{split}$	3		27.5	points (after weighting)						
rear			0.0	4	Deflection < 23 mm	2		≥6	nts					
	Chest	0.8	0	Deflection > 48 mm				i poi						
	Abdomen	0.8	4	4 points awarded by default	1		< 6	nax. 12						
	Femur	0.4	4	Axial Force _{compression} < 4.8 kN				ma						
	remur	0.4	0	Axial Force _{compression} > 6.8 kN		:	SafetyWissen by Carhs	i						

Side I	Side Impact							
	Head	1.0	4	HIC ₃₆ < 650	g)			
ES-2	пеай	1.0	0	HIC ₃₆ > 1000	weighting)			
	Chest	1.0	4	Deflection < 22 mm	weig			
			0	Deflection > 42 mm	(after v			
front	Abdomen	men 0.5	4	Force _{compression} < 1.0 kN				
	Abuomen		0	Force _{compression} > 2.5 kN	12 pt.			
	Pelvis	0.5	4	PSPF < 3.0 kN	max. 1			
	Peivis	vis 0.5	0	PSPF > 6.0 kN SafetyWissen by Carfis	E			

49





JNCAP

Dummy	Criteria		Weight	Points	Limits	
Whipl	ash Test					
	NIC		1	4	< 8 m²/s²	
	NIC		I	0	> 30 m²/s²	
	Upper Neck F _{x+}	~		4	< 340 N	
	obbei Meck i Xt	inior		0	> 730 N	
	Upper Neck F _{z+}	crite		4	< 475 N	Jg)
	Opper Neck Fz+	2n		0	> 1130 N	points (after weighting)
	Upper Neck My Flexion	i i i		4	< 12 Nm	
	opper neek my riexion	ors		0	> 40 Nm	
BioRID II	Upper Neck My Extension			4	< 12 Nm	(aft
BIOTRID II	opper neek my extension	n th	2	0	> 40 Nm	lts
	Lower Neck F _{x+}	ed c	-	4	< 340 N	poi
		bas		0	> 730 N	12
	Lower Neck F ₇₊	ted		4	< 257 N	max.
	201121 112011 124	cula		0	> 1480 N	E
	Lower Neck My Flexion	al		4	< 12 Nm	
	Lotter recently riexion	score is calculated based on the worst injury criterion		0	> 40 Nm	
	Lower Neck My Extension			4	< 12 Nm	
	Extension	S		0	> 40 Nm	

Where a value falls between the upper and lower limit, the score is calculated by linear interpolation (sliding scale).

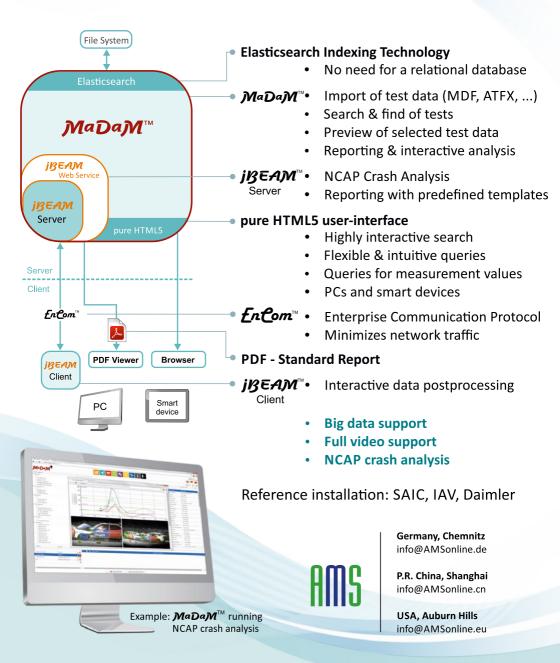
Overall Rating

	max. score	weight	max. weighted score	total	total
Occupant Protectio		weight	30010	total	totai
Full-width Frontal					
Driver	12	1.250	15		
Passenger	12	1.250	15		
Offset Frontal					
Driver	12	1.250	15		
Passenger (rear)	12	1.250	15	100	208
Side Impact				100	200
Driver	12	1.042	12.5		
Passenger ¹	12	1.042	12.5		
Whiplash					★★★≥130 ★★≥110
Driver	12	0.625	7.5		★<110
Passenger	12	0.625	7.5		
Pedestrian Protection	on (⊃ page 80)				
Head Impact	4	20	80	100	
Leg Impact	4	5	20	100	
Seat Belt Reminder					
Front	50	0.08	4	8	Safety Wissen by carhs.
Rear	50	0.08	4	5	carety model by CBITIS.

¹ For the passenger the same score as for the driver is assumed.

² Downgrade to 4 stars, unless at level 4 is reached for occupant protection and pedestrian head impact and level 3 is reached in pedestrian leg impact.

MaDaM[™] - the Genuine Web Solution by



_							
AFETY WISSEN	UPDATE				Ca	irt	.
KNCAF			Protocol 2017		e)	NC	AP
Category	Impact Safety		Pedestrian Safety		Driving Safety	w Car Assessme	nt Program
	Full Width Frontal	16	Head Impact	24	Rollover	5	
	Offset Deformable Barrier	16	Leg Impact	6	Braking	5	
	Barrier Side Impact	16			Basic Active Devices:		
	Child Protection	8			FCWS	0.5	
	Whiplash	4			LDWS	0.5	
	Pole Side Impact (optional ¹)	(2)			SLD	0.5	
					SBR front	0.5	
					SBR rear	0.5	
					AEB Inter-Urban	1	
					AEB City	1.5	
max. total points (1)	60 points		30 points		15 points		
normalized score (2)	actual points / (1)		actual points / (1)		actual points / (1)	
weighting (3)	60 %		25 %		15 %		
weighted score (4)	(2) × (3)		(2) × (3)		(2) x (3)		Overall score (6
	Additional Active Devices: (optic Advanced Airbag (1) - Max. tot				S (0.5); ISA (0.5); AEB Pedsti	rian (1);	Σ (4)+(5) max. 100
Overall classi	fication: Minimum normalized	scores	s (2) and total score (6) per ratin	g class			
1 st Grade	≥ 90.1 %		≥ 60.1 %		-		≥ 86.1 %

1 st Grade	≥90.1%	≥ 60.1 %	-	≥ 86.1 %
2 nd Grade	≥83.1%	≥ 50.1 %	-	≥ 81.1 %
3 rd Grade	≥ 76.1 %	≥ 40.1 %	-	≥ 76.1 %
4 th Grade	≥ 69.1 %	≥ 35.1 %	-	≥ 71.1 %
5 th Grade	≤ 69.0 %	≤ 35.0 %	-	≤ 71.0 %

Star rating per category: Minimum normalized scores (2) for the respective star rating

Category	Impact Safety	Pedestrian Safety	Driving Safety
*****	≥ 93.1 %	≥ 83.1 %	≥ 84.8 %
****	≥ 90.1 %	≥ 63.1 %	≥ 70.5 %
***	≥87.1%	≥ 43.1 %	≥ 55.4 %
**	≥ 84.1 %	≥ 23.1 %	≥ 40.3 %
*	≤ 84.0 %	≤ 23.0 %	≤ 40.2 %

¹ Optional items can be assessed upon the manufacturers request. The maximum total points remains the same.



UPDATE

SAFETY WISSEN

KNCA	Ρ			Protocol 2017	
Dummy	Region	Points	Criteria		
Frontal	Impact with 4	40 % Ov	erlap @ 64 km/h		
	Head, Neck	4	HIC ₃₆ < 650; M _{y,extension} < 42 Nm; F _{z,te}	ension < 2.7 kN; F _{x,shear} < 1.9 kN	
	neau, Neck	0	HIC36 > 1000; My, extension > 57 Nm; Fz,	tension > 3.3 kN; Fx,shear > 3.1 kN	
	Chest	4	Deflection < 22 mm; VC < 0.5 m/s		
	Chest	0	Deflection > 50 mm; VC > 1.0 m/s		
H III 50 %	Femur	4	Axial Force _{compr} < 3.8 kN; Knee displace	ment < 6 mm	
	Knee	0	Axial Force _{compr} > 9.07 kN; Knee displac	ement > 15 mm	ts
		4	TI < 0.4; Axial Force _{compr} < 2 kN		max. 16 points
	Tibia	0	TI > 1.3; Axial Force _{compr} > 8 kN		6 D
		01	steering wheel upward displacement 72	88 mm (from head score)	×.1
		01	steering wheel rearward displacement 9	0110 mm (from head score)	ma
	01 A-pillar rearward displacement 100200 mm (from chest score)				
Modifiers		-1	door latch or hinge failure (from chest so		
		01	pedal upward displacement 7288 mm		
		01	pedal rearward displacement 100200	mm (from tibla score)	
		- <u>1</u> -1	door opening during impact fuel leakage		
		-1	Tuerreakage		
Frontal	Impact with 1	LOO % O	verlap @ 56 km/h		
	Head, Neck	6	HIC ₁₅ < 500, F _{x,shear} < 1.2 kN, F _{z,tension} <	1.7 kN, My,extension < 36 Nm	
	neau, Neck	0	HIC ₁₅ > 700, Fx,shear > 1.95 kN, Fz,tension	> 2.62 kN, My,extension > 49 Nm	S
	Chast	6	Deflection < 22 mm		oint
H III 5 %	Chest	0	Deflection > 48 mm		a g
	F	4	Axial Force _{compr} < 3.8 kN		E E
	Femur	0	Axial Force _{compr} > 6.8 kN		max. 16 points
		_1	door oponing during impact		<u>د</u>

Modifiers

-1 fuel leakage

Barrier Side Impact (IVIDB) @ 55 km/n							
	Head	4	HIC ₁₅ < 500; a _{3ms} < 72 g				
	пеац	0	HIC ₁₅ > 700; a _{3ms} > 80 g				
	Chest	4	Deflection < 28 mm;	points			
	Chest	0	Deflection > 50 mm; VC \ge 1.0 m/s; Shoulder Force _{Lateral} \ge 3.0 kN	poi			
VV3 J070	Abdomen	4	Deflection < 47 mm;	16			
		0	Deflection > 65 mm; VC \ge 1.0 m/s	max.			
	Pelvis	4	PSPF < 1.7 kN	E			
PEIVIS	PEIVIS	0	PSPF > 2.8 kN				
Modifiers -1		-1	door opening during impact				

door opening during impact

Pole Side Impact @ 32 km/h

WS 50%	Head	2	HIC ₁₅ < 500	2
VV3 50%	пеац	0	HIC ₁₅ > 700	

Whipla	sh Test				
Dynamic	Assessment	1.5 Points	0 Points		-
	NIC	11.00	24.00		0 4)
	Nkm	0.15	0.55	Its	d to
BioRID	Rebound velocity (m/s)	3.2	4.8	points	(scaled to
	Upper Neck Fx, shear (N)	30	190	9 0	(sc
llg	Upper Neck Fz,tension (N)	360	750	тах.	Its
	T1 acceleration* (g)	9.30	13.10	Ê	oir
	T-HRC* (ms)	57	82		10 points
Geometr	y Assessment	1 Point	-1 Point		
HRMD	Backset (mm)	40	100	max. 1 pt	max.
ILVID	Height (mm)	0	80	μ	_

* Only the maximum score from either T1 acceleration or head restraint contact time is used in the rating.







BNVSAP Bharat New Vehicle Safety Assessment Program (India)

Time schedule

Phase I

- starting October 2016: Manufacturers can have their vehicles assessed on a voluntary basis
- starting October 2017: BNVSAP selects vehicles to be assessed
- Phase II starting October 2020: Extension of the tests: ODB 64 km/h, FW 50 km/h, Rear Impact 35 km/h, Whiplash
- Phase III starting October 2022: adapatation of the rating based on accident data

Phase I Assessment scheme

Category	Test / Requirement	Max. points available for meeting relevant legal (AIS) requirements	Max. points available for meet- ing BNVSAP criteria	Max. total points	
Adult Occupant	ODB Frontal Test 40 % / 56 km/h (AIS 098 / UN R94)	4	12	16	
Protection	MDB Side Test 50 km/h (AIS 099 / UN R95)	4	4	8	
Child Occupant Protection	Dynamic Assessment in ODB Frontal Test	-	4	4	
Pedestrian Protection	Head Impact (AIS 100)	4	-	4	
	Rear Impact (AIS 101 / UN R34)		2		
	Type approved ABS System		2		
	Seat Belt Reminder (SBR) Driver 1 point, Passenger 1 point		2		
Other Requirements	Validated Electronic Stability Control (ESC)	-	1	max. 8	
Requirements	Validated Electronic Brake Distribution (EBD)		1		
	Type approved head restraint system (for all forward facing outboard seats)		1		
	Child lock functionality check		1		
Total max.				40	

	Overall	Rating	Adult Occupa	Adult Occupant Protection			
Rating	required points (out of max. 40)	% of max	required points (out of max. 24)	% of max			
****	34	85	21	87.5			
****	28	70	17	70.8			
***	22	55	12	50			
**	16	40	8	20			
*	12	30	4	10			

Note: BNVSAP is still in its introduction phase. Therefore modifications may still occur.

Product Liability in the Automobile Industry

Course Description

carhs

In the framework of the ongoing extension of active and passive safety systems automobiles are becoming increasingly complex.

In this context the faultlessness of systems becomes more and more important, as with growing complexity not only the number but also the severity of possible faults is increasing. An indicator for this is the growing number of recalls in recent years.

Each manufacturer holds the responsibility for consequential damages caused by its products when used as intended. This responsibility is defined by law in all countries and has civil and criminal penalties.

Examples include the recalls of large numbers of vehicles that several OEMs were obliged to do during the last few years.

Obviously a safety related recall of a mass product may have severe or even existence-threatening consequences.

Consequently, manufacturers must ensure faultlessness throughout their organization.

Course Objectives

The aim of this course is to convey the importance of product liability for businesses and employees as well as an understanding of preventive measures.

Note: Product liability is not limited to passive safety. Therefore this course is also suitable for developers of active safety systems and driver assistance systems.

Who should attend?

The seminar is aimed at all decision-makers in the automotive development, who want to learn about the consequences of product liability and want to learn about preventive measures.

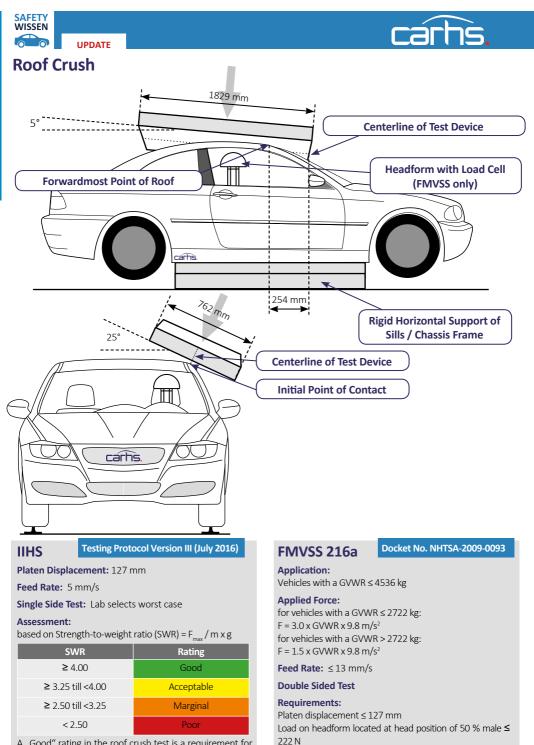
Course Contents

- Fundamentals of Product Liability
- Civil and criminal responsibility of the company and personal liability of employees
- Liability for Defects
- Product liability in Europe and in the U.S.
- U.S. TREAD ACT, Reporting obligation for OEMs and suppliers
- Product liability and advertisement and public relations of companies
- Quality management and its relevance from a product liability point of view
- Product liability in the supply chain
- Instructions, warnings
- Risk minimization within the organization, prevention
- Documentation, conclusive evidence
- Insurance of product liability risk
- Recall decision and processing



Hans-Georg Lohrmann was Manager of Reliability & Conformity of Production at ZF TRW Automotive GmbH. He has many years of experience in the field of safety, reliability and product liability in the automotive sector. Since September 2015 he has retired and is still active as a freelance consultant. He specializes in the area of restraint systems for vehicle occupant protection and supports his clients in the areas of reliability, safety planning and methods of verification, application and development of a product conformity certificate system and litigation support.

es	DATE	COURSE ID	VENUE	DURATION	I PRICE	LANGUAGE
Venu	0607.02.2017	2911	Alzenau	2 Days	1.290,- EUR till 09.01.2017, thereafter 1.540,- EUR	
es &	2324.05.2017	2913	Alzenau	2 Days	1.290,- EUR till 25.04.2017, thereafter 1.540,- EUR	
Dat	1617.10.2017	2912	Alzenau	2 Days	1.290,- EUR till 18.09.2017, thereafter 1.540,- EUR	



A "Good" rating in the roof crush test is a requirement for the Top-SafetyPick award.



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accelerated safety simulation



info@cfm-schiller.de www.cfm-schiller.de



Crashworthy Car Body Design - Design, Simulation, Optimization

Course Description

In the development of a car body different - sometimes conflicting - design requirements have to be met. Fulfilling crash regulations is a key task. Therefore it is mandatory that designers have a good understanding of the crash behavior of mechanical structures. The combination of knowledge about mechanics and the ability to use modern design tools allows for an efficient development process without unnecessary design iterations. The objective of the seminar is to present new methods for crashworthy car body design.

At the beginning of the course the mechanical phenomena of crash events will be discussed. Subsequently modern development methods (CAD design and crash simulation) will be treated. Thereafter modern implementations of safety design measures will be presented. Mathematical optimization of structural design - which is increasingly used in industry - will be covered at the end of the course.

Who should attend?

This 2 day course addresses designers, test and simulation engineers as well as project leaders and managers working in car body development and analysis.

Course Contents

- Mechanics of crash events
 - Accelerations during collisions
 - Structural loading during collisions
 - Examination of real crash events
 - Stability problems
 - Plasticity
- Design methods
 - Functional based design
 - Car body design
 - CAE conform design
- Crash simulation
 - Finite Element modelling of a car body
 - Finite Element analysis with explicit methods
 - Possibilities and limitations
 - Technical implementation of safety measures
 - Energy absorbing members
 - Car bodies
 - Safety systems
 - Pedestrian protection
 - Post crash
- Use of mathematical optimization procedures in real world applications
 - Approximation techniques
 - Optimization software & strategies
 - Shape and topology optimization



Prof. Dr.-Ing. Axel Schumacher (University of Wuppertal) studied mechanical engineering at the universities of Duisburg and Aachen. He received his doctorate on structural optimization from the university of Siegen. Following research projects for Airbus were focused on the optimization of aircraft structures. Thereafter he worked in the CAE methods development department of Adam Opel AG as project leader for structural optimization. From 2003 - 2012 he was a professor at the University of Applied Sciences in Hamburg and taught structural design, passive safety and structural optimization. Since 2012 he has been professor at the University of Wuppertal, where he holds the chair for optimization of mechanical structures.

es	DATE	COURSE ID	VENUE	DURATION	I PRICE	LANGUAGE
Venu	1617.03.2017	2919	Alzenau	2 Days	1.290,- EUR till 16.02.2017, thereafter 1.540,- EUR	
es &	2930.05.2017	2920	Alzenau	2 Days	1.290,- EUR till 01.05.2017, thereafter 1.540,- EUR	
Dat	1112.09.2017	2937	Tappenbeck	2 Days	1.290,- EUR till 14.08.2017, thereafter 1.540,- EUR	

nstructor





New test track

- Vehicle dynamics analyses
- Noise measurements
- Brake tests
- Analysis of driver assistance systems
- Testing of Emergency Brake Assist systems (EBA)

Crash test facilities

- Static and dynamic component tests
- Pedestrian protection tests
- Sled tests
- Full vehicle crash tests

Test facilities

- Operational stability analyses
- Endurance tests
- Vibration and oscillation analyses
- 3D laser scanning

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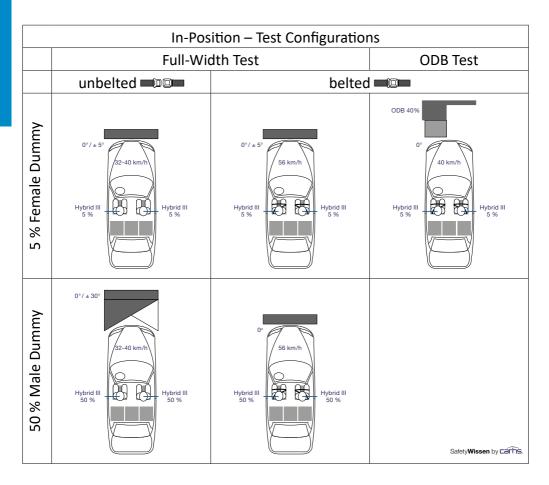








FMVSS 208: Frontal Impact Requirements: In-Position



FMVSS 208: Frontal Impact Requirements: Out of Position

Front seat	Dummy	Test configuration
Driver side	Hybrid III 5 % female	chin on airbag module in steering wheel chin on top of steering wheel
	CRABI 12m	in 23 defined CRS / positions
Passenger side	Hybrid III 3 y/o	chest on instrument panel head on instrument panel
	Hybrid III 6 y/o	chest on instrument panel head on instrument panel



Development of Frontal Restraint Systems meeting Legal and Consumer Protection Requirements

Course Description

Belts, belt-load limiters, airbags, steering column, knee bolster, seat... - only if all the components of a frontal restraint system are in perfect harmony it is possible to meet the different legal limit values as well as the requirements of consumer tests. However, these requirements, e.g. FMVSS 208, U.S. NCAP, Euro NCAP et al. are manifold and extensive, partly contradict each other, or the requirements superpose each other. Therefore it is a challenge for every development engineer to develop a restraint system by a clear, strategic procedure; time-saving and target-oriented with an optimal result.

In this 2-day seminar this strategic way of development will be shown. You will learn a procedure how to ideally solve the complex development task of a typical frontal restraintsystem design within the scope of the available tools test and simulation. Especially the importance and the influence of individual system components (e.g. belt-load limiters) for the accomplishment of development-sub tasks (e.g. minimum chest deflection) will be covered. In addition the influence of the airbag module design on the hazards of Out-of-Position (OoP) situations is going to be discussed, and a possible development-path for the compliance with the OoP requirements according to the FMVSS 208 legislation will be shown. The possibilities and limits of the development tools test and simulation will be discussed and communicated. Last but not least tips and tricks for a successful overall system design will be part of this seminar.

In this seminar you will become familiar with a procedure for the successful development of a frontal restraint system. Furthermore you will learn which development tool, simulation or test, is best suited for the respective sub task. Moreover you will be made aware of the influence of the individual components of a restraint system (belts, belt-load limiters, airbags, steering column, knee bolster, seat,...) on the efficiency of the entire system.

Finally future topics such as the compatibility of vehicles as well as pre-crash preparation and prevention of accidents are integrated into the seminar.

Who should attend?

The seminar addresses simulation and test engineers, project engineers and project managers as well as the heads of development departments in the field of passive safety who work on the design of restraint-systems for vehicles.

Course Contents

- Identification of the relevant development load cases
- Procedures for the development of a restraint system
- Influence and importance of individual system components on the overall performance
- Development strategy for UN regulations and NAR restraint systems
- Development path for the conformance to the OoP requirements according to FMVSS 208

Instructor



Kai Golowko (Bertrandt Ingenieurbüro GmbH) has been working in the area of vehicle safety since 1999. He started his career as a test engineer for passive safety at ACTS. Since 2003 he has been working as senior engineer for occupant safety and pedestrian protection. Since 2005 he has managed the department vehicle safety at Bertrandt in Gaimersheim. In this position he is responsible for component development and validation and integrated safety.

es	DATE	COURSE ID	VENUE	DURATION	I PRICE	LANGUAGE
Venu	1516.02.2017	2939	Gaimersheim	2 Days	1.290,- EUR till 18.01.2017, thereafter 1.540,- EUR	
ates &	1011.07.2017	2901	Alzenau	2 Days	1.290,- EUR till 12.06.2017, thereafter 1.540,- EUR	
Dat	1516.11.2017	2940	Tappenbeck	2 Days	1.290,- EUR till 18.10.2017, thereafter 1.540,- EUR	







Protection Criteria for Frontal Impact Tests

Configuration Criterion	Criterion		Rigi	Rigid Barrier In-Position			Deformable Barrier	Barrier		Out of Position	osition	
		CMVSS 208 (old),	EWIVSS 208	806 8			UN R94,	FMVSS 208		EWIVSS 208	806 5	
Requirements		ADR 69/00,		5 200	UN R137	8137	ADR 73/00,				C 100	
		FMVSS 208 (old)		3 200			FMVSS 208 (old) CIVIV 33 200				0 2 00	
Dummy		Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	CRABI
Size		50 % male	50 % male	5 % female	50 % male	5 % female	50 % male	5 % female	5 % female	6 year	3 year	1 year
	HIC ₃₆ /HPC ₃₆ [-]	1000 (FMVSS. ADR)			1000	1000	1000					
Head	HIC15 [-]	700 (CMVSS)	700	700				700	700	700	570	390
	a _{3ms} [g]				80	08	80					
	N _{ij} [-] (4 Values)		1.0	1.0				1.0	1.0	1.0	1.0	1.0
	F _{x,shea} r [kN]				3.1	2.7	3.1 @ 0 ms 1.5 @ 25-35 ms 1.1 @ ≥ 45 ms					
Neck	F _{z,tension} [kN]		4.17	2.62	3.3	2.9	3.3 @ 0 ms 2.9 @ 35 ms 1.1 @ ≥ 60 ms	2.62	2.07	1.49	1.13	0.78
	F _{z,compr.} [kN]		4.0	2.52				2.52	2.52	1.82	1.38	0.96
	M _y [Nm]				57	57	57					
	a _{3ms} [g]	60	60	60				60	60	60	55	50
Chest	Deflection [mm]	76.2 (FMVSS. ADR) 50 (CMVSS)	63	52	42	42 [34] ¹	50 [42] ³	52	52	40	34	30 ²
	VC [m/s]				1.0	1.0	1.0					
Femur	Axial Force [kN]	10	10	6.805	9.07	7	9.07 @ 0 ms 7.58 @ > 10 ms	6.805	6.8			
Knee	Displacement [mm]						15					
TF 55	π[-]						1.3 (4 Values)				Defet Miles	
	Axial Force _{compr.} [kN]						8.0				Salety WISSEIL by Coll 113	oy car is.
¹ planned tightening of requirements ² currently no measurement possible ³ as from 1 September 2018	planned tightening of requirements as of 2020 ^a currently no measurement possible ³ as from 1 September 2018	020										

carhs

Frontal Impact Protection Criteria Compared

Regulation	Crash	ATD								~
Criterion	Туре	[UoM]						Safe	ety Wissen by	carhs.
HIC ₁₅		[-]	300	400	500	600	700	800	900	1000
FMVSS 208	FWRB/ODB	HIII 5/50								
FMVSS 208	OOP	HIII 5								
FMVSS 208	OOP	HIII 6y/o								
FMVSS 208	OOP	HIII 3y/o								
FMVSS 208	OOP	CRABI 12m								
Euro NCAP ¹	ODB/FWRB	HIII 5/50					<u>N</u>			
C-NCAP	ODB/FWRB	HIII 5				//////////////////////////////////////	N			
JNCAP	ODB	HIII 5				MIIIIIN				
IIHS	ODB/SOB	HIII 50								
HIC ₃₆		[-]	300	400	500	600	700	800	900	1000
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 5/50								
C-NCAP	ODB/FWRB	HIII 50				////	//////////////////////////////////////	WWWWW	MUUUU	\mathbb{N}
JNCAP	ODB/FWRB	HIII 50					<u> </u>	(#111111)	MIIIII	
Head a _{3ms}		[g]	60	65	70	75	80	85	90	95
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 5/50								
Euro NCAP ¹	ODB/FWRB	HIII 5/50					N			
C-NCAP	ODB/FWRB	HIII 50				N///////	<u> </u>	/////////		
Chest Comp	pression	[mm]	10	20	30	40	50	60	70	80
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 5/50								
FMVSS 208	FWRB/ODB	HIII 5								
FMVSS 208	FWRB	HIII 50								
FMVSS 208	OOP	HIII 5								
FMVSS 208	OOP	HIII 6y/o								
FMVSS 208	OOP	HIII 3y/o								
FMVSS 208	OOP	CRABI 12m								
Euro NCAP	ODB	HIII 50								
Euro NCAP	FWRB	HIII 5								
C-NCAP	ODB/FWRB	HIII 50			.(N <u>IIIII</u> N)	N <u>IIIII</u> N.				
C-NCAP	ODB/FWRB	HIII 5			///////////////////////////////////////	M(()()()				
JNCAP	ODB/FWRB	HIII 50			(W))))))))	<u>/////////////////////////////////////</u>				
JNCAP	ODB	HIII 5			()/////////////////////////////////////	/////////				

Legend:

Regulations: requirements are met / NCAP: maximum score

Regulations: requirements not met / NCAP: zero score

 $^{\rm 1}$ assessed only if Head ares peak > 80 g

Please note that the values indicated in this graph may be rounded and that additional criteria may exist. Please take exact values and additional criteria from the tables for the respective regulation.

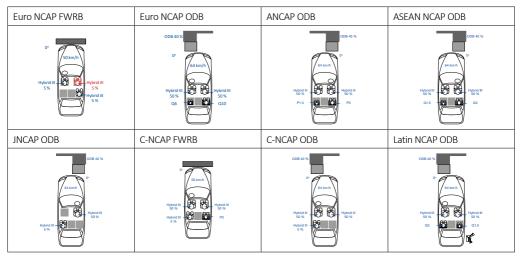
SAFETY WISSEN	UPDATE							cá		5.
Regulation	Crash	ATD						0-fr	ty Wissen by C	
Criterion	Туре	[UoM]						Sale	tywissen by L	
Chest a _{3ms}		[g]	30	40	50	60	70	80	90	100
FMVSS 208	FWRB/ODB	HIII 5/50								
FMVSS 208	OOP	HIII 5						-		
FMVSS 208	OOP	HIII 6y/o						_		
FMVSS 208	OOP	HIII 3y/o								
FMVSS 208	OOP	CRABI 12m								
IIHS	ODB/SOB	HIII 50								
JNCAP	ODB/FWRB	HIII 50			///////////////////////////////////////					
5110,1	000,000									
Chest VC _{ma}	X	[m/s]	0	0.2	0.4	0.6	0.8	1.0	1.2	1.4
UN R94	ODB	HIII 50	1111111			11111111			1111111111	
UN R137	FWRB	HIII 5/50								
IIHS	ODB/SOB	HIII 5/50								
Euro NCAP	ODB/SOB							X		
C-NCAP		HIII 5/50 HIII 50						N		
C-NCAP	ODB/FWRB				////	W/////////////////////////////////////	(#/////////////////////////////////////			
Femur Faxia		[kN]	0	2	4	6	8	10	12	14
UN R94	ODB	HIII 50	111111	···		17111111				
UN R137	FWRB	HIII 5								
UN R137	FWRB	HIII 50								
FMVSS 208	ODB	HIII 50								
FMVSS 208	ODB/FWRB	HIII 5								
FMVSS 208	ODB/TWRB	HIII 5								
Euro NCAP	ODB	HIII 50					Nama -			
Euro NCAP	FWRB	HIII 50					anna			
C-NCAP	ODB	HIII 50								
JNCAP	ODB/FWRB	HIII 50						\		
JNCAP	ODB/TWRB	HIII 5						\ \		
JINCAP	ODB					W////				
Knee Displa	cement	[mm]	4	6	8	10	12	14	16	18
UN R94	ODB	HIII 50								
Euro NCAP	ODB	HIII 50								
IIHS	ODB/SOB	HIII 50								
C-NCAP	ODB/50B	HIII 50					1//////////////////////////////////////			
CINCAP	ODB/1 WKB	1111 30				W/////////////////////////////////////	(#/////////////////////////////////////			
Tibia Index		[-]	0	0.2	0.4	0.6	0.8	1.0	1.2	1.4
UN R94	ODB	HIII 50	1111111			11111111				11111111111
Euro NCAP	ODB	HIII 50								
IIHS	ODB ODB/SOB	HIII 50								
C-NCAP	ODB/50B	HIII 50					1//////////////////////////////////////			
					-(()()()()()	X\\\\\\\\	()())))))))	()()))))))))	X\\\\\ 	
JNCAP	ODB/FWRB	HIII 50				W/////////////////////////////////////	(#/////////////////////////////////////	(#/////////////////////////////////////	A////	
Tibia Comp	ression	[kN]	0	2	4	6	8	10	12	14
UN R94	ODB	HIII 50								
Euro NCAP	ODB	HIII 50			VIII TUTUT	in ann an a				
IIHS	ODB/SOB	HIII 50				in in the second				
C-NCAP	ODB/FWRB	HIII 50		/////////	\mathcal{N}	AUUUU				
	,,					******				



UPDATE

Safety Requirements for Rear Seats and Restraint Systems

Frontal impact tests with rear seat occupants





Side impacts tests with rear seat occupants

FMVSS 214	U.S. NCAP	IIHS	C-NCAP
Euro NCAP MDB	Latin NCAP MDB	ASEAN NCAP	KNCAP
WS 50% Ø 1000-00 A. MOS VLS, 1300 W 00	E5-2 S0 km/h 90° h MDB EEVE, 500 kg 015 03	552 50 m/h 50° 400 m/h 50° 50° 50° 50° 50° 50° 50° 50°	45 405 43 1300 4 5 1400 45 100 100 100 100 100 100 100 10



Rear Seat Occupant Protection in Frontal Impact

Course Description

Rear seat occupant protection has been a low priority until the recent introduction of safety assessment for rear adult and child occupants by Euro NCAP. Now it has moved into the focus of research and development.

In addition to the Euro NCAP requirements, further NCAP ratings as well as legal requirements need to be considered in the design of the restraint systems. And real world aspects cannot be neglected either.

During the 1-day seminar legal and NCAP requirements for rear seat occupant protection in frontal impact will be discussed. Furthermore the dummies used in the assessment will be presented with an empasis on the Q6 and Q10 child dummies. For the most important load cases the relevant criteria and possible influcening parameters of the restraint system will be discussed and explored. Finally solutions for the design of the restraint system on rear seat will be shown.

Note: Only frontal impact load cases will be considered.

Course Objectives

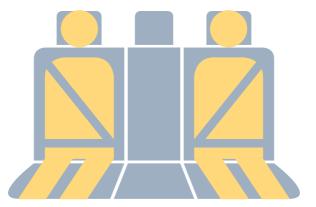
The objective of the seminar is to provide an understanding of the requirements and specifics in rear seat occupant protection, to provide the knowledge of test configurations and dummies, and to provide a view on state-of-the-art solutions.

Who should attend?

The seminar addresses simulation and test engineers, project engineers and project managers as well as the heads of development departments in the field of passive safety who work in R&D of occupant restraint-systems.

Course Contents

- Legal Requirements
- Requirements from consumer testing
- Dummies on the rear seat; Q6 and Q10 Child Dummies
- Relevant protection criteria for the most important load cases
- Solutions for restraint system design and optimization





Dr.-Ing. Burkhard Eickhoff (Autoliv B.V. & Co. KG) studied mechanical engineering in Hannover (Germany) focusing on vehicle engineering and applied mechanics. Starting from 1999 he worked with Autoliv B.V. & Co. KG as a test engineer for sled and crash tests. Since 2003 he has been project manager in systems development (safety belt) of the same company. Since 2012 he has worked as a group leader at Autoliv. He is involved in the definition and assessment of new restraint systems and he conducts feasibility studies using system simulation as well as dynamical tests. Moreover he has a consultant role regarding restraint system design. He finished his doctoral thesis at the Helmut Schmidt University Hamburg in 2012 on the reduction of belt induced thorax deflection in frontal crashes.

ę	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
Da	06.10.2017	2894	Alzenau	1 Day	740,- EUR till 08.09.2017, thereafter 890,- EUR	





MDB Side Impact Test Procedures according to UN R95, Euro NCAP and IIHS

Requirement UN R95		Euro NCAP	IIHS			
Impact angle		1				
MDB velocity		50 km/h		1 (())		
Barrier (MDB)	EEVC	AE-MDB IIHS				
Mass	Mass 950 kg		1500 kg			
Ground clearance	300 mm	300 mm (bumper 350 mm)	379 mm (bumper 430 mm)			
Upper edge height 800 mm		800 mm 1138 mm				
Width	1500 mm	1700 mm 1676 mm				
Dummy front seat ES-2 impact side		WS 50 % impact side SID IIs impact side				
Dummy rear seat	Q10 impact side Q6 far side		SID IIs impact side			
Protection Criteria	Head HPC < 1000 Chest VC < 1.0 m/s Rib deflection D < 42 mm Abdomen sum of APF < 2.5 kN Pelvis PSPF < 6.0 kN	 ⊃ page 28 (Adults) ⊃ page 87 (Children) 	➔ page 38	Safety Wissen by CarThS.		

Pole Side Impact Tests according to Euro NCAP, UN R135, GTR 14 and FMVSS 214 new

Requirement	Euro NCAP	UN R135 / GTR 14		FMVSS 214 new	U.S. NCAP
Vehicle Velocity (on Flying Floor)			up to 32 km/h		32 km/h
Impact angle		(blique 75	° on fixed pole	
Pole diameter			25	4 mm	
Dummy	WorldSID	50 % on impact side	ES-2 re o side	r SID IIs (Build Level D) on impact	SID IIs 5 % on impact side
Protection Criteria	➔ page 28	Head HIC ₃₆ < 1000 Shoulder F _{lateral} < 3.0 kN Chest deflection < 55 mm Abdomen deflection < 65 mm Lower Spine Acc. < 75 g PSPF < 3.36 kN	SID IIs: ES-2 re:	$\label{eq:HIC36} \begin{split} &\text{HIC36} < 1000\\ &\text{Lower Spine Acc.} < 82 \text{ g}\\ &\text{Pelvis Force} < 5.525 \text{ kN}\\ &\text{HIC36} < 1000\\ &\text{Chest deflection} < 44 \text{ mm}\\ &\text{Abdominal Force} < 2.5 \text{ kN}\\ &\text{PSFP} < 6 \text{ kN} \end{split}$	● page 33
Test Configuration	SafetyWissen by Cartis.			75° 16°	32 kmh

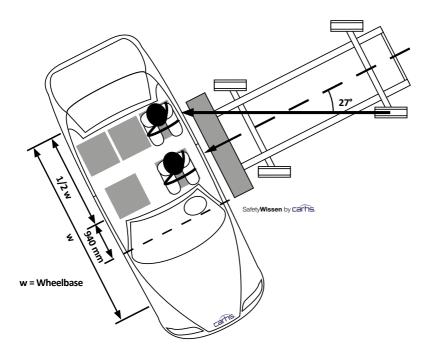
SAFETY WISSEN UPDATE



MDB - Side Impact Tests according to FMVSS 214 / U.S. NCAP

Requirement	FMVSS 214 new rule	U.S. NCAP	U.S. NCAP Upgrade ¹				
Impact angle		lateral 90°, 27° crab angle					
Impact velocity	53±1 km/h (33.5 mph) (~47 km/h in 90° direction)	61.9 ±0.8 km/h (~5	61.9 ±0.8 km/h (~55 km/h in 90° direction)				
Barrier		NHTSA MDB					
Mass		1368 kg					
Ground clearance		279 mm (Bumper 330 mm)					
Upper edge height		838 mm					
Width		1676 mm					
Dummy front seat	ES-2 re impact side	ES-2 re impact side	WorldSID 50 % (SBL F) impact side				
Dummy rear seat	SID IIs (Build Level D) impact side	SID IIs (Build Level D) impact side	SID IIs (Build Level D) impact side				
Protection Criteria	SID IIs: HIC ₃₆ < 1000 Chest acceleration < 82 g Pelvis force < 5.525 kN ES-2 re: HIC ₃₆ < 1000 Chest deflection < 44 mm Abdominal force < 2.5 kN Pelvis force < 6 kN	€ page 33	Criteria not yet defined				

¹ planned for model year 2019



CEACES. UPDATE Seat Adjustments for Side Impact Tests () () () () () () () () () ()								
	(1) Seat Fore/Aft	2 Seat Height	3 Seat Back Angle	(4) Head Restraint	5 Head Restraint	6 Seat Base Tilt		
	Seat Fole/Alt	Seat neight	Seat Dack Aligie	Height	Fore/Aft	Seat base filt		
Euro NCAP MDB	mid + 20 mm	lowest	manuf. design position or 23°	mid	mid ¹	mid		
Euro NCAP Pole	mid + 20 mm	lowest	manuf. design position or 23°	mid	mid ¹	mid		
UN R95	mid	height of non-adjustable passenger seat or mid	manuf. design position or 25°	top surface level with head COG or uppermost	mid	mid		
UN R135	mid + 20 mm	lowest	manuf. design position or 23°	uppermost or manuf. design position.	most rearward	mid		
U.S. NCAP / FMVSS 214 ES-2RE	mid	lowest ²	manuf. design position or 25°	uppermost	most forward	"absolute" mid²		
U.S. NCAP / FMVSS 214 SID-2s	most forward position	mid	head at 0°	lowest	most forward	"absolute" mid ²		
U.S. NCAP / WorldSID 50	mid + 20 mm	lowest ²	manuf. design position or 25°	uppermost	most forward	"absolute" mid²		
ISO WorldSID 50	mid + 20 mm	lowest	manuf. design position or 23°	uppermost or manuf. design position.	s	afety Wissen by carhs .		

¹ If there is any interference with the rear of the dummy head, move the HR to the most rearward position. ² Seat base tilt adjustment 6 has priority w.r.t. seat height adjustment 2.





Side Impact Protection Criteria Compared

Regulation	Crash	ATD								
HIC15		[-]	300	400	500	600	700	800	900	1000
Euro NCAP JNCAP C-NCAP IIHS ¹ Pole: no sliding sca	MDB/Pole ¹ MDB MDB MDB	WS 50 ES-2 SID2s SID2s								
HPC	ne but capping on	[-]	300	400	500	600	700	800	900	1000
UN R95	MDB	ES-2								
HIC ₃₆		[-]	300	400	500	600	700	800	900	1000
UN R135 FMVSS 214 C-NCAP	Pole MDB/Pole MDB	WS 50 ES-2/SID2s ES-2								
Head a _{3ms}		[g]	60	65	70	75	80	85	90	95
Euro NCAP C-NCAP ² Pole: no sliding sca	MDB/Pole ² MDB ale but capping onl	WS 50 ES-2 y for ares peak >								
Chest Comp		[mm]	20	25	30	35	40	45	50	55
UN R95 UN R135 FMVSS 214 Euro NCAP IIHS	MDB Pole MDB/Pole MDB/Pole MDB	ES-2 WS 50 ES-2 WS 50 ES-2								
C-NCAP JNCAP	MDB MDB	ES-2 ES-2 ES-2								
Shoulder La	teral Force	[kN]	0	1	2	3	4	5	6	7
UN R135	Pole	WS 50								
Chest VC _{ma}	x	[m/s]	0	0.2	0.4	0.6	0.8	1.0	1.2	1.4
UN R95 C-NCAP IIHS	MDB MDB MDB	ES-2 ES-2 ES-2								
Lower Spine	e a _{3ms}	[g]	0	25	50	75	100	125	150	175
UN R135	Pole	WS 50								
Abdomen F	orce	[kN]	0	0.5	1	1.5	2	2.5	3	3.5
UN R95 FMVSS 214 C-NCAP JNCAP	MDB MDB/Pole MDB MDB	ES-2 ES-2 ES-2 ES-2								
Abdomen Co	ompression	[mm]	40	45	50	55	60	65	70	75
Euro NCAP	MDB/Pole	WS 50				MAAAAA				
PSPF		[kN]	0	1	2	3	4	5	6	7
UN R95 UN R135 FMVSS 214 Euro NCAP C-NCAP JNCAP	MDB Pole MDB/Pole MDB/Pole MDB MDB	ES-2 WS 50 ES-2 WS 50 ES-2 ES-2 ES-2								
Pelvis Force		[kN]	0	1	2	3	4	5	6	
FMVSS 214 C-NCAP	MDB/Pole MDB	SID2s SID2s								



Side Impact - Requirements and Development Strategies

Course Description

In addition to the protection in a frontal impact, the protection in a side impact has a fixed place in the development of vehicles. Continuous aggravation of consumer tests and legal regulations, e.g. due to new pole tests (UN ECE-R135 and Euro NCAP), enhanced deformable barriers and the prospective introduction of World-SID-Dummies (5 / 50%ile) are causing a need to further improve side impact protection. In order to achieve this enhancement, it is necessary to get a much more profound understanding of the highly complex phenomena and modes of action in a side impact which goes far beyond the simple application of additional airbags.

The seminar provides a comprehensive overview of today's standard test procedures including country-specific variations, the legal regulations and the requirements of consumer protection as well as an outlook on changes in the near future. In addition, tools, measuring methods and criteria, and especially virtual methods such as crash and occupant simulation, as well as the analysis of the performance of the restraint systems will be discussed. Furthermore it will be explained how a target-oriented use of CAE-simulation and hardware tests can lead to optimal passenger values, while at the same time obeying to boundary conditions such as costs, weight and time-to-market. A part of the workshop with crash-data analysis finally deepens the understanding.

it is especially interesting for project managers and managers, who deal with side impact and who would like to gain a deeper understanding of this topic in order to use it for an improvement of procedures.

Course Contents

- Challenges of side impacts
- Side impact-relevant protection criteria. Legal tests (FMVSS 214, UN ECE R95, UN ECE R135, ...) Other tests (Euro NCAP, U.S. NCAP, further NCAPs, IIHS, car manufacturer-specific tests)
- Development methods and tools:
- Crash and occupant simulation, range of application and limitations.
- Performance of restraint systems in side impact:
- Analysis of the performance of protection and restraint systems in side impact. Discussion of the limitations, conflicts and problems.
- Development strategy for an optimal restraint system for side impact
- Target-oriented use of CAE-simulation and hardware tests
- Workshop with analysis of crash-data and discussion of the results

Who should attend?

The seminar addresses development engineers who are new in the field of side crash, or who have already gained some experience in the field of safety, as well as developers of assemblies that have to fulfil a crash-relevant function. Furthermore



Stephanie Wolter (BMW AG) studied Engineering Physics at the University of Applied Sciences Munich. Since 1995 she has been working at BMW AG in different functions in the field of side protection, such as pre-development, development of side airbags and as a project engineer in various car lines. Moreover, she represents BMW-Group in various national and international bodies that deal with side impact and other aspects of side protection, e.g. German Side Impact Working Group, ISO Working Groups, etc.

Instructors



Bart Peeters Weem (BMW AG) studied mechanical engineering at the University of Technology in Eindhoven with focus on system and control. Since 2003 he has worked at BMW on passive safety development. First as Simulation Engineer, later as team leader and project referent. Since 2015 he is head of the development of full vehicle side impact protection for BMW 1-, 2- and 3-series, MINI and BMW-i.

S	DATE	COURSE ID	VENUE	DURATION	N PRICE	LANGUAGE
Venu	0405.04.2017	2938	Gaimersheim	2 Days	1.290,- EUR till 07.03.2017, thereafter 1.540,- EUR	
tes &	0708.06.2017	2932	Alzenau	2 Days	1.290,- EUR till 10.05.2017, thereafter 1.540,- EUR	
Dat	2829.11.2017	2933	Alzenau	2 Days	1.290,- EUR till 31.10.2017, thereafter 1.540,- EUR	

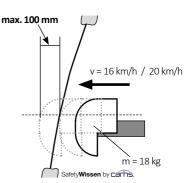


FMVSS 226 - Ejection Mitigation

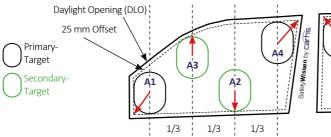


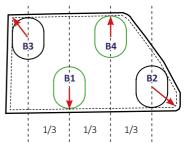
- At up to 4 impact test locations on each side window in the first 3 rows of seats the head excursion may not exceed 100 mm
- Tests at two impact velocities: 16 km/h and 20 km/h
- Head protection systems (e.g. curtain airbags) must be fired before the impact:
 - at 20 km/h with a time delay of 1.5 s prior to the impact
 - at 16 km/h with a time delay of 6 s prior to the impact
- Tests are done without glazing or with pre-damaged glazing
 pre-damage: perforation in a 75 mm grid pattern
- Valid for vehicles with GVWR ≤ 4536 kg
- Phase-In: 2013 2017

Front Row Window









Steps	Front Row Window	Rear Row Windows Safety Wissen by carries.				
1	Set Primary Target A1 in lower front corner	Set Primary Target B3 in upper front corner				
2	Set Primary Target A4 in upper rear corner	Set Primary Target B2 in lower rear corner				
3	Divide horizontal distance between A1 and A4 in thirds	Divide horizontal distance between B3 and B2 in thirds				
4	Move A3 at the first third vertically upward	Move B1 at the first third vertically downward				
5	Move A2 at the second third vertically downward	Move B4 at the second third vertically upward				
6	Measure Distances D _x (horizontal) and	D, (vertical) of the target center points				
7	If D _z (A2 - A3) < 135 mm and D _z (A2 - A3) < 170 mm \rightleftharpoons Eliminate A3	If D $_{z}$ (B1 - B4) < 135 mm and D $_{z}$ (B1 - B4) < 170 mm \Rightarrow Eliminate B4				
8	If D _x (A4 - A3) (or A2 if A3 was eliminated in step 7) < 135 mm and D _y (A4 - A3/2) < 170 mm \Rightarrow Eliminate A3/2	If D _x (B3 - B4) (or B1 if B4 was eliminated in step 7) < 135 mm and D _y (B3 - B4/1) < 170 mm \Rightarrow Eliminate B4/1				
9	If D _x (A4 - A2) (or A3 if A2 was eliminated in step 8) < 135 mm and D _y (A4 - A2/3) < 170 mm \Rightarrow Eliminate A2/3	If D _x (B2 - B1) (or B4 if B1 was eliminated in step 8) < 135 mm and D, (B2 - B1/4) < 170 mm \Rightarrow Eliminate B1/4				
10	If D _z (A1 - A4) < 135 mm and D _z (A1 - A4) < 170 mm \rightleftharpoons Eliminate A4	If D _z (B3 - B2) < 135 mm and D _z (B3 - B2) < 170 mm \Rightarrow Eliminate B3				
11	If only 2 targets remain: Measure absolute distance D the center points of the targets					
12	If D > 360 mm, set additional 3rd target on the center of the line connecting the targets					
13	If less than 4 targets remain, repeat steps 1-12 with the impactor rotated by 90 degrees. If this results in a higher number of targets use the rotated targets.					
14	If no target is found rotate the impactor in 5 degree steps, until it is possible to fit the impactor in the DLO-offset. Then place the center of the target as close to the geometric center of the DLO as possible.					

Valid for vehi Phase-In: 201

Locating Targets:

Test Procedure TP-226-00, Mar 2011

Head Impact on Vehicle Interiors

arns

UN R21

Test Procedure

A pendulum equipped with a spherical impactor (165 mm) hits the interior parts in front of the driver and passenger (side, pedal and steering wheel excluded) with a velocity of 24.1 km/h.

Protection Criteria

a_{3ms} < 80 g; no failure of structure and sharp edges in impact zone

Pendulum test is not necessary, if it can be shown that there is no contact between head and the instrument panel in case of a frontal impact.

This can be done by crash tests, sled tests and/or numerical occupant simulation. (See app. 8 of UN R21)

FMVSS 201U

Test Procedure TP-201-02, Jan 2016

[s]

Test Procedure

A Free Motion Headform (FMH) impactor hits the upper interior parts with a velocity of 24 km/h (A-, B-, C-pillar, roof etc.).

FMH Impactor Data

Mass of FMH impactor: 4.54 kg Head form according to SAE J 921 and J 977 including triaxial acceleration sensor.

Protection Criteria

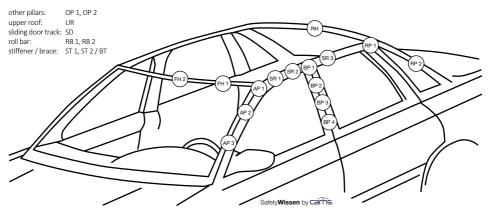
HIC Calculation

$$HIC = sup_{t_1,t_2} \left\{ \left[\frac{1}{(t_2-t_1)} t_1^{f_2} adt \right]^{2,5} (t_2-t_1) \right\} \qquad t_2-t_1 < 36 \text{ ms; } a \text{ [g]; } t_1 = 0 \text{ ms; } t_2 \text{ ms; } a \text{ ms;$$

HIC value for FMH *HIC(d)* = 0.75446 HIC + 166.4

HIC(d) must not exceed 1000.

24 points defined for impact according Test Procedure TP-201U-02 (each side, left and right)







Head Impact on Vehicle Interiors: FMVSS 201 and UN R21

Course Description

To prevent injuries resulting from impacts of the occupants' heads on vehicle interior parts, these parts need to be designed in a way which allows sufficient deformation space to reduce the loads on the head. Internationally there are two important regulations regarding the design of interiors, such as cockpits, roof and door liners: The U.S. FMVSS 201 and the Regulation UN R21. Both regulations stipulate requirements concerning the maximum head acceleration or the HIC in impacts on interior parts.

The objective of this course is to provide an overview of the legal requirements and to show how these can be fulfilled. The focus of the seminar is on the development process and the development tools and methods. In particular the interaction of testing and simulation will be described and different design solutions will be discussed. Typical conflicts of objectives in the design - e.g. to fulfil NVH requirements, static stiffness, or misuse, while fulfilling the safety standards at the same time - are addressed in this seminar. Examples of practical solutions will be shown and discussed.

In addition, the development according to the head impact requirements in the overall-context of vehicle development is described in this seminar.

In a workshop exemplary head impact locations in a vehicle interior and impact areas on a dashboard are determined.

Who should attend?

This seminar is especially suited for engineers and technicians who work on the development of vehicle interior parts and who want to become familiar with the safety requirements that are relevant for these parts.

Course Contents

- Introduction
- Rules and regulations concerning head impact
 - FMVSS 201
 - UN R21
- Development tools
 - Numerical Simulation
 - Test
- Workshop: Determination of impact locations in a vehicle
- Development process and methods
 - Solving of conflicts of objectives
 - Typical deformation paths, padding materials



Torsten Gärtner (Adam Opel AG) has been working as a simulation expert since 1997. From numerous projects he has extensive experience in the field of occupant simulation and interior safety. He is Technical Lead Engineer Safety Analytics at Adam Opel AG. Before that he worked as department manager for safety with Tecosim GmbH and spent 10 years in various management positions with carhs gmbh.

Instructors



Karsten Wolff (Continental Safety Engineering International GmbH) studied Traffic Safety Technology at the University of Wuppertal. During his studies he worked at BGS (Böhme & Gehring Sicherheitstechnik) in the fields of dummy calibration and head impact. In 1998 he joined Continental Safety Engineering International as an engineer. In 2000 he established FMVSS201U testing at Continental and in 2002 he introduced pedestrian protection testing. Later on UN ECE R21 and FMVSS201L testing was added, followed by ejection mitigation. In 2003 he became team leader for pedestrian protection and interior head impact, in 2009 he started leading the development and testing for FMH und pedestrian protection and since 2012 he has been team leader of the competence center for pedestrian protection and interior head impact. In this role he acts as a link between simulation, project and testing.

S	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
Venues	05.04.2017	2829	Alzenau	1 Day	740,- EUR till 08.03.2017, thereafter 890,- EUR	
es &	12.06.2017	2898	Alzenau	1 Day	740,- EUR till 15.05.2017, thereafter 890,- EUR	
Dates	27.09.2017	2931	Alzenau	1 Day	740,- EUR till 30.08.2017, thereafter 890,- EUR	



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AUTOMOTIVE SAFETY TESTING

Universal Impact Simulation = Seat Belt Anchorage = Head & Seat Back Restraint = Roof Crush & Door Intrusion
Instrumented Crash Wall
Acceleration-Deceleration Sled
Sled Crash Facility = Laser-Measurement Device = Bumper Pendulum



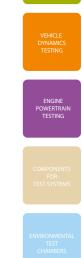
Multi-Axis Acceleration Sled with Dynamic Pitch & Yaw Functionality



BHIA250-VC Launcher for FMH and Guided Head Impacts



BIA Universal Impact Simulation Test System



Beyond Expectations



Automotive Safety Testing = Engine & Powertrain Testing = Vehicle Dynamics Testing Components for Test Systems = Environmental Test Chambers

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12th PraxisConference **Pedestrian Protection**

The PraxisConference Pedestrian Protection is held every June or July with over 150 participants, including delegates from all major OEMs. It is the world's largest expert meeting in the field of pedestrian protection. The intensive discussions at the info-points and between the presentations show that the participants value the innovative conference concept. Highlights of the event are the demonstrations in the laboratory of Germany's Federal Highway Research Institute and the OEM's presentations of pedestrian protecting solutions implemented in current car models.

Although the industry has been working on pedestrian protection for many years now, the constant development of the requirements (regulations and NCAP) continuously raises new questions that will be answered during this conference.

Expert speakers provide concentrated information regarding current and future requirements, latest research findings and technical solutions. Both, testing and numerical simulation are covered in the conference presentations.

In addition to this the conference offers hands-on praxis session in the laboratory. Here, test equipment and impactors are demonstrated and explained in detail. The preparation, execution and analysis of pedestrian impact tests are shown in live demonstrations.

Conference Topics:

- Current status and future development of the regulations (UN R127, GTR 9)
- Global consumper protection requirements for pedestrian protection
- Future development of impactors
- Pedestrian AEB systems
- Pedestrian safety techologies (active bonnets, airbags)
- Test equipment

Who should attend?

The PraxisConference is suited for pedestrian protection experts from throughout the industry. Even beginners will find the event an excellent opportunity to quickly acquire theoretical and practical knowledge and become part of the expert community.

	DATE	28 29. June 2017	
	HOMEPAGE	www.carhs.de/pkf	Co-hosted with
Facts	VENUE	Bundesanstalt für Straßenwesen, Brüderstraße 53, 51427 Bergisch Gladbach	BGS
	LANGUAGE	German with simultaneous translation into English	
	PRICE	1.450,- EUR till 31.05.2017, thereafter 1.690,- EUR	BGS Böhme & Gehring GmbH









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Pedestrian Protection - Development Strategies

Course Description

rarne

Phase 2 of the EU regulation on pedestrian safety was introduced, Japan recognizes the UN Regulation 127 and Euro NCAP annually adjusts details in its pedestrian rating protocols. Currently, the greatest challenge regarding pedestrian protection in the vehicle development process is to generate a facelift of successor model based on a car that had received a 5 star Euro NCAP rating prior to 2010, that will be type approved according to phase 2 of the European regulation and also continue to receive a 5 star rating according to Euro NCAP's latest protocols. Stricter injury criteria, modified testing areas and the testing of vehicles that were previously not tested because of their weight, require the thorough knowledge of the requirements and a strict implementation of the requirements in the development process.

In the introduction the seminar informs about the different impactors that are used for pedestrian safety testing. Thereafter the various requirements (regulations and consumer tests) are explained and compared.

The focus of the seminar is on the development strategy: Which decisions have to be taken in which development phase? What are the tasks and priorities of the person in charge of pedestrian protection? As a background, ideas and approaches towards the design of a vehicle front end in order to meet the pedestrian protection requirements are discussed. In addition to that, the seminar explains how the function of active bonnets can be proven by means of numerical simulation. This includes both, the pedestrian detection that need to be proven with various impactors or human models, as well as the proof that the bonnet is fully deployed at the time of impact.

Who should attend?

The seminar is intended for development, project or simulation engineers working in the field of vehicle safety, dealing with the design of motor vehicles with regard to pedestrian protection.

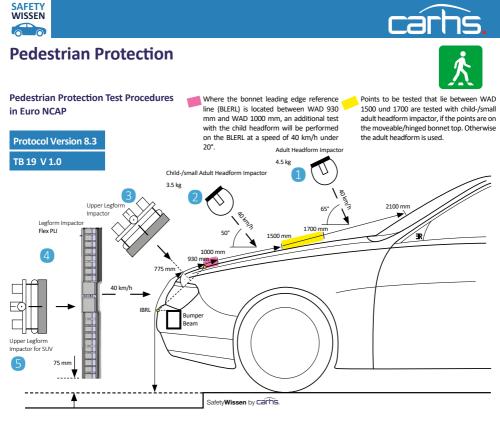
Course Contents

- Introduction with an overview of current requirements regarding pedestrian protection
 - Legal requirements (EU, UN Regulations, Japan, GTR)
 - Consumer tests (Euro NCAP, JNCAP, KNCAP)
- Presentation and discussion of the design and application of the impactors
 - Leg Impactors (Flex PLI, EEVC, Upper Legform)
 - Head Impactors (Child head, Adult head)
- Methods in numerical simulation, testing and system development
- Requirements on the design of vehicle front ends for pedestrian protection
- Solutions to fulfill the requirements
 - Passive solutions
 - Active solutions (active bonnets, airbags)
- Development strategy
 - Interaction between simulation and testing
 - Integration in the vehicle development process



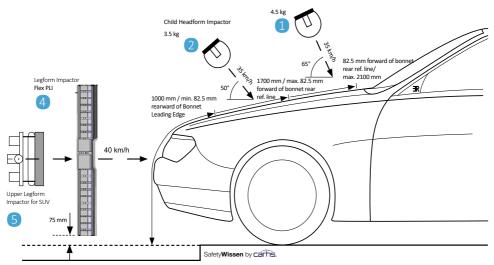
Maren Finck (carhs.training gmbh) is a Project Manager at carhs.training gmbh. From 2008 - 2015 she worked at EDAG as a project manager responsible for passive vehicle safety. Previously, she worked several years at carhs GmbH and TECOSIM as an analysis engineer with a focus on pedestrian safety and biomechanics.

es	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
Venu	29.03.2017	2819	Alzenau	1 Day	740,- EUR till 01.03.2017, thereafter 890,- EUR	
ates &	31.05.2017	2895	Alzenau	1 Day	740,- EUR till 03.05.2017, thereafter 890,- EUR	×
Dat	10.10.2017	2941	Gaimersheim	1 Day	740,- EUR till 12.09.2017, thereafter 890,- EUR	



Pedestrian Protection Test Procedures according to UN R127.02

Adult Headform Impactor



THE ROAD IS THERE **FOR EVERYONE!**

From virtual analysis to validation in our test centre: we are making the roads that little bit safer for pedestrians.

Single-source pedestrian protection function development: one partner for the customer

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From our experience as the world's leading independent engineering service provider, we know that vehicle safety is of key importance when developing complete vehicles. We offer all the services relevant to pedestrian protection, from **project management** and **simulation** through to **testing** in our fully equipped test facilities. At many sites, and also close to you.

Are you interested in finding out how our experience can help you create both function and emotion? Then ask us.



Contact EDAG Engineering GmbH fgs@edag.de

Jörg Barnscheid Tel.: +49 89 350989-189



For more information on the subject of pedestrian protection see: **fgs.edag.de**





UPDATE

SAFETY WISSEN

Test Procedures and Protection Criteria for Pedestrian Protection

S Upper Legform ⁷ 9.5 kg	G					Lower Legform ⁷	4					10.5 kg	3 Ilmar Lagform			9 165 mm	Child Headform				Ø 165 mm	Adult Headform				Test Method	
ACL/PCL Elongation (mm) VL (km/h) Sum of forces (kN) Bending Moment (Nm)	ACL/PCL Elongation (mm) VL (km/h)	ACL/PCL Elongation (mm)		MCL Elongation (mm)	Tibis Donding (Nim)	Bending angle (") Shearing (mm)	Acceleration (g)	Ground clearance d (mm)	VL (km/h)	Legform	Bending Moment (Nm)	Sum of forces (kN)	VU (km/h)	αU (°)	HPC/HIC (-)	on Windscreen	WAD (mm)	VC (km/h)	αC (°)	HPC/HIC (-)	on Windscreen	WAD (mm)	VA (km/h)	αA (°)		Parameter	
5 285			10	202 19	101				~	Fle	285 Nm	5 kN	20	90 w.r.t. IBR	650	~	1000 - 17	~		650	Y	1700 (15)	~	•	max. score	Euro U.S. I	
6 350		40	10	340 22	0//0			75	40	Flex PLI	350 Nm	6 kN	20 - 33	90 w.r.t. IBRL ⁴ - WAD 930	1700	yes	1000 - 1700(1500) ¹	40	50	1700	yes	1700 (1500) ¹ - 2100	40	65	zero score	Euro NCAP U.S. NCAP ⁸	
Drints to be tested that lie between WAD 1500 and 1700 are tested with shild-semiladult			0	202 14.8	τητ			75	40 (44) ⁵	Flex PU					650	yes	1000 - 1700	40	50 (20 ²)	650	γes	1700 - 2100	40	65	max. score	JNCAP	
F			13	19,8	306			U	44) ⁵	: PU					1700	ß	- 1700	0	20 ²)	1700	ß	- 2100	0	5	zero score	CAP	
⁶ In an area ⁷ For vehicle	5 300 / 285 ¹²	4	10	202 19	101			7	4	Fley					650	Y	1000	40	5	650	Y	1700	40	65	max. score	KNCAP C-NCAP ¹¹	
In an area no wider than 264 mm. For vehicles with a lower humo.	5 7.5 / 6 ¹² 300 / 285 ¹² 510 / 350 ¹²	40	10	340 22	0/10			75	40	Flex PLI					1700	yes	1000 - 1700	ö	50	1700	yes	1700 - 2100	ö	Ū	zero score	САР	
264 mm. er bumper height	7.5 510	40				6	170 (250) ⁶	25	40	EEVC					$1000 / 1700^3$	no	1000 - 1700 ¹⁰	35	50	$1000 / 1700^3$	no	1700 - 2100 ¹⁰	35	65	Phase 2	EU Regulations 78/2009 and 631/2009	
2 < 425 mm the lo	7.5 510	40	13	240 (300) 22	9/0001 01/ C			75	40	Flex PLI					1000 / 1700 ³	no	1000 ⁹ - 1700 ¹⁰	35	50	$1000 / 1700^3$	no	1700 - 2100 ¹⁰	35	65		UN R127	
⁶ In an area no wider than 264 mm. ⁷ For vehicles with a lower bumper height < 425 mm the lower legform test ④ is applied. For vehicles with a lower bumper height ≥ 500 mm the upper legform test ⑤ is applied. For vehicles with a lower bumper height ≥ 425 mm an < 500 mm the impactor is at the choice of the	7.5 510	40	13	22	910001010			75	40	Flex PLI					1000 / 1700 ³	no	1000 - 1700 ¹⁰	35	50	$1000 / 1700^3$	no	1700 - 2100 ¹⁰	35	65		GTR No. 9	
 is applied. is applied. For st the choice of the 	7.5	40	13	22	9/00C/01/C			75	40	Flex PLI					1000 / 1700 ³	no	1000 - 1700	35	50	$1000 / 1700^3$	no	1700 - 2100	35	65		Japan Article 18 Attachment 99	

SafetyWissen by carhs.

¹² C-NCAP

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Airbag Component Test Rig for various airbag- and steering column tests



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LIPDATE

Testing Protocol Version 8.3

Euro NCAP - Pedestrian Protection: Head and Leg Impact Grid Method

Head Impact

SAFET)

WISSEN

Between WAD 1000 and WAD 2100 impact points are located on a fixed 100 mm grid, the selection of "Worst Case" points by the test institute is no longer required. The manufacturer provides a result prediction (points) for the Grid-Points. Euro NCAP verifies 10 randomly selected points, the manufacturer can nominate up to 10 additional randomly selected points. A tolerance of 10% is applied to the verification tests, i.e. even if the actual HIC is 10% above or below the margins of the predicted score, the predicted score is applied. At the verification points the actual test result is divided by the manufacturer's prediction. This so called correction factor is applied to all the grid points to obtain the final score:

Actual tested score

Predicted score = Correction Factor

Per Grid-Point 0 - 1 points are available according to the following scheme:

	HIC ₁₅	< 650	1.00 Point
650 ≤	HIC ₁₅	< 1000	0.75 Points
1000 ≤	HIC ₁₅	< 1350	0.50 Points
1350≤	HIC15	< 1700	0.25 Points
1700≤	HIC ₁₅		0.00 Points

"Default" Results

Grid points on the A-pillars are defaulted to red = 0 points. Grid points on the windscreen that have distance of more than 165 mm from the windscreen base are defaulted to green = 1 point. Defaulted locations are not included in the random selection of verification tests. Where the vehicle manufacturer can provide evidence that shows an A-pillar is not red, those grid points will be considered in the same way as other points.

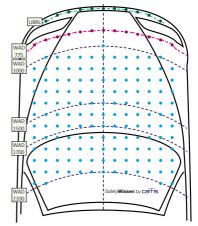
Unpredictable Grid Locations: blue Zones

In the following areas

- Plastic scuttle
- Windscreen wiper arms and windscreen base
- Headlamp glazing
- Break-away structures

the manufacturer may define a "blue zone" consisting of up to 2 adjacent grid points, for which no prediction is made. A maximum of eight zones may be blue over the entire headform impact area.

The laboratory will choose one blue point to assess each zone. The test results of blue points will be applied to all the grid point(s) in each zone.



Total score:

The total score will be calculated as follows:

- Σ Predicted Score x Correction Factor
- + ∑Default Scores
- + \sum Scores from Blue Zones
- = Total
- ÷ Number of Grid Points
- = Percentage of max. achievable score
- x 24 (Maximum achievable score)
- = Total Score for Headform Test

Leg Impact

For leg impact a 100 mm grid on WAD 775 (Upper Legform) respectively on Upper Bumper Reference Line (Flex PLI Legform) is used. Euro NCAP selects either the centerline point or an adjacent point as a starting point for testing. Starting from this position every second grid point will be tested. Symmetry is applied across the vehicle. Grid points that have not been tested will be awarded the worst result from one of the adjacent points. Manufacturers may sponsor additional test for those points that are not tested (in advance). Per Grid point up to 1 point is awarded. For the Upper Legform the score is based upon the worst performing parameter (Sum of Forces / Bending moment). For the Legform the 1 point per grid point is divided into two independent assessment areas of equal weight (0.5 Pts./each): Tibia moments and ligament elongations.

Total score:

The total score for the Upper/Lower Legform tests will be calculated as follows:

- Σ Scores of all Grid Points
- ÷ Number of Grid Points
- = Percentage of max. achievable score
- x 6 (Maximum achievable score)
- = Total Score for Legform Test

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DEVELOPING SAFER VEHICLES SINCE 1995



- and performance engineering for turnkey projects
- Deep understanding of legal and 🛛 🔶 Official Euro NCAP test house customer requirements
- Team of more than 500 safety experts

- Integration of design, simulation 😽 Testing facilities in Germany and Spain

 - Involved in research and pre-development activities

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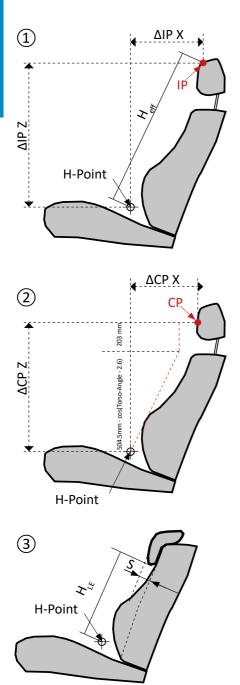


UPDATE



carhs.

Euro NCAP Rear Seat Whiplash Assessment



Assessment Protocol Version 7.0.3

Testing Protocol Version 1.0

 Effective Height H_{eff} requirements for the headrest: in highest position ≥ 770 mm and in worst case position ≥ 720 mm

Calculation of Heff:

 $H_{eff=} \Delta IP \ X \cdot sin \ (Torso-Angle) + \Delta IP \ Z \cdot cos \ (Torso-Angle) \\ IP: Intersection \ Point$

Determination of IP X and IP Z: IP X = $88.5 \cdot \sin (\text{Torso-Angle-} 2.6) + 5 + \text{CP X}$ IP Z = uppermost intersection of the headrest contour in the seat centerline with a vertical line through IP X

(2) Backset $\Delta CP X$ requirements for the headrest

in mid position and in worst case position:

 $\Delta CP X \le 7.128 \cdot Torso-Angle + 153$ CP: Contact Point

③ Requirements for the non-use position of the headrest:

- 1) > 60° rotation of the headrest in non-use position
- 2) ∆ Torso-Angle use / non-use > 10°
- 3) Height of lower edge of the headrest HLE: 250 mm \leq HLE \leq 460 mm
- with $H_{LE} = \Delta X \cdot sin$ (Torso-Angle) + $\Delta Z \cdot cos$ (Torso-Angle)
- Thickness of the lower edge of the headrest S ≥ 40 mm

Score if the requirements (see above) are met:

The outboard seating positions of rear seating rows are assessed. Any centre seating position needs to comply with the requirements of UN R17-08.

Parameter	Points per seat
1 H _{eff}	1.5
② ΔCP X _{mid}	1*
② ΔCP Xworstcase	0.5*
③ Non-Use	1*
max. total	4
Scaling	1/4n (n=number of seats)

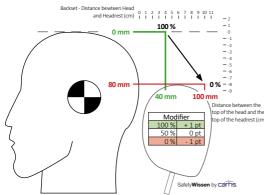
* only if Heff requirements are met

carh	.		EUF		۱P		U	PDATE	SAFETY WISSEN
Euro NCAP Fr	ont Se	eat Wł	niplash	n Asses	ssmen	t			
Seat Performance Crite	Ass	essment Pro	otocol Vers	ion 7.0.3	Testing	Protocol Ve	ersion 3.2		
Whiplash Test	Lc	ow Severity Pul	se	Mec	lium Severity F	Pulse	Hi	gh Severity Pu	se
Safety Wissen by Carhs.	Higher perfor- mance	Lower perfor- mance	Capping Limit	Higher perfor- mance	Lower perfor- mance	Capping Limit	Higher perfor- mance	Lower perfor- mance	Capping Limit
NIC	9.00	15.00	18.30	11.00	24.00	27.00	13.00	23.00	25.50
Nkm	0.12	0.35	0.50	0.15	0.55	0.69	0.22	0.47	0.78
Rebound velocity (m/s)	3.0	4.4	4.7	3.2	4.8	5.2	4.1	5.5	6.0
Upper Neck F _{x,shear} (N)	30	110	187	30	190	290	30	210	364
Upper Neck F _{z,tension} (N)	270	610	734	360	750	900	470	770	1024
T1 acceleration* (g)	9.40	12.00	14.10	9.30	13.10	15.55	12.50	15.90	17.80
T-HRC (ms)	61	83	95	57	82	92	53	80	92

* up to T-HRC (=Time to Head Restraint Contact)

If the Higher Performance Limit is reached, 0.5 points are awarded per criterion. A sliding scale is used between Higher and Lower Performance Limit (0.5 0 points). Only the maximum score from either T1 acceleration or head restraint contact time (T-HRC) is used in the assessment. If the capping limit is exceeded by one criterion, the entire test is rated with zero points.





Worst Case Geometry

1/n points (where n = the number of front seats) will be available for each front seat scoring more than 0 points in the worst case (= lowest and rearmost position) geometry assessment.

Seat Stability Modifier

The high severity pulse is subject to an additional seatback issues between the op of the head and the op of the head arc (m) seats with a rotation of 32° or greater

Dummy Artefact Modifier

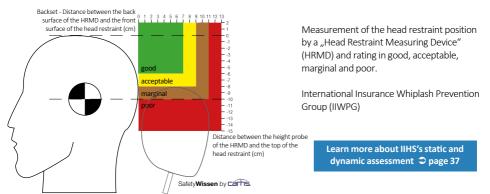
A two point negative modifier is applied as a means of penalising any seat that, by design, places unfavourable loading on other body areas or exploits a dummy artefact.

The assessment is based on the worst performing parameter from either the height or backset.

Overall Rating

For the overall rating (\bigcirc page 30) the total of max. 11 points (3 per pulse + 1 Geometry + 1 Worst Case Geometry) is scaled by the factor 2/11 and is part of the Adult Occupant Protection rating.

Static Geometry Assessment by IIWPG / IIHS





Whiplash Testing and Evaluation in Rear Impacts

Course Description

In real-world accidents, distortions of the cervical spine or so-called whiplash injuries following a rear impact are among the most expensive injuries for the insurance industry. About 75 % of all injury costs of the insurers are caused by whiplash injuries in highly-motorized countries. About 80 % of all injuries in a rear impact are whiplash-injuries. This is why this type of injury – even though it is neither very serious nor lethal – has reached a high priority in the endeavors to develop test procedures and assessment criteria which help in designing constructive measures in the car in order to avoid this type of injury.

As an introduction, this seminar refers to the different accident data for whiplash injuries, which offer many realizations but no consistent pattern with regard to the biomechanical injury mechanisms. However, some organizations – mainly from the field of consumer information and insurance institutes – are working on the development of test procedures and assessment criteria. The most active ones are Thatcham (UK) and IIHS (USA) which are united in the group IIWPG (International Insurance Whiplash Prevention Group), SNRA and Folksam (Sweden) and the German ADAC.

In 2008 Euro NCAP has introduced a whiplash test procedure as part of its rating system. In 2014 an additional assessment for the rear seats was added. The Euro NCAP assessment will be explained in detail in the seminar. Furthermore, the EEVC working group 20 is active as a consulting authority concerning whiplash injuries for the legislation in Europe.

The new Global Technical Regulation No. 7 (Head Restraints) is unsatisfactory from the European point of view. Therefore the United Nations work on a second phase of this regulation. The focus of this work is on improving the BioRID dummy and on the definition of so called Seat Performance Criteria.

All discussions about the assessment of whiplash injuries within the framework of consumer information have in common, that the protection effect in a rear-end impact needs to be examined in an isolated vehicle seat by means of a sled test using a generic acceleration pulse. It turns out to be problematic, however, that presently there is no traumato-mechanical explanation of the phenomenon "whiplash injury" and that all the currently discussed dummy-criteria with the respective limit values follow a so-called "black-box approach". Experts try to correlate the measured dummy criteria with the findings from accident data and to thus derive limit values. In this context the available dummy-technology with the different measuring devices and criteria, as well as the proposed limit values are going to be presented.

In the last part of the seminar different seat design concepts (energy-absorbing, respectively geometry-improving), subdivided into active and passive systems will be introduced, and their advantages and disadvantages will be discussed.

Who should attend?

The seminar addresses development engineers who are new in the field of rear impacts or who have already got some experience in the field of safety, as well as developers of subassemblies which have to fulfill a crash-relevant function. It is furthermore especially interesting for project managers and managers who deal with the topic of rear-end impacts and who would like to obtain a better knowledge of this subject in order to use it for an improvement of procedures.

Course Contents

- Introduction into the characteristics of a rear-end impact
- Overview of the most important whiplash requirements
- Injury criteria
- Dummy-technology for rear impacts
- Presentation of the Euro NCAP and FMVSS 202-dynamic test procedures
- Outlook on possible harmonization-tendencies
- Explanation of the possible design measures in car seats



Thomas Frank (LEAR Corporation GmbH) joined the passive safety department of Lear Corporation in 2002 after graduating from the Technical University of Berlin in physical engineering sciences. At Lear Thomas Frank initially worked as a test engineer in crash testing, later he developed head rests. Today he is expert for low speed rear impact safety. In his position he guides the seat development with respect to meet whiplash protection requirements in regulations and consumer tests.

(enues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
- S	20.02.2017	2896	Alzenau	1 Day	740,- EUR till 23.01.2017, thereafter 890,- EUR	
Dates	04.09.2017	2897	Alzenau	1 Day	740,- EUR till 07.08.2017, thereafter 890,- EUR	





UPDATE

Child Occupant Protection Assessment in Euro NCAP

Protocol Version 7.1

Dynamic assessments

SafetyWissen by carhs

ΔFFT

Testing:

max, 49 points

Q6: The Q6 dummy shall be seated in an appropriate CRS for a six year old child or a child with a stature of 125 cm. This will be either the CRS recommended by the vehicle manufacturer, or if there is no recommendation, a suitable CRS from the top pick list.

Q10: The Q10 dummy shall be seated on a booster cushion only. This will be the booster cushion recommended by the vehicle manufacturer. Where the vehicle manufacturer recommends a high back booster with detachable backrest it will be used without backrest. If there is no recommendation for a booster cushion, one will be chosen by Euro NCAP from a list of suitable options contained in the Technical Bulletin TB012.

Preconditions: Where any of the following events occur zero points will be awarded to the dummy.

Frontal impact: During the forwards movement of the dummy only, the diagonal belt slips off the shoulder

Frontal impact: The pelvis of the dummy submarines beneath the lap section of the belt or the lap section prevents the dummy from moving upwards during rebound and is no longer restraining the pelvis.

Frontal and side impacts: The dummy pelvis does not remain in the booster seat /cushion and is not correctly restrained by the lap section of the seatbelt.

Frontal and side impacts: CRS does not remain within the same seating position or is no longer correctly restrained by the adult belt.

Frontal and side impacts: There is any breakage or fracturing of load-bearing parts of the belt system including buckles, webbing and anchorage points.

Frontal and side impacts: There is any breakage or fracturing of any seat belt lock-offs, tethers, straps, ISOFIX anchorages or any other attachments which are specifically used to anchor the CRS to the vehicle fail.

Modifier: If, during the forwards movement of the dummy, the diagonal belt moves into the gap between the clavicle and upper arm with folding of the belt webbing, a penalty of -4 points will be applied to the overall dummy score of the impact in which it occurs.

	Dummy	Region		Points	Criteria
	Frontal in	mpact (ODB)			
				4	$HIC_{15}^{-1} \le 500$, $a_{3ms} \le 87$ g
		Head		0	$HIC_{15}^{-1} \ge 700, a_{3ms} \ge 100 g$
		neau		- 2 (Modifier ²)	Head forward excursion > 450 mm
	Q6/			- 4 (Modifier)	Head forward excursion > 550 mm
	Q10	Neck		2	Upper Neck $F_z \le 1.7$ kN
nts		Neck		0	Upper Neck $F_z \ge 2.62$ kN
jod		Chest		2	a _{3ms} ≤41 g
max. 24 points		Chest		0	a _{3ms} ≥55 g
ma	Side imp	act (MDB)			
		Head		2	$HIC_{15}^{1} \le 500$, $a_{3ms} \le 72$ g
		riedu		0	$HIC_{15}^{-1} \ge 700, a_{3ms} \ge 88 g$
	Q6/	Neck		1	Upper Neck F _{res} < 2.4 kN (Q6) Upper Neck F _{res} < 2.2 kN (Q10)
	Q10	Neck		0	Upper Neck $F_{res} \ge 2.4$ kN (Q6) Upper Neck $F_{res} \ge 2.2$ kN (Q10)
		Chart		1	a _{3ms} < 67 g
		Chest		0	a _{3ms} ≥67 g
In	stallatio	on of CRS			
ä	Universa	I CRS		points	4
12	ISOFIX C	RS		points	2
max.	i-Size CRS	5		points	4
-	manufac	turer recommended CRS		points	2
Ve	hicle b	ased assessment			
Pre	condition	ns:			
Pro	vision of	three-point seat belts on all	passenger seats		
Tal	les in the	vehicle handbook stating cle	early, which seating positions are suitable or no	suitable for Univ	versal / ISOFIX / i-Size CRS
			d (both front and rear seats if applicable), the CF IOT suitable for any rearward facing CRS.	S tables in the ve	ehicle handbook must clearly indicate that when these
		bility of the 2nd row outboa R16 Annex 17 - Appendix 1	rd seats with Gabarit according to	points	1
ıts		bility of all other passenger s R16 Annex 17 - Appendix 1	eats with Gabarit according to	points	1
oints	2 costs w	ith i-Size and TonTether mar	king	noints	2

nts	UN ECE R16 Annex 17 - Appendix 1	points	1
jo	2 seats with i-Size and TopTether marking	points	2
. 13	3 independent seats with i-Size and TopTether marking	points	1
max	2 or more seating positions are suitable for fully independent use with the largest size of rearward facing (Class C) ISOFIX CRS, Fixture (CRF) ISO/R3,	points	1
	passenger airbag warning marking and manual / automatic disabling	points	2/4
	integrated CRS	points	1 (1 CRS) / 3 (2 or more CRS)

 $^1\,\mathrm{HIC}_{15}$ is only applied if there is hard head contact, otherwise the score is based on a_{3ms} only

² Q10 only







Child Occupant Protection Assessment in Latin NCAP Protocol Version 3.1

Requirements for points for Child Protection Rating: child seats (CRS) must be recommended by the vehicle manufacturer. CRS must be available for purchase from dealers, in the 3 big Latin NCAP markets (Argentina, Brazil, Mexico). CRS must be available at the 3 most important cities of each of the 3 big markets in at least 2 retailers per city. The CRS manufacturer must be officially represented locally in each one of the 3 big markets.

			essment	must be officially represented locally in each one	Dummy		1½	C	23					
	stra	ained	by any of the vehicle interface				ist not be parti	ally or wholly	unre-					
	Hea	ad Co	ntact with the vehicle: any he	ad contact with the vehicle results in 0 points fo	the head performance									
	Fro	ntal l	mpact											
	Hea	d			points	4	0	4	0					
10	E		no head contact with CRS head contact with CRS	no direct evidence + Head ^a res peak Head a _{res} 3ms	g	< 80 ≤ 72	≥ 88	< 96 ≤ 87	≥ 100					
max. 16 points	worst score from	For	ward Facing CRS		points	4	0	4	0					
6 pc	scol		forward head excursion	relative to Cr point	mm	≤ 549	≥ 550	≤ 549	≥ 550					
х. 1	orst	Rea	arward Facing CRS											
ma	3		head exposure	no compressive load on top of head, head fully restrained within CRS	points	4	0	4	0					
					points	2	0	2	0					
	Nec	:k		upper Neck F _z	kN	≤ 1.7	≥ 2.62	≤ 1.7	≥ 2.62					
	Che	st		a _{res 3ms}	g	≤ 41	≥ 55	≤ 50	≥ 66					
ix. 49 points max. 8 points		e Imp quire		:: head containment within shell of CRS, also th	ere must be no	o fracturing o	f the CRS							
2 8 :					points	4	0	4	0					
max. 49 points max. 8 point			no head contact with CRS head contact with CRS	no direct evidence + Head ^a res peak Head a _{res} 3ms	g	< 80 ≤ 72	≥ 88	< 80 ≤ 72	≥ 88					
Inst	allati	ion of	CRS											
13	CRS	from	the reference list		points		1	.0						
	CRS	recor	mmended by the manufacture	r	points			2						
Ve	hicle	Base	d Assessment											
	prov	ision	of three-point seat belts				not equipped or the vehicle I							
				Gabarit according to UN ECE R16.05	points			2						
			•	usly accommodate any reference list CRS	points		:	1						
Ę	3 se	ating	positions that can simultaneou	usly accommodate i-Size CRS	points		-	1						
points	2 pa		ger seats equipped with ISOFIX	0	points			1						
13			ese 2 passenger seats meet i-S	· ·	points		+	1						
max.			positions comply with require arward facing ISOFIX seats	ments for largest	points		:	1						
			nger airbag		points	2								
	pass	senge	r airbag warning and disabling		points	ints max. 4								
		•	ed CRS		points			1						
	1 int	tegrat	ed "Group I-III" CRS		points		-	1						

Child Occupant Protection Assessment in ASEAN NCAP COP Protocol Version 1.3

		Dyr	namic	assessment: Frontal Impact		Dummy	Q1	1/2	C	13
		Hea	ad			points	4	0	4	0
		ε		no head contact with CRS head contact with CRS	no direct evidence + Head ^a res peak Head a _{res} 3ms	g	< 80 ≤ 72	≥88	< 96 ≤ 87	≥ 100
	points	e from	For	ward Facing CRS		points	4	0	4	0
	5 po	score .		forward head excursion	relative to Cr point	mm	≤ 549	≥ 550	≤ 549	≥ 550
	x. 16									
49 points	тах.	ž		head exposure	no compressive load on top of head, head fully restrained within CRS	points	4	0	4	0
. 49						points	2	0	2	0
max.		Ne	:k		upper Neck Fz	kN	≤ 1.7	≥ 2.62	≤1.7	≥ 2.62
		Che	est		a _{res 3ms}	g	≤41	≥ 55	≤ 50	≥66
	÷	Dyr	namic	assessment: Side Impact						
	. 8 pt.	Hea	ad			points	4	0	4	0
	max.			no head contact with CRS head contact with CRS	no direct evidence + Head ^a res peak Head a _{res} 3ms	g	< 80 ≤ 72	≥88	< 96 ≤ 72	≥88
	12	Inst	allatior	n of CRS						
	m.	Voh		cod Accorcmont						





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Passenger Cars in Low-Speed Crashes

Course Description

In addition to the design of car structures for the protection of its occupants at high impact velocities, requirements and test procedures for collisions at low speeds, which massively influence the design of the vehicle front, were brought to the fore in recent years.

For the initial insurance classification of passenger cars classification tests of RCAR / AZT (impact speed up to 15 km/h) are used to determine standardized repair costs. To meet the insurance classification tests, many vehicles are equipped with cross member systems that feature energy absorbing elements (crash boxes), that can be connected via a detachable connection to the longitudinal members in the vehicle front.

Additional partly conflicting requirements are added through the EC Regulation 78/2009/EC and the NCAP tests for pedestrian protection. Compliance with the directive in the leg impact area is usually achieved by energy absorption in conjunction with a targeted support of the impacting leg in the immediate front area of the vehicle.

In connection with the design of vehicles for the different requirements, numerous conflicts occur, which often can only be solved at the expense of a non-optimum front end package or increased weight and manufacturing costs.

Additional requirements regarding the design of the vehicle front result from legislation for vehicle protection (UN R42, ...) and internal testing procedures of the manufacturer for ensuring management of everyday damages for his vehicles.

Course Objectives

In this seminar, you first get an overview on the requirements and regulations which have an impact on the design of cars for the various low-speed crash constellations. This is followed by a presentation of current energy management in the front body structure and an introduction of technical solutions. Based on the state of the art approaches of integral safety are discussed. Using interactive visualization of driving maneuvers, possibilities and limits of safety concepts, using e.g. precrash sensors and which could be implemented in the future, are discussed.

Who should attend?

The seminar is aimed at specialists from passenger car and light commercial vehicle development, engineers and technicians from simulation and testing, project engineers and managers who want to get an overview of the requirements and technological solutions for the development of passive and integrated safety systems for passenger cars in low-speed crash.

Course Contents

- Requirements and test procedures for low-speed crash
 - Introduction to the requirements for low-speed crash tests
 - Legal tests
 - Consumer protection tests
 - Other requirements
- Energy management and structural forces in the vehicle front
 - Load paths and structure loading
 - Connections to high-speed test
 - Workshop for analyzing crash data and the impact of structural design changes
 - Changes of structural design
 - Influence of crash sensing and restraint systems
- Design of passive systems
 - Conceptual solution approaches
 - Methods for system design
 - Conflicts of objectives
 - Technological feasibility and limits
- Discussion of integral safety systems
 - Simulation of driving maneuvers and time distance considerations
 - Potential of integrated solutions
 - Technological feasibility and limits



Prof. Dr. Harald Bachem (Ostfalia University of Applied Sciences) has been in charge of teaching and research in vehicle safety at the Ostfalia University of Applied Sciences since 2011. Prior to joining the university he held various management positions in industry where he was in charge of development and testing of vehicle safety functions. His last management position was head of cab body development at MAN Truck & Bus AG. Bachem is chairman of VDI Brunswick and vice chairman of the Wolfsburg Institute for Research, Development and Technology Transfer e.V.

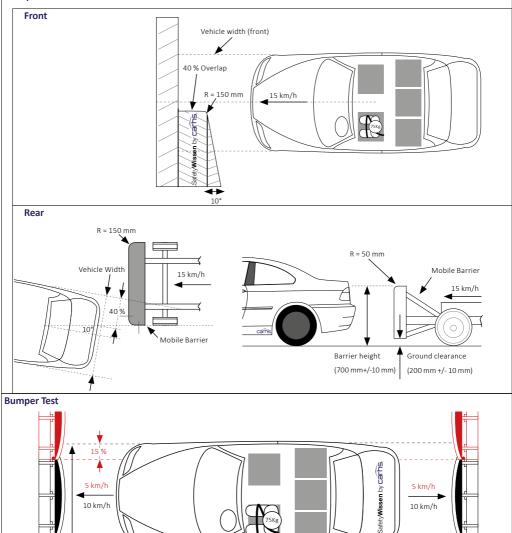
nues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
& Ve	08.03.2017	2815	Alzenau	1 Day	740,- EUR till 08.02.2017, thereafter 890,- EUR	
Dates	18.10.2017	2862	Alzenau	1 Day	740,- EUR till 20.09.2017, thereafter 890,- EUR	





RCAR Insurance Tests





Vehicle Width at Front Axle

Barrier ground clearance measured from the track surface to the lower surface of the bumper barrier:

Test	Ground Clearance	Remarks
Front 100%	455 ^{±3} mm	
Rear 100 %	$405^{\pm3}mm$ or $455^{\pm3}mm$	EU and Asia (AZT) 405 mm, USA (IIHS) 455 mm
Front / Rear 15 %	$405^{\pm3}mm$ or $455^{\pm3}mm$	Asia (IAG) and USA (IIHS) 405 mm





UN ECE Vehicle Classification

Consolidated Resolution on the Construction of Vehicles (R.E.3), Revision 4

Category	Wheels	Engine Capacity	Maximum Design Speed	Unladen Mass	Power	Seats	Maximum Mass
L1	2	≤ 50 cm³	≤ 50 km/h				
L2	3	≤ 50 cm³	≤ 50 km/h				
L3	2	> 50 cm ³	> 50 km/h				
L4	3 ¹	> 50 cm ³	> 50 km/h				
L5	3 ²	> 50 cm ³	> 50 km/h				
L6	4	≤ 50 cm³	≤ 45 km/h	≤ 350 kg ³	≤4 kW		
L7	4			≤ 400 kg ^{3,4}	≤ 15 kW		
Μ			Vehicles use	d for the carria	ge of passenger	ſS	
M1	≥4					≤ 9	
M2	≥ 4					> 9	≤ 5 t
M3	≥ 4					> 9	> 5 t
Ν			Vehicles u	ised for the cari	riage of goods		
N1	≥ 4						≤ 3.5 t
N2	≥ 4						3.5 t < m ≤ 12 t
N3	≥ 4						> 12 t
0			Trailer	s (including sen	ni-trailers)		
01							≤ 0.75 t
02							0.75 t < m ≤ 3.5 t
O3							3.5 t < m ≤ 10 t
04							> 10 t
Т			Agricu	Iltural or foresti	ry vehicles		
G				Off-Road vehic	les		

¹ asymmetrically arranged in relation to the longitudinal median plane

² symmetrically arranged in relation to the longitudinal median plane

³ not including the mass of the batteries in case of electric vehicles

 $^{4} \leq 550$ kg for vehicles intended for carrying goods

Applicability of selected UN Regulations to vehicle categories:

UN R	L1	L2	L3	L4	L5	L6	L7	M1	M2	M3	N1	N2	N3	01	02	03	04
11								•			•						
12								•			•						
14								•	•	•	•	•	•				
16		•		•	•	•	•	•	•	•	•	•	•	•	•	•	•
17								•	•	•	•	•	•				
21								•									
25		•		•	•	•	•	•	•	•	•	•	•				
32								•									
33								•									
42								•									
94								•									
95								•			•						
127								•			•						
135								•			•						
137								•							SafetyW	lissen by C	carhs.



Automotive Safety Summit Shanghai 2017

For the last 3 years **»SafetyTesting China«** has attracted more than 250 participants each year to discuss the latest requirements and innovations in testing of active and passive safety. The newly developed **»Automotive Safety Summit Shanghai«** continues the successful SafetyTesting series and expands the scope of the event to all aspects of automotive safety. Join **»Automotive Safety Summit Shanghai«** on August 1 - 2, 2017 at the Kerry Hotel in Pudong, Shanghai, China.

Keynotes from international experts, presentations on requirements and innovations, the latest developments in testing and simulation for active and passive systems will make this event a true highlight for every decision maker and engineer in the fields of active and passive safety. With the rapid rise of New Energy Vehicles (EV, PHEV and FCV), new challenges are surfacing for the safety community. The **»Automotive Safety Summit Shanghai«** is setting a focal point on **Safety of New Energy Vehicles**, discussing requirements, technologies and validation aspects for safety of NEVs.

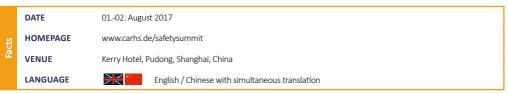


- Safety of New Energy Vehicles
- Global Legal and Consumer Requirements
- Pedestrian Safety
- Autonomous Emergency Braking
- Safety Testing and Simulation
- Safety in Autonomous Driving

A special session will be dedicated to Start-Ups in automotive Safety, featuring young companies with highly innovative ideas.

Who should attend?

»Automotive Safety Summit Shanghai« is addressing decision makers and engineers at all stages of the development phase, managers during the conceptual phase who need to understand upcoming global requirements, design engineers, testing and simulation specialists.















Introduction to Data Acquisition in Safety Testing

Course Description

Sensor technology and data acquisition are central elements of safety testing. A 100 % reliability of the used technology in combination with the highest accuracy of the employed sensors are the basis for the success and usefulness of the tests in vehicle development.

The course first presents a short overview on the historical development of data acquisition technology in the safety field and continues by going into details of current technologies of sensors, data acquisition as well as dummy and vehicle instrumentation.

Based on the procedures of a safety test, the different tasks of calibration and certification of sensors, filtering and evaluation of signals, as well as the calculation and evaluation of measurement errors will be explained.

The course provides the basic knowledge in crash data acquisition and gives a comprehensive overview on the procedures employed in data acquisition in the crash testing environment.

Course Objectives

The course participants will learn about the technology and terminology of sensor and data acquisition technology used in safety testing. They will be qualified to define tests, to supervise tests and to interpret and evaluate test results.

Who should attend?

This introductory course aims at new test engineers and project engineers as well as engineers from simulation departments at automotive OEMs, suppliers and engineering service providers.

Course Contents

- Sensors
 - Basic sensor principles
 - Sensors in safety testing
 - Selection of sensor systems
- Systems for data acquisition (DAS)
 - State of the art in DAS technology
 - InDummy and Onboard DAS
 - Filtering
- Instrumentation
 - Overview dummy instrumentation
 - Overview vehicle instrumentation
 - Overview instrumented barriers
- Evaluation & Measuring Errors
 - Error calculation (set-up of sensors, sensors, DAS, evaluation...)
 - Sources of errors in crash testing
 - Interpretation of signals
- Calibration and Certification
 - Dummy certification
 - Sensor calibration
 - SAE J211
- Procedures
 - Test preparation
 - Test execution
 - Test evaluation



Thomas Wild (Continental Safety Engineering International GmbH) studied Electrical and Tele-Communications Engineering at the Technical University Darmstadt. Since 1996 he has been employed at Continental Safety Engineering International as a measurement engineer. 1998 - 2001, he assumed additional responsibilities as an application engineer in the algorithm development. Since 2003 he is team leader measurement and video technology. Since 1997 he works in the working group Data Processing in Vehicle Safety (MDVFS).

nues	DATE	COURSE ID	VENUE	DURATION PRICE	LANGUAGE
& Vel	2728.04.2017	2929	Alzenau	2 Days 1.290,- EUR till 30.03.2017, thereafter 1.540,-	EUR
Dates	1920.10.2017	2930	Alzenau	2 Days 1.290,- EUR till 21.09.2017, thereafter 1.540,-	EUR



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CC 1540	1440 x 1024 @ 4000 fps
CC 2020	1920 x 1080 @ 2000 fps
CC 4010	2560 x 1600 @ 1000 fps

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Current Dummy Landscape

2017 2	G	TR	Α	US			A	sia						Am	erica						E	urop	e				
2017 2018 2019 2020 o = planned, no date specified	GTR 14 (Pole Side)	GTR 7	Australian NCAP	ADR (Frontal, Side)	ASEAN NCAP	Korean NCAP	China NCAP	China Regulations	JNCAP	Japan Regulations	Latin NCAP	IIHS	U.S. NCAP	FMVSS xxx (OMDB)	FMVSS 202a	FMVSS 213	FMVSS 214	FMVSS 208	Euro NCAP	UN R137	UN R135	UN R129	UN R44	UN R95	UN R94	Dummies	
o date specit		•	•	•	•	•	•	•	•	•	•	•	•					•	•	•					•	HIII 50 %	
fied			•			•	•		•				•					•	•	•						5 %	Frontal Impact
																			•							HIII 95 %	Impact
													•	0					•							THOR 50 %	
			•	•	•		•	•	•	•	•													•		ES-2	
													•				•									ES-2re	Side I
							•					•	•				•									SID-IIs	Side Impact
	•		•	•		•	•						•				0		•		•					World SID	
															•											HIII 50 %	Rearl
		•	•			•	•		•			•							•							BioRID II	Rear Impact
																•		•								Crabi	
																•										Cami	•
	Safety															•		•								H	Child
	SafetyWissen by carhs.		•				•									•							•			P Series	
	arh <u>s</u>		•		•	•	•				•					0			•			•	0			Q Series	

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THOR 50 % Male: Injury Criteria and Risk Functions

Region	Criterion	Calculation	Risk Function			
	HIC ₁₅ (-)	$\left (t_2 - t_1) \left[\frac{1}{(t_2 - t_1)} \int_{t_1}^{t_2} a(t) dt \right]^{2.5} \right _{max}$	$p(AIS \ge 3) = \Phi \left[\frac{\ln(HIC_{15}) - 7.45231}{0.73998} \right]$			
Head	Brain Injury Criterion BrIC (-)	$\begin{split} \sqrt{\left(\frac{\max(\omega_x)}{\omega_{xc}}\right)^2 + \left(\frac{\max(\omega_y)}{\omega_y}\right)^2 + \left(\frac{\max(\omega_z)}{\omega_{zc}}\right)^2} \\ \text{with } \omega_{[x,y,z]} = \text{Anguar velocity } (\text{rad/s}) \\ \omega_{xC} = 66.25 \text{ rad/s} \\ \omega_{yC} = 56.45 \text{ rad/s} \\ \omega_{zC} = 42.87 \text{ rad/s} \end{split}$	$p(AIS \ge 3) = 1 - e^{-\left(\frac{BTRC}{0.3907}\right)^{2.84}}$			
Neck	N _{ij} (-)	$\label{eq:Fz} \frac{F_z}{F_{zc}} + \frac{M_y}{M_{yc}}$ with FzC = 2520 N/-3640 N (tension/compression) M_VC = 48 Nm/-72 Nm (flexion/extension)	$p(AIS \ge 3) = \frac{1}{1 + e^{3.227 - 1.969N_{ij}}}$			
Chest	Multi-point Thoracic Injury Criterion R _{max} (mm)	$\begin{split} & max(UL_{max}, UR_{max}, LL_{max}, LR_{max}) \\ & \text{with} \\ & [U/L R/L]_{max} \\ & = max\left(\sqrt{[L/R]X_{[U/L]S}^2 + [L/R]Y_{[U/L]S}^2 + [L/R]Z_{[U/L]S}^2 + [L/R]Z_{[U/$	$\begin{split} P(AIS \geq 3 age, R_{max}) \\ &= 1 - exp\left(-\left[\frac{R_{max}}{exp(4.4853 - 0.0113age)}\right]^{5.03896}\right) \end{split}$			
Abdomen	Compression A _{max} (mm)	$\frac{\max(\delta L, \delta R)}{d_{abd}}$, with $\delta[L/R]: \text{Peak X-axis deflection of the [left / right]}$ $abdomen$ $d_{abd} = 238.4 \text{ mm}$	$p(AIS \ge 3) = 1 - e^{-\left(\frac{A_{max}}{0.4247}\right)^{26719}}$			
Pelvis	res. Actetabulum Load F _R (kN)	$\sqrt{F_x^2 + F_y^2 + F_z^2}$	$p(AIS \ge 3) = \Phi\left[\frac{\ln(F_R/0.72) - 1.6526}{0.1991}\right]$			
Femur	Axial Load F _z (kN)	-	$p(AIS \ge 2) = \frac{1}{1 + e^{5.7949 - 0.5196F_x}}$			
Tillia	Revised Tibia Index RTI (-)	$\frac{F}{F_c} + \frac{M}{M_c}, \text{ with}$ $F_C = 12 \text{ kN}$ $M_C = 240 \text{ Nm}$	$p(AIS \ge 2) = 1 - exp\left(-exp\left[\frac{ln(RTI) - 0.2468}{0.2728}\right]\right)$			
Tibia	F _{z,upper} (kN)	-	$p(AIS \ge 2) = \frac{1}{1 + e^{5.6654 - 0.8189F_x}}$			
	Fz,Iower (kN)		$p(AIS \ge 2) = \frac{1}{1 + e^{4.572 - 0.670F_z}}$			
Faat	M _{y,ankle} (Nm)	$\begin{split} M_{\gamma}-F_{x}D-\frac{ma_{x}D}{2} &, \text{with} \\ M_{\gamma}(\text{Nm}), F_{x}(\text{N}) \text{ of the lower tibia load cell} \\ a_{x}(m/s^{2}) \text{ of the tibia} \\ D = 0.0907 \text{ m} \\ m = 0.72 \text{ kg} \end{split}$	$p(AIS \ge 2) = \frac{1}{1 + e^{6.535 - 0.1005M_y}}$			
Foot	M _{z,ankle} (Nm)	$M_x - F_y D - \frac{ma_y D}{2}$, with $M_x(Nm)$, $F_y(N)$ of the lower tibia load cell $a_y(m/s^2)$ of the tibia D = 0.0907 m m = 0.72 kg	$p(AIS \ge 2) = \Phi\left[\frac{M_x - 40Nm}{10Nm}\right]$			

Source: Saunders, Parent, Ames; NHTSA OBLIQUE CRASH TEST RESULTS: VEHICLE PERFORMANCE AND OCCUPANT INJURY RISK ASSESSMENT IN VEHICLES WITH SMALL OVERLAP COUNTERMEASURES; ESV 2015; Paper Number: 15-0108





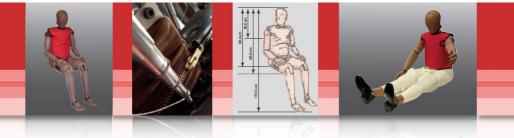


You have a challenge? We have a solution!

HIGH VOLTAGE TESTINGVEHICLE SAFETYcomponentsdummy servicesanalysisENVIRONMENTAL SIMULATIONCONSULTINGLABORATORIESSPECIAL TEST CONFIGURATIONENDURANCE STRENGTH AND DURABILITYtestingdisperse testsMOTORSPORTtest technologyTRAININGSconstruction

New employee @ACTS: THOR-M 50th dummy

- Operation required as of 2018:
 - US NCAP Full frontal
 - US NCAP Oblique offset moving deformable barrier impact test
- Replaces the HIII 50th dummy



www.acts.de www.magna.com



Praxis Conference

A new generation of crash test dummies is entering the market. THOR, World SID and Q-Dummies replace older dummy models. This brings some challenges:

- The new dummies require significant adaptations of restraint system, vehicle interiors and vehicle structures.
- The calibration and certification of the new dummies is much more demanding for the laboratories.
- The handling of the new and more complex dummies with their digital instrumentation and new sensors require entirely new processes and intensive training of the technical staff.
- Validated and robust CAE models of the new dummies are required to perform meaningful and reliable simulations.

The new PraxisConference Crash Dummy, jointly organized by BGS Böhme & Gehring and carhs.training, is dedicated to these issues. It brings together users and developers, and sees itself as a communication platform for experts.

A highlight of the event is the hands-on praxis session in the laboratory of the German Federal Highway Research Institute (BASt) where topics such as dummy seating, calibration, measurement, mounting and handling are shown in practice and attendees can gain hands-on experience.

Who should attend?

The PraxisConference is aimed at everyone who has to deal with the new dummy generations:

- Technicians from crash test, sled test or dummy labs
- Simulation engineers
- Developers of restraint systems, interior components or vehicle structures
- Developers of dummies and dummy simulation models who want to get in touch with users







	DATE	11 12. October 2017	
	HOMEPAGE	www.carhs.de/pkcd	Co-hosted with
Facts	VENUE	Bundesanstalt für Straßenwesen, Brüderstraße 53, 51427 Bergisch Gladbach	BGS
	LANGUAGE	German with simultaneous translation into English	
	PRICE	1.450,- EUR till 13.09.2017, thereafter 1.690,- EUR	BGS Böhme & Gehring GmbH

Test

Innovation

Test

Design

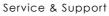
Test

Process

Test

Service







Adult ATDs



Child ATDs



Load Cells



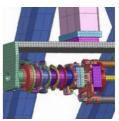
Test Fixtures



DAS Integration



Pedestrain Testing



FEA Models



Putting Safety to the Test www.humaneticsatd.com



Overview Dummies Weights, Dimensions and Instructions for Calibration

Adult Dummies for Frontal / Rear Impact



UPDATE

	Weight (kg)	Seating Height (cm)	Instruction for Calibration		
Hybrid II 50 % Male	74.4	90.7	CFR 49 Part 572, Subpart B		
Hybrid III 5 % Female	49.1	78.7	SAE Engineering Aid 25 CRF 49 Part 572, Subpart O		
Hybrid III 50 % Male	77.7	88.4	CFR 49 Part 572, Subpart E 1999/98/EG		
Hybrid III 95 % Male	101.2	93.5	SAE Engineering Aid 26		
BioRID II	77.7	88.4	User Manual		

Adult Dummies for Side Impact



	Weight (kg)	Seating Height (cm)	Instruction for Calibration
Eurosid 1	72.0	90.4	Eurosid 1 Certification Procedure 96/27/EG, UN R95
ES-2	72.0	90.9	FTSS- User Manual / UN R95
ES-2 re	72.0	90.9	CFR 49 Part 572, Subpart U
US-SID	76.7	89.9	CFR 49 Part 572, Subpart F
US-SID/Sid-H3	77.2	89.9	CFR 49 Part 572, Subpart M
SID IIs	44.5	79.0	CFR 49 Part 572, Subpart V
WorldSID 5 % Female	48.27		User Manual
WorldSID 50 % Male	74.88	87.0	User Manual

Child Dummies



	Weight (kg)	Seating Height (cm)	Instruction for Calibration
P0, P¾, P6, P10	3.4-32.0	34.5-72.5	User Manual
P3	15.0	56.0	User Manual
P1½	11.0	49.5	P1½ User Manual
Q1	9.6	47.9	Q1 User Manual
Q1½ (18m)	11.1	49.9	Q1,5 User Manual
Q3	14.5	54.4	Q3 User Manual
Q6	23.0	63.6	Q6 User Manual
Q10	35.5	73.4	Q10 User Manual (Rev. A Draft)
CRABI 12m	10.0	46.4	CFR 49 Part 572, Subpart R
Hybrid II - 3 y/o	15.1	57.2	CFR 49 Part 572, Subpart C
Hybrid II - 6 y/o	21.5	64.5	CFR 49 Part 572, Subpart I
Hybrid III - 3 y/o	16.7	54.6	CFR 49 Part 572, Subpart P
Hybrid III - 6 y/o	23.4	63.5	CFR 49 Part 572, Subpart N
Hybrid III - 10 y/o	35.2	72.39	CFR 49 Part 572, Subpart T

Testing Services

Fullscale crash facility Road restraint system tests Testing bridge Sled tests Structure deformation tests

Engineering

UFO – Ultra Flat Overrunable Robot Driving Robot ASIS – Advanced Side Impact System ConAS– Controlled Application for Structure Deformation MCB – Moveable Crash Block



testing

DSD







passion for crash



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- DAkkS CERTIFIED CALIBRATION LAB

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Dummy – Trainings

Course Description

The seminars give you the opportunity to gain efficiency and security in the use and handling of dummies.

After a short theoretical introduction you are going to be trained in the handling of the respective dummy-type in a dummy lab in practical exercises in work groups.

Course Contents

- Introduction of the respective dummy-type History, development, assemblies, standard instruments, optional measuring points, recent modifications, regulations for application/test, calibration
- Complete disassembly of the dummies in work groups
 Explanation of the functions of the assemblies and the individual parts, special features, deviations from other dummy-types, practical hints for the handling of individual assemblies, sensors and cabling, special tools, other devices, cleaning
- Complete assembly of the dummies in work groups work steps, possible assembly errors, mounting of the sensors, cabling, adjustments of joints, storing/transport
- Dummy calibration
 Demonstration and explanation of the calibration tests

Course Objectives

- Efficiency and security in use and handling of dummies
- Exact knowledge about assembly, mechanics and sensor positions
- Understanding of the measuring possibilities and limits

Who should attend?

Project and test engineers, technicians, mechanics







DUMMY	Hybrid III 5%	%, 50% , 95%			
DATE	0910.02.17	2526.09.17			
COURSE ID	2961	2962			
PRICE	1.290,- EUR (each)				
DUMMY	THOR				
DATE	2728.03.17	0405.12.17			
COURSE ID	2977	2978			
PRICE	1.490,- EUR (each)				
DUMMY	BioRID II				
DATE	1516.02.17	1718.10.17			
COURSE ID	2965	2966			
PRICE	1.290,- EUR (each)				
DUMMY	WorldS	ID 50%			
DATE	2021.03.17 27				
COURSE ID					
PRICE	1.490,- EUR (each)				
DUMMY	ES-2 / ES-2re				
DATE	0708.03.17	1415.11.17			
COURSE ID	2971	2972			
PRICE	1.290,- El	JR (each)			
DUMMY	SID IIs				
DATE	1415.03.17	2122.11.17			
COURSE ID	2973	2974			
PRICE	1.290,- EU	JR (each)			
DUMMY	P-/Q-Child	l Dummys			
DATE	20.02.17	07.11.17			
COURSE ID	2967	2968			
PRICE	740,- EU	R (each)			
DUMMY	Q6 /	Q10			
DATE	21.02.17	08.11.17			
COURSE ID	2969	2970			
PRICE	740,- EU	R (each)			
DUMMY	Hybrid III 3 & 6 y/o				
DATE	13.02.17	27.09.17			
COURSE ID	2963	2964			
PRICE	740,- EUR (each)				
VENUE	Bergisch Gladbach				
LANGUAGE					

Dummy Specialists, BGS Böhme & Gehring GmbH

BGS operates the dummy calibration laboratory of the German Federal Highway Research Institute (BASt). BGS calibrates crash test dummies for the automotive industry. The seminars are held by experienced engineers from BGS' team.

Instructors



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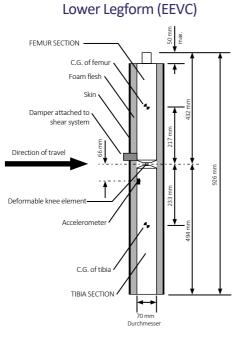
www.safetywissen.com





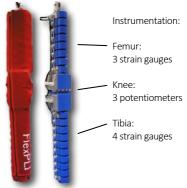


Impactors for Pedestrian Protection



LengthDiameterMass926 mmca. 132 mm13.4 kg

Flexible Pedestrian Legform Impactor: Flex PLI

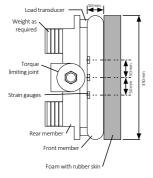


Proposed criteria and limits for Flex PLI:

Criterion	Limit	
Tibia bending Moment	340 Nm (380 Nm in exception zone)	
MCL Elongation	22 mm	
ACL / PCL Elongation	13 mm	

Length	Diameter	Mass
975 mm	132-140 mm	13.4 kg

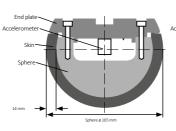
Upper Legform

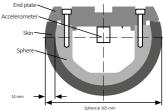


350 mm ca. 155 mm 11 - 18 kg	Length	Width	Mass
	350 mm	ca. 155 mm	11 - 18 kg

Adult Headform Impactor

Child Headform Impactor





SafetyWissen by Carhs.

	Diameter	Mass		Diameter	Mass
Adult Headform	165 mm	4.5 kg	Child Headform	165 mm	3.5 kg

more on pedestrian protection <a> page 78

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Pedestrian Protection - Test Procedures

Course Description

A basic prerequisite for successful implementation of pedestrian protection is a detailed knowledge of test requirements. This seminar provides the complete knowledge regarding the test methods as defined by the EU Directive on pedestrian protection and Euro NCAP's pedestrian protection assessment in theory and praxis.

Compact presentations explain the basics and technical details of the regulation and the test protocols. Practical exercises the BASt's test laboratory include test preparation, vehicle marking, selection of test points, handling of the impactors and the actual testing with head and legform impactors.

Course Contents

- Basics and current status of the regulations (presentations)
- Euro NCAP Rating (presentation)
- Test preparation according to Euro NCAP Testing Protocol and EU Directives (practical exercises)
- Test demonstrations: Head, Upper Legform and Legform impact (demonstrations and practical exercises)
- Discussion

Who should attend?

- Project-, test- and simulation engineers,
- Technicians, mechanics

Venues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
60	2527.04.2017	2993	Bergisch Gladbach	3 Days	1.790,- EUR	
Dates	1921.09.2017	2994	Bergisch Gladbach	3 Days	1.790,- EUR	

Pedestrian Protection Workshop: Flex PLI

Course Objectives

- Detailed Knowledge of the new Impactor
- Experience with Handling and Usage of the Impactor
- Understanding of the Impactor's Functionality

Course Contents

- History, Biomechanics, Evaluation, Legislation
- Assembly, Transducers, Onboard Data Acquisition, Technical Details
- Disassembly along with Comments on Function of Components

- Assembly along with practical Tips and Pointers to Specialities and possible Mistakes
- Adjustments of the Compound Springs, Clamping Bolts, Stopper Cables, etc.
- Demonstration of both Certification Procedures
- Data Analysis and Interpretation of Test Results

Who should attend?

- Project-, test- and simulation engineers,
- Technicians, mechanics

Venues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
త	06.04.2017	2999	Bergisch Gladbach	1 Day	740,- EUR	
Dates	14.09.2017	3000	Bergisch Gladbach	1 Day	740,- EUR	

Pedestrian Protection Workshop: Test Areas and Test Points

Course Objectives

- Experience with the new Vehicle Markup
- Certainty in its Application
- Deep Understanding of the Procedure

Course Contents

- Basics, Background and Development of the Procedure
- Test Area Determination, Borders, Exemption Zones, Special Cases
- Necessary Laboratory Equipment, Helpful Tools

- Exemplification by a complete Mark-up of a Vehicle
- Color Scheme, Manufacturers Predictions, allowed Tolerances
- Default Green / Default Red Definitions
- Result Analysis, Point Assessment
- Adaption of the Principle to Upper- and Lowerleg Areas

Who should attend?

- Project-, test- and simulation engineers,
- Technicians, mechanics

nues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
& Ve	05.04.2017	2997	Bergisch Gladbach	1 Day	740,- EUR	
Dates	13.09.2017	2998	Bergisch Gladbach	1 Day	740,- EUR	

Active Safety & Driver Assistan



Introduction to Active Safety of Vehicles

Course Description

Increasing demands on the protection of vehicle occupants have led to a continuous reduction in the number of injured and killed persons. While more than 20,000 persons have been killed on German roads in the early 1970s, this number is now well below 4,000. Passive safety, i. e. measures which are designed to minimize the consequences of an accident, has made a significant contribution to this achievement.

While the potential of passive safety is considered to be largely exhausted and huge efforts are required to achieve further progress in occupant protection, active safety has become increasingly important in recent years. Active Safety means measures which prevent an accident or at least reduce the collision speed and thus the energy input.

While technologies such as ABS or ESP have been established years ago and have proven their effectiveness, new techniques such as the emergency brake or the lane keeping assist and numerous other driver assistance systems are just entering the market. It can be assumed that these systems will be widely used in the next few years and will lead to a further decrease in the number of traffic victims.

Automated driving can be seen as the next step of active safety. Although there is still a lot of development needed in this area, it can be assumed that vehicles which will driven at least partially automatically in certain traffic scenarios will enter the market over the next ten years.

In the seminar first a brief introduction to active safety, in contrast to passive safety is given. This is followed by a presentation of current active safety systems and an overview of the requirements of legislation and consumer protection organizations. In addition, current and upcoming developments in the area of driver assistance systems and automated driving are presented.

Who should attend?

The seminar is aimed at new and experienced engineers working in the field of active vehicle safety in research and development departments of automotive OEMs or suppliers, as well as for all other interested parties, which want to receive an overview of current and future developments in the areas of active vehicle safety, driver assistance and automated driving.

Course Contents

- Fundamentals of active safety
 - Basic principles of action
 - Legal requirements
 - Euro NCAP requirements
- Current active safety systems
 - ABS
 - ESC
 - Brake assist
 - Pre-crash systems
 - Driver assistance systems
 - Basic requirements and design strategies
 - Current and future driver assistance systems
 - Automated driving
 - State of the art
 - Opportunities and risks
 - Human machine interface
 - Market introduction strategies



Dr. Gerd Müller (Technical University of Berlin) has been working at the department automotive technology of the Technical University of Berlin since 2007. From 2007 to 2015 he was a research assistant. Since 2015 he has been a senior engineer of the same department. His research focuses on vehicle safety and friction coefficient estimation. Dr. Müller gives the lecture "Fundamentals of Automotive Engineering" and conducts parts of the integrated course "Driver Assistance Systems and Active Safety".

nues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
& Vel	08.05.2017	2944	Alzenau	1 Day	740,- EUR till 10.04.2017, thereafter 890,- EUR	
Dates	17.11.2017	2945	Alzenau	1 Day	740,- EUR till 20.10.2017, thereafter 890,- EUR	

Euro NCAP





NCAP Tests for Active Safety and Driver Assistance

Safety Assist Assessment based on:

- Seat Belt Reminder (SBR):
 - On all front row seats 2 Points
 - additionally on all rear seats 1 Point
 - Speed Assist Systems (SAS)



		SLIF Speed Limit Information Function	MSA Manual Speed Assistance	ISA Intelligent Spee Assistance
Communicating Speed Limit	Subsign recognition (conditional speed limits):			
camera based	no	0.25 Points		0.25 Points
camera paseu	yes	0.5 Points		0.5 Points
map based	no	0.25 Points		0.25 Points
map based	yes	0.5 Points		0.5 Points
combined	no	0.75 Points		0.75 Points
combined	yes	1 Point		1 Point
Warning Function			0.5 Points	1 Points
Speed Limitation	precision -10/+0 km/h		0.75 Points	0.75 Points
speed Limitation	precision -5/+0 km/h		1 Point	1 Point
 Test speed 72 km LDW Systems: 1. lane marking: lateral velociti 	st (VUT) leaves straight line path 1/h			e path
 LKA Systems: 1 P lane marking: 	oint solid line		∫1LC/ ≦ -0.5 III	
	es 0.1 - 1.0 m/s in 0.1 m/s steps riterion: Distance to Line Crossin		f 5 tests at lateral velocities	between 0.1 0.5 m/s
 Assessment c 	iterion. Distance to Life Crossin	$ g(D) C \le -0.4 \text{ III III } 5 \text{ OUL } 0$	I D LESIS AL IALEI AI VEIOCILIES	between 0.1 - 0.5 m/s

- HMI: Default ON (0.2 Points), Haptic/supplementary warning (0.2 Points), Blind Spot Monitoring (0.1 Points): Total: 0.5 Points
- AEB Inter-Urban: max. 3 Points more ⊃ page 126
- AEB City: max. 3 Points (as part of the Adult Occupant assessment) more 2 page 120
- AEB VRU Pedestrian: max. 6 Points (as part of the Pedestrian Protection assessment) more 2 page 122
- Planned extensions:
 - additional scenarios for AEB City / AEB Inter-Urban (starting 2018): Variation of impact point / angle
 - Extension of the Lane Support Systems assessment in the areas "Run Off Road / Road Edge Detection (starting 2018). Higher total score available: 4 Points.
 - AEB VRU Cyclist (as of 2018): max. 6 Points (as part of the Pedestrian Protection assessment)
 - Junction Assist (as of 2020)
- NCAP Seat Belt Reminder compliant with FMVSS 208 as a prerequisite for 3 or more stars
 - ABS as a prerequisite for 3 or more stars
 - ESC compliant with GTR 8 as a prerequisite for 4 or more stars

Safety Assist Technology (SAT) Assessment

(Weighting: 25 % of the overall rating)

- Effective Braking & Avoidance (EBA): ABS / ESC: 8 Points
- Seat Belt Reminder Driver / Passenger (with seat occupancy detector) / rear seats: 6 Points
- Blind Spot Technology: 2 Points
- Advanced SAT: AEB, LKA, LDW, FCW etc.: 2 Points more 🗢 page 45

Get familiar with all NCAP tests in just 2 days with our Seminar: NCAP - New Car Assessment Programs: Tests, Assessment Methods, Ratings learn more on ∋ page 118

more 🗢 page 44

Latin I

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SAFETY WISSEN

NCAP Tests for Active Safety and Driver Assistance

	planned for 2018 (MY 2019):	· · · ·						
	 Crash Avoidance Rating cons Forward Collision Warnin 		age 130		Crash Avoida	nce Rating ((as of 2018)	
	 Crash Imminent Braking: 12 Points more ⊃ Page 130 Dynamic Brake Support: 11 Points 				Stars	require	ed points of 100)	
CAP	0 0	8 8 4 4				٤	80	
U.S. NCAP	 Semi-automatic headligh Amber rear turn signal: 6 		****	(60			
	Lane Departure Warning	7 Points			***	4	40	
	 Blind Spot Detection: 8 Pe Assessment of the risk for 		v Factor SSF): 20	Points	**	2	20	
	additionally as part of the peo				*		0	
	AEB Pedestrian	Page 128						
	 AEB (part of the Top Safe approach to standing veh assessment of the speed 	icle at 20 km/h and 40 km						
		20 km/h T			40 km/			
	Speed reduction Points	< 8 km/h 8-14 km/ 0 1	/h ≥ 15 km/h 2	< 8 km/h 0	8-14 km/h 1	15- 34 km/h 2	≥ 35 km/h 3	
s	 1 additional point for FCV 	/ (Forward Collision Warni	ng) meeting the U.	S. NCAP crite	ria			
IIHS	 Rating scheme: 							
	Points							
	Rating	BASIC	ADVANCED	S	UPERIOR			
	 Advanced Lighting (part of Assessment of the illumin systems that automatical 	ation and glare of high and	d low beam headlig	ghts in various	s test scenarios	. Additional cr	edit is given for	
JNCAP	 SBR: 8 Points Advanced Safety Award, AEB (similar to Euro NCAF AEB Pedestrian (day time LDW (at 60 and 70 km/h) Rear View Monitor: max. ASV+ Award for cars achi ASV++ Award for cars achi 	P AEB Inter-Urban, max 60 I: max. 25 Points I: max. 8 Points 6 Points eving > 12 Points	km/h without CCR	b scenario): n	nax. 32 Points			
KNCAP	 Braking Performance Tests: Measurement of the stopping distance from 100 km/h on dry and wet road. Check if vehicle stays within the 3.5 m wide track while braking: 5 Points Basic Active Devices: FCWS, LDWS, SLD, SBR front, SBR rear: 0.5 Points each AEB Inter-Urban: 1 Points AEB Inter-Urban: 1 Points Additional Active Devices (optional): Max. total points for Additional Active Devices = 2 Points ASCC, BSD, RCTA, LKAS, ISA: 0.5 Points each AEB Predestrian, Advanced Airbag: 1 Point each 							
C-NCAP	Active Safety Assessment pla ESC: 4 Points AEB/FCW Car to Car Rear		hting: 15 % of th	ie overall ra	ting): more a	⊃ Page 54		
	 AEB Pedestrian: 3 Points 							







How can you protect yourself

> if you can't see everything?

INTEGRATED SAFETY BY NATURE

Bat: mammal of the order Chiroptera (/kai'roptərə/; from the Greek $\chi\epsilon$ (ρ - cheir, "hand" and $\pi\tau\epsilon\rho$ óv - pteron, "wing"). Bats use sensory techniques like echolocation, smell, hearing and the ability to detect ultraviolet light to detect, localize, and classify prey while avoiding collisions with other bats.







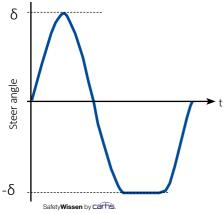
Test of ESC Systems in UN R13H (R140), GTR 8 and FMVSS 126

Step 1: Slowly-Increasing-Steer Manoeuvre to determine parameter A

At a constant velocity of 80 ± 2 km/h the steering angle is ramped at 13.5 deg/s until a lateral acceleration of 0.5 g is reached. Out of 2 series (1x left turn / 1x right turn) with 3 repetitions of the manoeuvre the steering angle A (in degrees) at which the lateral acceleration is 0.3 g is determined using linear regression.

Step 2: Sine with Dwell Manoeuvre to assess Oversteer Intervention and Responsiveness

At a velocity of von 80±2 km/h the vehicle is subjected to two series of test runs using a steering pattern of a sine wave at 0.7 Hz frequency with a 500 ms delay beginning at the second peak amplitude:

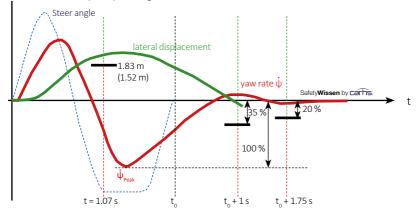


One series uses counterclockwise steering for the first half cycle, and the other series uses clockwise steering for the first half cycle. In each series of test runs, the steering amplitude is increased from run to run, by 0.5 A, starting at 1.5 A. The steering amplitude of the final run in each series is the greater of 6.5 A or 270 degrees, provided the calculated magnitude of 6.5 A is less than or equal to 300 degrees. If any 0.5 A increment, up to 6.5 A, is greater than 300 degrees, the steering amplitude of the final run is 300 degrees.

Performance Requirements:

Yaw Rate

- 1 s after completion of the steering input (t₀) < 35 % of the first peak value of yaw rate recorded after the steering wheel angle changes sign.
- 1.75 s after completion of the steering input (t₀) < 20 % of the first peak value of yaw rate recorded after the steering wheel angle changes sign.
- Lateral displacement of the vehicle center of gravity with respect to its initial straight path when computed 1.07 seconds
 after the Beginning of Steer (BOS)
 - for vehicles with GVM (GVWR) \leq 3500 kg > 1.83 m
 - for vehicles with GVM (GVWR) > 3500 kg > 1.52 m





Autonomous Driving, Advanced Driver Assistance, and Accident Avoidance: Technologies, Scenarios, Legislation, Challenges

Course Description

With the increasing market penetration of Advanced Driver Assistance Systems (ADAS), some of the latest car models offer automated driving in specific traffic scenarios. These partially automated systems, however, must be supervised permanently by the driver. Highly automated systems where the driver must take-over the vehicle control only on request, are expected already in the near future, with the focus on automated driving in traffic jams and on the highway. While the regulatory framework is aborning, major need for action is the so-called backend providing not only highly accurate and actual digital map data, rather the release of the autopilot on specific routes and information about eventual hazards.

In addition to these autopilots in series production vehicles enabling temporarily autonomous driving in specific traffic scenarios under certain circumstances, IT companies, Google first and foremost, as well as carpool services such as Uber, are developing and testing driverless cars. Even some OEMs (Volvo, Ford) have announced to develop self-driving cars for passenger transportation like taxis or shuttle busses. Due to the enormous cost savings by eliminating the driver, significantly more expensive and increasingly powerful technologies can be used in these vehicles, i.e. a 360° high-resolution laser-scanner.

An essential objective of autonomous driving is the reduction and avoidance of accidents. Based on accident analysis, the potential to this effect, both of ADAS and autopilots, is estimated, including the remaining or insufficiently addressed gaps.

The seminar describes and explains in detail the existing and anticipated ADAS, autopilots and accident avoidance systems with a specific focus on the sensors, communication systems and algorithms used, such as artificial intelligence. In particular, the leap from partial to high automation is highlighted, including the technical gaps, the system boundaries, the requirements of functional safety and system validation are discussed. Furthermore, the potential impact on occupant protection systems along with synergies between active and passive safety are touched. Particularly challenging is the re-transition of the vehicle control from the autopilot to the driver. In this context, the importance of the human-machine interface (HMI) along with driver monitoring systems are illustrated. Last, but not least, the legal challenges to automated driving are highlighted, the vehicle certification requirements in particular.

Who should attend?

This seminar offers an introduction in all aspects of automated driving. As a result, it is useful to all experts working in research and development of ADAS, automated driving and active safety, including sensors, algorithms, human machine interface, communication systems, vehicle interior design, future mobility and traffic concepts.

In particular, the seminar addresses technicians, system and component engineers, project engineers and managers in the automotive industry, both vehicle manufacturers and suppliers who are interested in the actual and future technologies of automated driving and active safety.

Course Contents

- Overview of market trends, the requirements of legislation and consumer ratings
- Advanced Driver Assistance Systems: Functions and technologies
- Motivation, Drivers and benefits of automated driving
- Scenarios of automated driving, the leap from partial to high automation
- Technologies and sensors used, technical gaps and boundaries
- Legal and other challenges, system validation and driver monitoring in particular
- Accident avoidance systems and technologies, the potential of ADAS and autopilots to this effect
- Not yet sufficiently addressed gaps in accident scenarios and accident root causes, based on accident analysis
- Synergies between active and passive safety (Integrated Safety)

lest se ti ti ti ti ti w w

Dr. Lothar Groesch has been working in safety engineering for more than 40 years, both at one of the leading OEMs in Passive & Active Safety, and with a major supplier in pioneering new automotive safety sensors & systems. From 2000 to 2009, he worked in the United States as a Product Director for Automotive Safety Systems, thus he is particularly familiar with U.S. specific requirements. Although he only joined the carhs team quite recently, he has a long experience in guest teaching at several universities in the U.S. & Germany, as well as in company internal training seminars, technical marketing, customer presentations & workshops. In 2009 Dr. Grösch has founded Groesch Automotive Safety Consulting and is primarily working in driver assist and accident avoidance systems.

nes	DATE	COURSE ID	VENUE	DURATION	I PRICE	LANGUAGE
Venu	0607.04.2017	2902	Alzenau	2 Days	1.290,- EUR till 09.03.2017, thereafter 1.540,- EUR	
es &	0304.07.2017	2866	Alzenau	2 Days	1.290,- EUR till 05.06.2017, thereafter 1.540,- EUR	
Dates	0910.11.2017	2867	Alzenau	2 Days	1.290,- EUR till 12.10.2017, thereafter 1.540,- EUR	



SAFETY WISSEN

NEW



Levels of Driving Automation according to BASt, SAE and NHTSA definitions

						Execution of Steering and Acceleration/ Deceleration
						Monitoring of Driving Environment
						Fallback Performance of Dynamic Driving Task
All driving modes	Some driving modes	Some driving modes	Some driving modes	Some driving modes		System Capability
	Fully automated	Highly automated	Partially automated	Assisted	Driver Only	BASt Level
5 Full Automation	4 High Automation	3 Conditional Automation	2 Partial Automation	1 Driver Assistance	0 No Automation	SAE Level
3/4 Limited Self Driving Automation / Automation 116		3 Limited Self Driving Automation	2 Combined Function Automation	1 Function Specific Automation	0 No Automation	NHTSA Level

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- Braking: R90, ECE13H, SAEJ2909
- Coastdown: J2263, WLTP GTR15
- Pass-By-Noise: R41, R51



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NCAP - New Car Assessment Programs: Tests, Assessment Methods, Ratings

Course Description

In 1978 the first New Car Assessment Program (NCAP) was established by NHTSA in the United States. The goal was to motivate competing car manufacturers to enhance the safety level of their cars beyond the minimum safety standards defined by regulations. The same approach has been followed globally by other organizations (e.g. by Euro NCAP, IIHS, ANCAP, JNCAP, KNCAP,C-NCAP,...) Euro NCAP which has been established in 1997 has taken a leading role and has significantly influenced other countries and regions. The NCAP programs in many cases are highly dynamic, especially in comparison with rulemaking activities. In order to reach the goal to continuously improve the safety level of cars, the requirements need to be permanently adapted to the state of technology. Developers in the automotive industry need to know about upcoming changes at an early stage in order to be able to design or equip their vehicles accordingly.

In this seminar attendees get an overview of the organizations in charge of the NCAP programs and become familiar with the various test and assessment methods.

NEW

The seminar is conducted serveral times a year with changing focuses:

- Focus passive safety: Here the focus is on test and assessment methods for passive safety. Frontal and side impact, whiplash, child protection and pedestrian protection are discussed in detail. Tests for active safety are only mentioned in as far as they are relevant for the overall rating. (Seminars with a focus on passive safety are higlighted in blue in the table below)
- Focus active safety: Here the focus is on active safety systems such as AEB or lane assistance. The tests and assessments for these systems are explained in detail. Test for passive safety are only mentioned in as far as they are relevant for the overall rating. (Seminars with a focus on active safety are higlighted in green in the table below)

In both focusses the current overall rating methods are described and explained. In addition to that an outlook is given on the roadmaps and future developments of the NCAP programs.

Who should attend?

The seminar addresses design, simulation, testing and project engineers as well as managers who want to get a current overview on the global range of NCAP programs with an outlook on upcoming topics and trends from an insider. Depending on the focus of their work attendees should chose the appropriate focus of the seminar.

Course Contents

- New Car Assessment Programs overview
- U.S. NCAP
- IIHS
- Euro NCAP
- ANCAP
- JNCAP
- Korea NCAP
- China NCAP
- Latin NCAP
- ASEAN NCAP
- BNVSAP
- Global NCAP

Instructor	
2	

Director and Professor Andre Seeck (German Federal Highway Research Institute) is head of the division "Vehicle Technology" with the German Federal Highway Research Institute (BASt). In this position he is responsible for the preparation of European Safety Regulations. He is also head of the strategy group on automated driving and represents the German Federal Ministry of Transport and Digital Infrastructure in the Board of Directors of Euro NCAP. These positions enable him to gain deep insight into current and future developments in vehicle safety.

nes	DATE	COURSE ID	VENUE	DURATION PRICE	LANGUAGE
Venu	2021.03.2017	2878	Alzenau	2 Days 1.290,- EUR till 20.02.2017, thereafte	r 1.540,- EUR
tes &	2223.06.2017	2879	Alzenau	2 Days 1.290,- EUR till 25.05.2017, thereafte	r 1.540,- EUR
Dat	0203.11.2017	2880	Alzenau	2 Days 1.290,- EUR till 05.10.2017, thereafte	r 1.540,- EUR



(())

SAFETYUPDATE +active

The concept is familiar: To keep software up-to-date you regularly make an update. The same is true for automotive safety engineering: To keep yourself up-to-date you have to attend the SafetyUpDate on a regular basis. Here you get a comprehensive overview of all relevant news in automotive safety.

Active + Passive Safety = SafetyUpDate +active

The SafetyUpDate reflects the close integration of active and passive safety and combines both topics in one event. General topics such as the NCAP consumer tests are dealt with in plenary presentations, whereas specific topics such as testing are presented in parallel session on active respectively passive safety.

Conference topics include:

- Regulations for active and passive safety
- NCAP consumer protection tests
- Development tools: Test & Simulation
- Development strategies & solutions
- Biomechanics & accident research

From Experts for Experts

The speakers are leading experts from government agencies, consumer protection organizations, industry and universities. We consider it important that the UpDate presentations are product-neutral and practical.

Meeting Point: Expert Dialog

In addition to the presentations the SafetyUpDate encourages the communication among experts. After the presentations the speakers are available for discussions at the Meeting-Point.

Who should attend?

The SafetyUpDate is aimed at automotive developers who are interested in active or passive vehicle safety and want to bring their knowledge up-to-date. In addition to the knowledge update, SafetyUpDate offers excellent opportunities to build and maintain contacts in the safety community.

	DATE	1617. May 2017	2627. September 2017		
	HOMEPAGE	www.carhs.de/asu	www.carhs.de/gsu		
Facts	VENUE	Stadthalle Aschaffenburg	Technische Universität Graz		
	LANGUAGE	German with translation into English	German with translation into English		
	PRICE	1.450,- EUR till 18.04.2017, thereafter 1.690,- EUR	1.450,- EUR till 29.08.2017, thereafter 1.690,- EUR		













Approach to stationary target





Euro NCAP Test Method for AEB City

Assessment Protocol Version 7.0.3 Test Protocol Version 1.1

 $v = 10 \text{ km/h} \dots 50 \text{ km/}$

h	in	5	km/h	step

v=0 km/h

v _o (km/h)	Points for Accident Avoidance	Remarks
10	1	Prerequisites for scoring in AEB City:
15	2	 minimum 1.5 points (out of 2) from the whiplash assessment of front seats (page 85)
20	2	■ up to 20 km/h accidents must be completely avoided
25	2	For $v_0 > 20$ km/h accident mitgation is rewarded. The score is calculated from the
30	2	remaining impact velocity v _، Points for Accident Avoidance * (v,-v,)/v,
35	2	Example: At $v_0 = 30$ km/h the target is impacted at a remaining velocity of $v_1=10$
40	1	km/h:
45	1	2 Points * (30 km/h - 10 km/h) / 30 km/h = 1.333 Points
50	1	
HMI Assessment		AEB City systems, that are default ON at the start of every journey and can not be de-activated by the driver with a single push on a button are awarded 2 Points

The raw score of a maximum of 14 points from the AEB test is scaled down to a maximum of 2.5 points (scaling factor 0.179). The HMI points are scaled to a maximum of 0.5 points (scaling factor 0.25). The total **maximum score for AEB City is 3 points** and is part of the **Adult Occupant Rating**.

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AEB City

120

cárhs



PraxisConference Autonomous Emergency Braking

The PraxisConference AEB focuses on technical development and testing details of safetyrelated driver assistance systems, like emergency brake assist and autonomous evasive steering.

First of all, leading experts in the field of requirements and technical solutions present the facts you need to develop and approve AEB systems in accordance with state-of-the-art science and technology. This includes current and upcoming requirements, vehicle presentations, development strategies as well as the question of the responsibility for consequences caused by mistakes of an autonomous driving function. Furthermore, we expand our field of action with heavy commercial vehicles, for which AEB systems are already mandatory. We are excited to announce that the 2017 PraxisConference AEB takes place at CARISSMA, Technische Hochschule Ingolstadt. The second conference day, called "DemoDay", offers practical sessions on the CARISSMA indoor and outdoor proving grounds. Test equipment, such as targets, driving robots, GPS-technologies and control software, is demonstrated and explained in detail. The preparation, execution and analysis of AEB tests are shown in live demonstrations. For our participants this offers the chance to view the systems under test conditions, clarify their questions and get an overview of test conditions for cars and heavy commercial vehicles.



- Legal and consumer protection requirements
- Best practice: testing and simulation
- Outlook on the development process for autonomous evasive steering and driving
- Vehicle technology: introduction of up-to-date driver assistance systems
- Test equipment: targets, driving robots, control and measurement software

Who should attend?

The PraxisConference AEB addresses everyone, who works in the field of safety-related driver assistance systems. If you want to improve your network, you will meet interesting conversation partners with development, system integration, regulation and testing backgrounds.

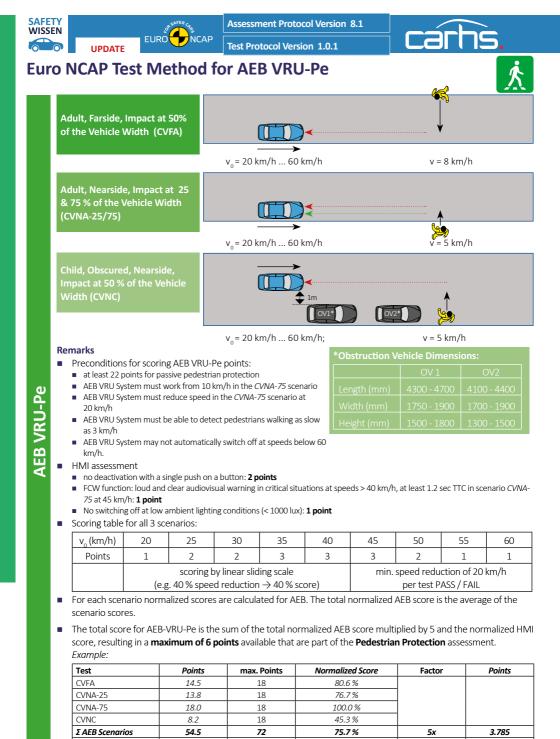
	DATE	28 29. September 2017			
	HOMEPAGE	www.carhs.de/pkaeb			
Facts	VENUE	TH Ingolstadt, Esplanade 10, 85049 Ingolstadt			
	LANGUAGE	German with simultaneous translation into English			
	PRICE	1.450,- EUR till 31.08.2017, thereafter 1.690,- EUR			











нмі

2

4

50 %

0.5

4.285

1x total AEB VRU-Pe Score



ADAS Validation

Test & Validation Planning Measuring Equipment Setup

Validation Tests

Measured Data Documentation

Analysis and Report

- Functional Valididation acc. to NCAPs, OEM Specification
- Functional Valididation acc. to ISO 26262
- Bus Communication Valididation

Application of optimized ADTF Filters and MATLAB Scripts

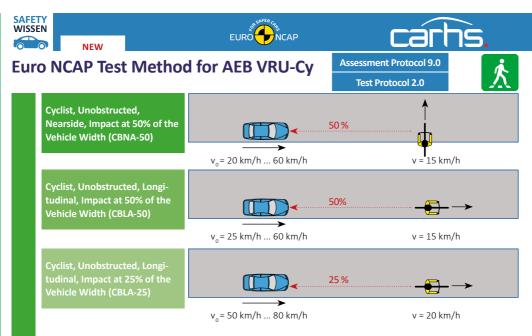


Contact

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Headquarters EDAG Engineering GmbH · Kreuzberger Ring 40 65205 Wiesbaden · Germany





Prerequistes for scoring:

- the AEB system must be default ON at the start of every journey
- system may not automatically switch off at a speed < 80 km/h
- the score of the pedestrian impact tests (legforms & head) must be ≥ 22 points

Scoring table:

AEB VRU-Cy

			points av	ailable per te	est speed
test speed v ₀ (km/h)	AEB	FCW	CBNA-50	CBLA-50	CBLA-25
		AEB	AEB	FCW	
20	score = points x (v ₀ - v _{impact})/v ₀		1		
25			1	1	
30			1	1	
35			1	2	
40			1	2	
45	(6. s)		1	3	
50	pass /fail:	pass /fail:	1	3	3
55	points are awarded if v _{impact} ≤ v₀ - 20 km/h		1	3	3
60			1	1	1
65		points are awarded if warning is			1
70		issued @ TTC \geq 1.7 s			1
75					1
80					1
		9	2	7	
normalized score (2) = actual score / (1)				(4	1)
		AEB Cyclist total points	6 points x ((3) + (4)) / 2		

Additional scenarios will be implemented in 2020.



AB Dynamics provides innovative solutions for vehicle testing on the track and in the laboratory

Anthony Best Dynamics supplies advanced testing technology to all of the largest 25 car manufacturers in the world*

High speed collision between ABD's guided soft target vehicle (GST) and the ADAS test vehicle



Driving Robots Used worldwide for tests such as sinedwell (ESC test), fishhook and ADAS development. ABD robots can be used with a human driver in the vehicle or for driverless control of the vehicle.



Driverless Test Systems AB Dynamics' Driverless systems give precise and repeatable control of vehicles to eliminate the risk of driver injury during dangerous vehicle tests.



ADAS Test Systems Used for the development, testing and proving of vehicle Advanced Driver Assistance Systems (ADAS). The motion of the soft target vehicle or pedestrian is synchronised with the test vehicle to create collision scenarios.

www.abd.uk.com



Test Protocol Version 1.1



Euro NCAP Test Method for AEB Inter-Urban



CCRs*: Approach to stationary target		$v_{0} = 30 \text{ km/h} \dots 80$) km/h	V	= 0 km/h
CCRm*:					
Approach to slower tar	get	v _o = 30 km/h 80) km/h	v =	≥20 km/h
CCRb*:		(()	d	→ 〔	
Approach to braking target * CCR: Car-To-Car Rear; s: standing;		$v_0 = 50 \text{ km/h}$ $v_0 = 50 \text{ km/h}$ $v_0 = 50 \text{ km/h}$	d _o = 12 m d _o = 40 m d _o = 12 m	$v_0 = 50 \text{ km}$ $v_0 = 50 \text{ km}$	→ n/h, a = -2 m/s ² n/h, a = -2 m/s ² n/h, a = -6 m/s ²
m: moving; b: braking		$v_0 = 50 \text{ km/h}$	$d_0 = 40 \text{ m}$	v _o = 50 km	n/h, a = -6 m/s²
stationary ta v _o (km/h) Points fo		Points for AEB	arget (CCRm) Points for	FCW	braking targe (CCRb)
30 2		1	_		
35 2		1	-		
40 2		1	-		
45 2		1	-		
50 3		1	1		1 point each
55 2		1	1		for AEB and for FCW per
60 1		1	1		scenario
65 1		2	2		
70 1		2	2		
75 1		-	2		
80 1		-	2		
Σ 18		11	11		2 x 4

HMI Assessment		Systems that can not be de-activated with a single push on a button are awarded 2 points
		Supplementary warning for the FCW system(e.g. head-up display, belt
		jerk, brake jerk): 1 point
		Reversible pre-tensioning of the belt in the pre-crash phase: 1 point

The total AEB Inter-Urban score results from the following weighting of the normalized scores (%):

AEB Inter-Urban = FCWscore x 1.0 + AEBscore x 1.5 + HMIscore x 0.5

This results in a **maximum total score of 3 points for AEB Inter-Urban**, which is part of the **Safety Assist** assessment. The AEBscore (respectively FCWscore) is the average score from all the scenarios.

Example:

System	FCW			A	HMI			
Scenario	CCRs	CCRm	CCRb	CCRm	CCRb	De-activation	Warning	Pretension
Points	15.264	8.404	4	5.078	2.700	2	0	0
Score	84.7 %	76.4 %	100.0 %	46.2 %	67.5 %	50.0 %		
	FCWscore = (84.7 % + 76.4 % + 100 %) / 3 = 87.0 %			AEBscore = (46.2 %	HMIscore = 50.0 %			
Total		87 % x 1.0 + 56.9 % x 1.5 + 50 % x 0.5 = 1.974 points (out of 3)						

For systems that only offer the AEB function, the results of tests at all speeds (covering AEB and FCW) are used to calculate separate normalized AEB and FCW scores for each scenario. Where AEB and FCW test speeds are overlapping, the test result of AEB is duplicated for FCW.

DEKRA Automobile Test Centre Klettwitz. Expertise in child safety.



As an integral part of the DEKRA Technology Centre, the DEKRA Automobile Test Centre at the EuroSpeedway Lausitz is divided into four centres of expertise, so-called modules. A special core field of activity is assigned to each of these modules. With the development of the new i-Size test system in 2015, an important aspect has now been added to the range of services for child seats.

Test types

- > Sled and catapult facility for frontal, side and rear impact tests on ECE bench or in vehicle bodies
- > Rollover test bench
- > i-Size measurement
- > Temperature test
- > Energy absorption
- > Conditioning of components

Tasks

- > Development tests
- > Homologation service according to ECE R44 and 129
- > Customer requirements
- > COP tests

Accreditation as test laboratory according to ISO 17025

> Germany - DakkS

Designation as Technical Service

- > Germany KBA
- > Netherlands RDW

Test bench for lateral impact, child seats





Test bench for rear impact, child seats







DEKRA Automobil Test Center Senftenberger Straße 30 | 01998 Klettwitz Phone: +49.35754.7344-500 | Fax: +49.35754.7345-500

www.datc.de

U.S. NCAP Rear Automatic Braking*

Rear Automatic Braking Feature Confirmation Test Procedure (Working Draft), Dec. 2015



Dummy

4a Euro NCAP Pedestrian - Child Dummy static

Test-Procedure

- Place the direction selector in reverse while maintaining full pressure on the brake pedal.
- Release the vehicle's brake pedal and allow the vehicle to coast backward while maintaining the vehicle's centerline within +/- 1 inch of the longitudinal line marked on the ground.
- Allow the vehicle to coast until the rear automatic braking feature intervenes by automatically engaging the service brakes bring the vehicle to a stop or until the vehicle strikes the test object. Once either of these two outcomes occurs, the vehicle's brake pedal should be depressed to end the test trial. Every effort must be made to safely conduct this test. If testing indoors, proper ventilation must be provided. No personnel shall be located to the rear of a test vehicle at any time during the test trial.

Requirements

A positive test outcome would involve the vehicle coming to a stop before it reaches the location of the test object and with no physical contact with the test object for each of the three test object locations assessed.

* Please note: The rear automatic brake test is part of the U.S. NCAP upgrade planned for model year 2019. The test procedure and requirements are based on "Rear Automatic Braking Feature Confirmation Test Procedure (Working Draft), December 2015". Docket NHTSA-2015-0119.

SAFETY WISSEN

NFW/

Approach to stationary target

	20 km/h Test			40 km/h Test				FCW
Speed reduction	< 8 km/h	8-14 km/h	≥ 15 km/h	< 8 km/h	8-14 km/h	15-34 km/h	≥ 35 km/h	
Points	0	1	2	0	1	2	3	1

Rating Scheme:

Points			
	1	2-4	>5
Rating	BASIC	ADVANCED	SUPERIOR

IIHS AEB / Front Crash Prevention Test

3.05 m

= 3.66 m

d = 9.14 m

 $v_{0} = 20 \text{ km/h}$

 $v_{0} = 40 \text{ km/h}$

AEB Test Protocol, V. I, Oct. 2013



v = 0 km/h

v = 0 km/h

we act for your safety



Advanced testing technologies for active safety systems to reduce road facilities

4activeSystems GmbH | Industriepark 1 | 8772 Traboch +43 3842/45 106 600 | www.4activesystems.at SAFETY WISSEN

U.S. NCAP Crash Imminent Braking

CRASH IMMINENT BRAKE SYSTEM PERFORMANCE EVALUTION, October 2015

ſ

LVS (Lead Vehicle Stopped) Approach to stationary target	v _o = 25 mph (40.2 km/h)	v = 0 mph
LVM (Lead Vehicle Moving) Approach to slower target	v _o = 25 mph (40.2 km/h) v _o = 45 mph (72.4 km/h)	v = 10 mph (16.1 km/h) v = 20 mph (32.2 km/h)
LVD (Lead Vehicle Decelerating) Approach to braking target	d_0 $v_0 = 35 \text{ mph (56.3 km/h)} d_0 = 45.3 \text{ ft (13.8 m)}$ $\pm 8 \text{ ft (2.4 m)}$	v _o = 35 mph (56.3 km/h). a = -0.3 g
False Positive Test Approach to steel trench plate	$v_0 = 25 \text{ mph} (40.2 \text{ km/h})$ 8 ft x 12 ft x 1 $v_0 = 45 \text{ mph} (72.4 \text{ km/h})$	in (2.4 m x 3.7 m x 25 mm)

Requirements

Scenario	LVS	LVM 25 mph	LVM 45 mph	LVD	False Positive
Require- ment	∆v≥9.8 mph (15.8 km/h)	no impact	∆v≥9.8 mph (15.8 km/h)	∆v ≥ 10.5 mph (16.9 km/h)	deceleration \leq 0.5 g

U.S. NCAP Forward Collision Warning

	FORWARD COLLISION WARNING SYSTEM C	ONFIRMATION TEST, Feb 2013
LVS (Lead Vehicle Stopped)		
Approach to stationary target	v _o = 45 mph (72.4 km/h)	v=0 mph
LVM (Lead Vehicle Moving)		
Approach to slower target	√ ₀ = 45 mph (72.4 km/h)	v=20 mph (32.2 km/h)
LVD (Lead Vehicle Decelerating)		> III)
Approach to braking target	→ v _o = 45 mph (72.4 km/h) d _o = 89.4 ft (30 m) ± 8.2 ft (2.5 m)	v _o = 45 mph (72.4 km/h). a = -0.3 g

Requirements

Scenario	LVS	LVM	LVD
Require-	Alert no later than	Alert no later than	Alert no later than
ment	2.1 s TTC	2.0 s TTC	2.4 s TTC

TRAFFIC INFORMATION FOR DRIVERS



4 KM OF

SLOW MOVING TRAFFICAHEAD

ADJUST SPEED

TRAFFIC JAM ASSIST

IN STOP&GO MODE CONTINUE DRIVING STRESS-FREE

ZF-NETWORKING MECHANICAL AND ELECTRONIC SYSTEMS WITH ADVANCED INTELLIGENCE ZF.COM/TECHNOLOGY-TRENDS



MOTION AND MOBILITY





Car Body Design for Analysis Engineers

Course Description

In general analysis engineers have a sound knowledge on numerical methods and experience in structural analysis with the Finite Element Method. To make a valuable contribution to the vehicle development process using numerical simulation, knowledge on car body design and functional layout is required. To efficiently undertake lightweight design all fundamental requirements have to be taken into account early in the design process. These requirements will be outlined in the seminar. Additionally the characteristics of the specific organization of the development process have to be incorporated.

Course Objectives

The objective of the seminar is to transfer the knowledge needed for an analysis engineer to play a part in vehicle development. Especially the examination of design variants of existing car bodies makes the seminar descriptive and practical.

Who should attend?

This 2 day seminar is aimed at analysis engineers working in the automotive industry.

Course Contents

- Load carrying principles of lightweight design
 - Load assumptions
 - Design principles
 - Technology of car body construction
 - Car body architecture
 - Structural materials and pre-products
 - Material selection
 - Manufacturing methods
 - Joining techniques

- Development process described at the example of the improvement of static properties
 - Principal structure of the development process
 - CAE-compatible CAD
 - Finite Element modelling of a car body
 - Static behaviour of the car body structure
 - Finite Element Analysis of joints
- Measures for improved dynamic behavior
 - Part dimensioning taking into account vehicle vibrations
 - Dynamic analysis of full vehicles
- Measures for improved acoustic behavior
 - Acoustic design of a car body
 - Simulation methods
- Realization of safety measures
 - Energy absorption elements
 - Vehicle car bodies
 - Safety systems
 - Pedestrian protection
 - Post crash
- Use of optimization methods in industrial applications
 - Introduction into mathematical optimization
 - Approximation techniques
 - Optimization software
 - Optimization strategies
 - Shape optimization
 - Topology optimization



Prof. Dr.-Ing. Axel Schumacher (University of Wuppertal) studied mechanical engineering at the universities of Duisburg and Aachen. He received his doctorate on structural optimization from the university of Siegen. Following research projects for Airbus were focused on the optimization of aircraft structures. Thereafter he worked in the CAE methods development department of Adam Opel AG as project leader for structural optimization. From 2003 - 2012 he was a professor at the University of Applied Sciences in Hamburg and taught structural design, passive safety and structural optimization. Since 2012 he has been professor at the University of Wuppertal, where he holds the chair for optimization of mechanical structures.

nues	DATE	COURSE ID	VENUE	DURATION PRICE	LANGUAGE
& Ve	1920.06.2017	2922	Alzenau	2 Days 1.290,- EUR till 22.05.2017, thereafter 1.540,- EU	R 💦
Dates	1314.11.2017	2921	Alzenau	2 Days 1.290,- EUR till 16.10.2017, thereafter 1.540,- EU	۲ 💻



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Lightweight Design Strategies for Car Bodies

Course Description

Designing and developing light weight vehicles ready for series production is becoming increasingly important. Especially for fully electric vehicles with large and heavy battery packs light car bodies are indispensable. But also for other propulsion concepts lightweight is desirable. The focus in this seminar will be given to production ready vehicle concepts. Ideas taken from the extreme light weight design are integrated into the considerations. A symbiosis of the use of modern lightweight materials and the design of appropriate lightweight structures leads to efficient lightweight design. This multi-disciplinary task is only possible with development strategies that can simultaneously handle requirements of crash protection, vehicle dynamics, comfort, acoustics, durability and production of the vehicle. The aim of this seminar is to provide the competencies for the development of light vehicle structures.

Who should attend?

This seminar is aimed at designers, analysis engineers and project managers from car body, component and system development.

Course Contents

- Potentials of lightweight design
 - Motivation and problem definition
 - Current lightweight vehicle concepts
 - The "Lightweight Loop"
- Principles of lightweight design
 - Definition of requirements
 - Determination of design loads
 - Principal design rules
 - Approaches of bionics
 - Fail-safe, safe life, damage tolerance
 - Methodical concept finding (architecture, topology)

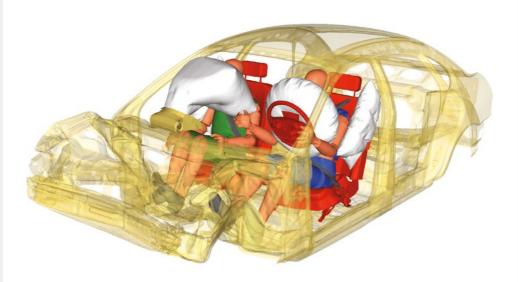
- Materials and their specific design rules
 - Material selection
 - Acquisition of material data
 - Steel, aluminum, magnesium
 - Fiber composites
 - Material mix and recycling
- Structures of lightweight design
 - Space-frame structures
 - Shell structures (beads, ribs, ...)
 - Foams and inlays
 - Composite sandwich structures
 - Related joining techniques (adhesive bonding, ...)
- Advanced CAE methods for lightweight design
 - Stability (buckling, ...)
 - Dynamics and Acoustics
 - Fracture mechanics, multi-scale models (observation of cracks, etc.)
 - Crash of small structures
 - Analysis of joints
 - Robustness analysis
 - Optimization of shape and dimension
- Case studies
- Selected Vehicle Components
- Ultra-lightweight vehicle concepts
- Vehicle concepts for mass production



Prof. Dr.-Ing. Axel Schumacher (University of Wuppertal) studied mechanical engineering at the universities of Duisburg and Aachen. He received his doctorate on structural optimization from the university of Siegen. Following research projects for Airbus were focused on the optimization of aircraft structures. Thereafter he worked in the CAE methods development department of Adam Opel AG as project leader for structural optimization. From 2003 - 2012 he was a professor at the University of Applied Sciences in Hamburg and taught structural design, passive safety and structural optimization. Since 2012 he has been professor at the University of Wuppertal, where he holds the chair for optimization of mechanical structures.

nues	DATE	COURSE ID	VENUE	DURATION PRICE	LANGUAGE
& Vei	2728.03.2017	2828	Alzenau	2 Days 1.290,- EUR till 27.02.2017, thereafter 1.540,-	EUR
Dates	2324.11.2017	2923	Alzenau	2 Days 1.290,- EUR till 26.10.2017, thereafter 1.540,-	EUR

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»AUTOMOBIL INDUSTRIE« LEICHTBAU**GIPFEL**

The »Automobil Industrie« - Light Weight Design Summit is the high level networking event for the pioneers in automotive lightweighting. The focus theme for 2017 is "E-Mobility – new Opportunities for Light Weight Design". Meet OEMs and suppliers on 09./10. March 2017 at the Vogel Convention Center in Würzburg, Germany.

Keynotes and expert presentations, technical sessions and live demonstrations highlight the importance of lightweighting for the future of electric vehicles.

Discussions about innovative ideas and the networking betwenn experts from OEMs and suppliers are at the core of the Light Weight Design Summit.

About the Focus Theme:

Digitization, connectivity, autonomous driving, electrification: Will these automotive megatrends move light weight design into the background?

Not at all, because all the new topics are added to the existing requirements on the current vehicles architecture. And they further increase the need for lightweighting in order to stay within weight boundaries.

In particular the electrification of the powertrain will leverage light weight design. Batteries, power electronics and E-drives will add weight as do new crash-protective enclosures for the batteries. Material selection and new design concepts create new challenges for the designer.

The future will be E-mobility, and current vehicle concepts will have to be revised or newly developed. The new approach is to revolutionize the vehicle body concepts while evolving the material concepts. This involves a substantial business potential - also for the suppliers.

Who should attend:

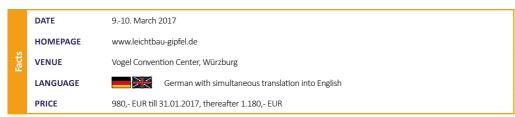
The Automobil Industrie Light Weight Design Summit is the platform for the communication between OEMs and suppliers. The summit addresses the technical management/CEO level of OEMs and suppliers, the purchasing management, heads of development and design, project engineers, innovation managers and materials specialists.













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Robust Design - Vehicle Development under Uncertainty

Course Description

The seminar addresses the current state of the art complemented by recent achievements in research and development to quantify and control uncertainties (lack-of-knowledge and variations) in vehicular development. Aspects of sensitivity and robustness analysis are discussed as well as topics in reliability, resilience, redundancy and model uncertainty. In addition, numerical methods for optimization with consideration of uncertainties and methods for model order reduction (MOR) to reduce computational effort are discussed. Applications (e.g. NVH, crash) illustrate the usage of the methods and the fact that methods should be adapted to the degree of maturity of the design in the development process.

Course Objectives

The seminar is focused on methods and their theoretical background to enable the participants to realize applications directly in the industrial context. Hence, uncertainties can be characterized, quantified, and – together with sensitivity analysis – concept and structural evaluations are made possible, which consider robustness, reliability, resilience, and redundancy. Corresponding optimizations can then be realized in an efficient manner.

Who should attend?

The seminar is proposed for engineers with first experiences in numerical concept and series development of vehicles, who are interested in including robustness, reliability and other aspects of uncertainty management in their industrial designs.

Course Contents

- Mathematical methods for uncertainty quantification
- Linear and non-linear sensitivity analysis (global / local)
- Design of Experiments (DoE), Response Surface Methods (RSM)
- Methods for model order reduction (MOR)
- Robustness versus reliability
- Robustness in early design stages (Set-based Design und Solution Space Approach)
- Methods for resilience, redundancy, model uncertainty
- Optimization under uncertainties
- Applications taken from acoustics and crashworthiness



Prof. Dr.-Ing. Fabian Duddeck (Technical University Munich) leads the research group on optimization and robustness at the Technische Universität München (TUM) since 2010. His research is focusing on shape and topology optimization for crash, NVH (noise vibration and harshness) and other disciplines including stochastic modeling and robustness assessments. Holding the chair for Computational Mechanics at the TUM, he also teaches and directs research at Queen Mary University of London (QMUL) and at the French Ecole des Ponts ParisTech (ENPC). His group is involved in industrial as well as national and international research projects. Prof. Duddeck has obtained his PhD (1997) and his Habilitation degree (2001) at the Technische Universität München.

nues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
& Vei	1314.02.2017	2818	Alzenau	2 Days	1.290,- EUR till 16.01.2017, thereafter 1.540,- EUR	
Dates	1213.09.2017	2950	Alzenau	2 Days	1.290,- EUR till 15.08.2017, thereafter 1.540,- EUR	



In the last 20 years computer simulation has become an indispensable tool in automotive development. Tremendous progress in software and computer technology makes it possible today to assess product and process performance before physical prototypes have been built. Despite of significant progress in simulation technology and impressive results in industrial application there remains a number of challenges which prevent a "100% digital prototyping". We at carhs.training call these Grand Challenges.

Automotive CAE Grand Challenge offers a platform for dialog

The automotive CAE Grand Challenge stimulates the exchange between users, scientists and software developers in order to solve these challenges. Annually the current, critical challenges in automotive CAE are being identified through a survey among the simulation experts of the international automotive industry. In the conference one session is dedicated to each of the most critical challenges, the so-called Grand Challenges. In each session CAE experts from industry, research and software development will explain the importance of the individual Challenge for the virtual development process and talk about their efforts to solve the challenge.

Automotive CAE Grand Challenges 2017

In September 2016 we have determined the important current challenges of automotive CAE - the so-called "Grand Challenges" - through a survey among the CAE experts of the international automotive industry. The below listed "Grand Challenges" form the topics of the sessions of our automotive CAE Grand Challenge 2017 conference.

- Crash: Material and failure models of plastics
- Fatigue: Virtual proofing ground, determination of load collectives
- NVH: Squeak and rattle, groaning
- Multi simulation: Multi trade simulation, influence of manufacturing on material and product
- Optimization: Topology optimization
- Safety: Stability of dummy models, including scatter of hardware dummies
- Strength: Failure models for adhesives

Who should participate?

The conference intends bringing together industrial users, researchers and software developers to discuss these current, critical challenges of automotive CAE and to initiate collaboration between these groups to help overcoming the Grand Challenges of automotive CAE. The presentation program of the conference provides both experts and beginners valuable information for their daily work. The possibility to meet and exchange with all stakeholders of automotive CAE is a great opportunity. In the accompanying exhibition participants can receive additional information from leading companies of CAE.

_					
	DATE	05 06. Apri	2017		
	HOMEPAGE	www.carhs.o	www.carhs.de/grandchallenge		
Facts	VENUE	Congress Park Hanau, Schloßplatz 1, 63450 Hanau			
	LANGUAGE		English		
	PRICE	850,- EUR til	l 08.03.2017, thereafter 980,- EUR		













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Material Models of Composites for Crash Simulation

Course Description

Increasing demands for weight reduction paralleled by requirements for improved crash performance and stiffness of structures have strongly pushed the development of advanced composites. The use of composite materials today is not limited to niche applications or secondary parts; they are increasingly used for important load carrying structural components in series production.

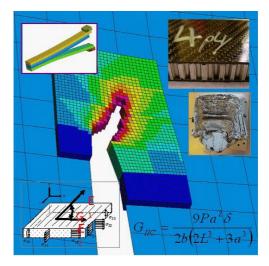
In this one day seminar Prof. Thomas Karall presents the foundations of structural impact and crash analysis of composites with the Finite Element Method. At the beginning of the seminar an overview of current and upcoming industrial applications of composite materials is given. Thereafter concepts for the correct physical modeling of the complex load degradation and failure mechanisms in numerical simulation are presented. The course concentrates on the numerical simulation of the crash behavior of composites and is accompanied with demonstrations using the PAM-CRASH code.

Who should attend?

The course addresses simulation and project engineers, project managers as well as researchers involved in the analysis and design of composite parts and structures.

Course Contents

- Current and upcoming areas of application of composite materials
- Analysis of composite materials
- Available material models and their application
- Modelling methods for plies and laminates
- FEM modelling of composites
- Failure mechanisms and their representation
- PAM-CRASH ply and delamination models
- Necessary material tests
- Examples





Prof. Dr. Thomas Karall (Hof University of Applied Sciences) studied mechanical engineering at the Technical University of Vienna and received his PhD as Assistant Professor at the University of Leoben in the field of fibre-reinforced plastics and the calculation by finite elements. From 2006 to 2010 he was head of department at the Austrian Research Institute for Chemistry and Technology in Vienna in the field of mechanical and thermal testing / fibre composites, and Secretary General of the Austrian Working Group for reinforced plastics. From 2010 to 2015 he worked as Lead Researcher for lightweight design at Virtual Vehicle Research Center in Graz. He was also a lecturer at the Technical University of Graz and lecturer at the FI Joanneum Graz. Since 2015 he has been Professor at the Engineering Department of the Hof University. His areas of work include lightweigt design, fibre-reinfoced composites and the finite element method.

ues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
& Vei	12.05.2017	2946	Alzenau	1 Day	740,- EUR till 14.04.2017, thereafter 890,- EUR	
Dates	27.10.2017	2947	Alzenau	1 Day	740,- EUR till 29.09.2017, thereafter 890,- EUR	

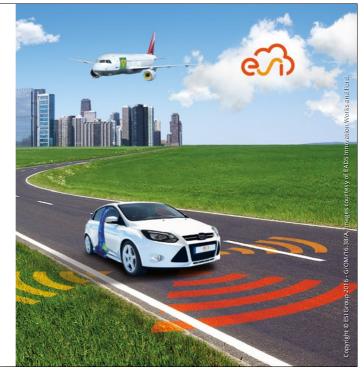
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Material Models of Metals for Crash Simulation

Course Description

Besides an appropriate spatial discretisation of the structure and a profound knowledge of the required load cases, appropriate material modelling is a key ingredient for predictive crash simulations. The load carrying structure of a car today still mainly consists of metallic materials. The materials to be described are diverse.

The seminar deals with the following materials:

- mild and high strength steels,
- cold formable AHSS and UHSS steels,
- hot formable and quenchable boron steels,
- wrought Al and Mg alloys,
- cast Al and Mg alloys.

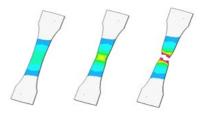
The objective of this 1 day course is to give the participants an overview of material models of metals used in crash simulation. In a first step the deformation behavior and the failure mechanisms of each material class are explained based on the material structure. The influence of strain rate on material behavior is an important aspect in the context of crash simulation and will be discussed in the seminar. In a second step phenomenological material models for crash simulation are introduced. In the third step the tests needed for the characterization of materials are described and the parameter identification for the material models is discussed. Finally and using example simulations the sensitivity of simulation results regarding the identified material parameters is shown.

Who should attend?

The course addresses engineers working in the field of crash simulation and heads of simulation departments interested in the important topic of material modelling.

Course Contents

- Overview of metallic materials used in cars
- Influence of material structure on mechanical behavior
- Phenomenological material models for metals
- Overview of experimental methods for material characterization
- Identification of material parameters from experiments
- Discussion of the sensitivity material parameters





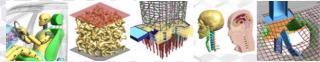
Dr.-Ing. Helmut Gese (MATFEM - Partnerschaft Dr. Gese & Oberhofer) founded the engineering consultancy MATFEM (from 1999 the company has been named MATFEM partnership Dr. Gese & Oberhofer) in 1993. MATFEM offers technical and scientific consultancy services at the intersection of material science and finite element methods. Besides performing FEM analysis projects the area of activity covers experimental and theoretical characterization of materials and the development of new material models for simulation.

ues	DATE	COURSE ID	VENUE	DURATION	PRICE	LANGUAGE
& Vel	09.05.2017	2899	Alzenau	1 Day	740,- EUR till 11.04.2017, thereafter 890,- EUR	
Dates	26.10.2017	2900	Alzenau	1 Day	740,- EUR till 28.09.2017, thereafter 890,- EUR	





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Material Models of Plastics and Foams for Crash Simulation

Course Description

Numerical simulation has become a fundamental element in the development of motor vehicles. Today, many important design decisions, especially in the field of crash, are based on simulation results. During the last few years there has been an increase in the use of foams in vehicles. These are, due to their variety and structure, much more complicated regarding the characteristics of the materials than "simple" materials such as steel or aluminum, which can be modelled rather well. Characterization of foam materials is a great challenge for the simulation expert. Although by now there are different modelling approaches available in explicit FEM-programs such as LS-DYNA and PAM-CRASH, these are, however, often not satisfactory. The application of these special material models requires a sound knowledge and experience.

The seminar provides an overview over plastics and foam materials used in automotive engineering and their phenomenology. On the first day you obtain an introduction into the simulation of elastic and visco-elastic polymers, such as elastomers and elastic polymer foams with volume elements. You are thereby coming to understand the available material models in explicit finite element programs.

On the second day the focus is on the treatment of plastics, such as thermo- and duroplastics through elasto-plasticity with isotropic hardening. Non-associated deformation is going to be discussed as well. The seminar is rounded off with the procedure for simulation of glass-fiber reinforced plastics using both isotropic and anisotropic material laws.

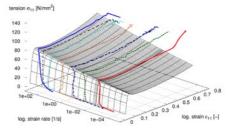
For a demonstration you are going to see examples created with the program LS-DYNA. References to material models in LS-DYNA and PAM-CRASH are going to help you in applying what you will have learnt.

Who should attend?

The seminar addresses experienced CAE engineers and heads of CAE departments with an interest in plastic and foam materials simulation. At least 1-year of experience with FEMprograms such as LS-DYNA and PAM-CRASH is suggested for participating in this course.

Course Contents

- Overview of polymer materials used in vehicle construction
- Verification and validation procedure for crash simulation
- Introduction to mechanics of materials
- Simulation of elastic and visco-elastic rubbers and foams with volume elements
- Overview of available material models in explicit finite element codes
- Simulation of elastic-plastic polymers under crash loading for validation
- Simulation of anisotropic materials with application to glass-fiber reinforced plastics





Prof. Dr.-Ing. Stefan Kolling (Giessen University of Applied Sciences) is Professor for Mechanics at the Giessen University of Applied Sciences (THM). Previously he worked as a simulation engineer at the Mercedes Technology Center in Sindelfingen. He was responsible for methods development in crash simulation. In particular he was involved in the modelling of non-metal materials such as glass, polymers and plastics. Prof. Kolling graduated from the Universities of Saarbrücken and Darmstadt, from where he also received his Ph.D. He is author of numerous publications in the field of material modeling.

nues	DATE	COURSE ID	VENUE	DURATION PRICE	LANGUAGE
& Vel	1011.05.2017	2909	Alzenau	2 Days 1.290,- EUR till 12.04.2017, thereafter 1.540,-	EUR 😹
Dates	2425.10.2017	2910	Alzenau	2 Days 1.290,- EUR till 26.09.2017, thereafter 1.540,-	EUR



Important Abbreviations

Α	
A-PCS	Advanced Pre-Collision System
	(Lexus)
AAA	American / Australian
	Automobile Association
AAAM	Association for the
	Advancement of Automotive
	Medicine
AAM	Alliance of Auto Manufacturers
AAIVI	(OSRP, USCAR)
-DAC	
aBAS ACC	Advanced Brake Assist System
	Adaptive Cruise Control
ACEA	Association of European
	Automobile Manufacturers
ACL	Anterior cruciate ligament
ACN	Automatic Collision Notification
ACU	Airbag Control Unit
ADAC	Allgemeiner Deutscher
	Automobil Club (German
	Automobile Association)
ADAS	Advanced Driver Assistance
	Systems
ADOD	Average Depth of Deformation
ADR	Australian Design Rules
AE-MDB	Advanced European Mobile
	Deformable Barrier
AEB	Autonomous Emergency
	Braking
AEBS	Autonomous Emergency Brake
	System
AHOD	Average Height of Deformation
AHOF	Average Height of Force
AHR	Active Head Rest
AIS (1)	Abbreviated Injury Scale
AIS (2)	Automotive Industry Standards
AISC	Automotive Industry Standards
	Committee
ANCAP	Australasian New Car
	Assessment Program
AOP	Adult Occupant Protection
	(Euro NCAP)
APF	Abdominal Peak Force
APPO	Assessment Protocol Prove Out
	(Euro NCAP)
APROSYS	Advanced PROtection SYStems
APSS	Active Pedestrian Safety
	, System
ARAI	Automotive Research
	Association of India
ASCC	Adaptive Speed Cruise Control
ASIC	Application-Specific Integrated
	Circuit
ASIL	Automotive Safety Integrity
	Level (functional safety)
ASIS	Adavanced Side Impact System
ATD	Anthropomorphic Test Device
AZT	Allianz Zentrum Technik
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В	
BAS	Brake Assist

BASt	Germany's Federal Highway
	Research Institute
BDA	Bonnet Deployment Actuator
BIS	Bureau of Indian Standards
BLE	Bonnet Leading Edge
BMVI	German Federal Ministry
	of Transport and digital
	Infrastructure
BoD	Board of Directors (Euro NCAP)
BOS	Beginning of Steer
BRIC	Brain Injury Criterion
BSD	Blind Spot Detection
С	
C-NCAP	China New Car Assessment
	Programme
C2C	Car-to-Car
CA	Crash Avoidance
CAD	Computer Aided Design
CAE	Computer Aided Engineering
CAN	Controller Area Network
Cars21	A Competitive Automotive
	Regulatory System for the 21st
	Century
CAT	Computer Aided Testing
CATARC	China Automotive Technology
	and Research Center
CCD	Charge Coupled Device
CCIS	Co-operative Crash Injury
	Survey
CCR	Car to Car-Rear
CDC	Collision Deformation
000	Classification
CEA	Comité Européen des
0271	Assurances
CFD	Computational Fluid Dynamics
CFR	Code of Federal Regulations
CITY	(USA)
CFRP	Carbon Fiber Reinforced Plastic
CIB	Crash Imminent Braking
CLEPA	Comité de liaison européen des
	fabricants d'equipements et de
	pièces automobiles
CMbB	Crash Mitigation by Braking
CIVIDD	(Ford)
CMBS	Crash Mitigation Brake System
CIVIDS	(Honda)
CMM	Coordinate Measuring Machine
CMOS	Complementary Metal Oxide
CIVIOS	Semiconductor
CMVR	Central Motor Vehicle Rules
CIVIVR	Canadian Motor Vehicle Safety
CIVIV55	Canadian Motor Venicle Safety Standards
000	
COG	Center of Gravity
CONTRAN	
COP (1)	Carry over Parts
COP (2)	Child Occupant Protection
cor	(Euro NCAP)
COS	Completion of Steer
CP	Contact Point

CRABI Child Restraint Airbag Interaction (Child Dummy), USA CRS Child Restraint System CSM Computational Structural Mechanics CSMA/CA Carrier Sense Multiple Access / **Collision Avoidance** CSMA/CD Carrier Sense Multiple Access / Collision Detection CV **Closing Velocity** CVFA Car to Vulnerable road user Farside Adult CVNA Car to Vulnerable road user Nearside Adult Car to Vulnerable road user CVNC Nearside Child D DAS Data Acquisition System DBS Dynamic Brake Support DCU Domain Control Unit DGPS Differential Global Positioning System DLO Daylight Opening DT Deployment Time E EBA **Emergency Brake Assist** EBD Flectronic Brake Force Distribution FCF Economic Commision for Europe (United Nations) ECOSOC United Nationions Economic and Social Council EDM Engineering Data Management EES **Energy Equivalent Speed** European Enhanced Vehicle-EEVC Safety Committee ELSA ELectric SAfety (UNECE/WP29 Working Group) EMC Electromagnetic Compatibility FOU Ease of use ES-2 re Euro SID 2 Rib Extension ESC Electronic Stability Control Enhanced Experimental ESV Vehicles Safety Program / Enhanced Safety of Vehicles Prog. ETC European Test Consortium ETSC European Transport Safety Council Euro NCAP European New Car Assessment Programme **EVITA** Experimental Vehicle for Unexpected Target Approach (TU Darmstadt) **EVPC** Electric Vehicles Post Crash EVT Euro NCAP Vehicle Target F

SAFFT

UPDATE

FARS

SAFETY WISSEN UPDATE

Important Abbreviations

-	
	System
FCW	Forward Collision Warning
FCWS	Forward Collision Warning
	System
FEM	Finite Element Method
FFC	Femur Force Criterion
Flex PLI	Flexible Pedestrian Legform
	Impactor
FMH	Free Motion Headform (FMVSS
	201)
FMVSS	Federal Motor Vehicle Safety
	, Standards
FPS	Frontal Protection System
FPSLE	Frontal Protection System
	Leading Edge
FRG	Floating Rib Guide
FRP	Fiber Reinforced Plastic
FSI	Fluid-Structure-Interaction
FTDMA	Flexible Time Division Multiple
TUNA	Access
FW	Full Width
FWDB	Full Width Deformable Barrier
FWRB	Full Width Rigid Barrier
IVVND	
G	
G.S.R.	General Statutory Rules
GAMBIT	Generalized Acceleration
	Model for Brain Injury
	Threshold
GCS	Glasgow Coma Scale
GIDAS	German in-Depth Accident
0.07.0	Study
GRSG	Groupe de Rapporteurs sur
01.50	la Sécurité Générale (WP29 -
	General Safety Provisions)
GRSP	Groupe de Rapporteurs sur
UNJF	la Sécurité Passive (WP29 -
CCD	Passive Safety)
GSR	General Safety Regulations
GTR	Global Technical Regulation
GVM	Gross Vehicle Mass
GVWR	Gross Vehicle Weight Rating
н	
HBM	Human Body Model
HGV	Heavy Goods Vehicle
HIC	Head Injury Criterion
HIT	Head Impact Time
	Harmonisation Interlab Test
HITS	Series
HLDI	Highway Loss Data Institute
HLLC	High Level Liaison Committee
HMI	Human Machine Interface
HNI	Head Neck Impactor
HNT	Horizontal Negative deviation
	from Target cell load
HOF	Height of Force
HPC	Head Performance Criterion
HPM	H-Point Manikin
HPS	Head Protection System
HPT	Head Protecting Technology

HRC	Time to head restraint first contact
HRMD	Head Restraint Measuring Device
HRV	Head Rebound Velocity
HTD	Hardest to detect
HV	High Voltage
<u> </u>	
IARV	Injury Assessment Reference Value
IBRL	Internal Bumper Reference Line
ICPL	Injury Criteria Protection Level
ICRT	International Consumer
	Research and Testing
IG	Informal Group
IHC	Intelligent Headlight Control
IHRA	International Harmonized
INNA	
	Research Activities
IIHS	Insurance Institute for Highway Safety
IIWPG	International Insurance
	Whiplash Prevention Group
INRETS	Institut National de Recherche
	sur les Transports et leur
	Sécurité
INSIA	Instituto Universitario de
	Investigación del Automóvil
IP	Intersection Point
IRC.	Injury Risk Curve
IRCOBI	International Research Council
INCODI	on the Biomechanics of Impact
IRF	Injury Risk Function
ISA	Intelligent Speed Assistance
ISM	Intelligent Speed Management
ISO	International Organization for
	Standardization
ISS	Injury Severity Score
ITC	Inland Transport Committee
	(UN ECE)
1	
J-MUT	Japan: Ministry of Land,
JIVILII	Infrastructure and Transport
JAMA	Japan Automotive
JAIVIA	
	Manufacturers Association
JARI	Japan Automobile Research
	Institute
JASIC	Japan Automobile Standards
	Internationalization Center
JNCAP	Japan New Car Assessment
	Program
V	
K	
KMVSS	Korean Motor Vehicle Safety
	Standards
KNCAP	Korean New Car Assessment
	Program
KTH	Knee - Thigh - Hip



LDWS	Lane Departure Warning
	System
LHD	Left Hand Drive
LIDAR	Light Detection and Ranging
LIN	Local Interconnect Network
LINCAP	Lateral Impact New Car
	Assessment Program (U.S.
	NCAP)
LKAS	Lane Keeping Assist System
LKD	Lane Keeping Device
LKS	Lane Keeping System
LL	Lower Leg
LNL	Lower Neck Load
LSS	Lane Support System
LTR	Land Transport Rules (New
	Zeeland)
м	
MAIS	Maximum AIS (Abbreviated
	Injury Scale)
MCL	Medial Collateral Ligament
MDB	Mobile Deformable Barrier
MOST	Media Oriented Systems
	Transport
MPDB	Moving Progressive
	Deformable Barrier
MSA	Manual Speed Assist
MTBI	Mild Traumatic Brain Injury
MVWG	Motor Vehicle Working Group
	(EU)
N	
NASS	National Automotive Sampling
	System
NASS CDS	NASS Crashworthiness Data
	System
NASS GES	NASS General Estimates System
NASVA	National Agency for
	Automotive Safety & Victims'
	Aid (Japan)
NCAP	New Car Assessment Program
NCSA	National Center for Statistics
	and Analysis (an Office of
	NHTSA)
NHTSA	National Highway Traffic Safety
	Administration (USA)
NIC	Neck Injury Criterion
NNT	Number Needed to Treat
NPACS	New Programme for the
	Assessment of Child-restraint
	Systems
NPRM	Notice of Proposed Rule
	Making
NTSEL	National Traffic Safety and
	Environment Laboratory
	(Japan)
•	
<u>о</u> ос	Occipital Condyles

OC Occi ODB Offse

Occipital Condyles Offset Deformable Barrier



Important Abbreviations

OICA OLC	Organisation Internationale des Constructeurs d'Automobiles Occupant Load Criterion	SINC.
OMDB	Oblique Moving Deformable Barrier	SLD SLIF
OoP	Out of Position	SMA
Ρ		SOB
PADI	Procedures for the assembly	SRA
	disassembly and inspection	SRP
PAEB	Pedestrian Automatic	SRS
	Emergency Braking	
PCL	Posterior Cruciate Ligament	SSF
PDB (1)	Partnership for	
	Dummytechnology and	SSR
	Biomechanics	ST
PDB (2)	Progressive Deformable Barrier	STAT
PDC	Park Distance Control	STNI
PDI	Pedestrian Detection Impactor	SUV
PEAS	Primary Energy Absorbing	SWR
	Structure	
PLI	Pedestrian Legform Impactor	
PMD	Photonic Mixer Device	Т
PMHS	Post Mortem Human Subjects	TCM
PMTO	Post Mortal Test Object	
PNCAP	Primary New Car Assessment	TDM
	Programme	TDM
PoC	Point of Collision	TEG
PP	Pedestrian Protection (Euro	TF B1
	NCAP)	ThCC
PPAD	Partner Protection Assessment	
	Deformation	THO
PSPF	Pubic Symphysis Peak Force	
PTS	Poly Trauma Score	THUI
_		TIPT
R		TREA
Radar	Radio Detection and Ranging	
RCAR	Research Council for	
	Automobile Repairs	TRL
RCTA	Rear Cross Traffic Alert	
RE	Rib Extension (for EuroSID II)	TRT
RFCRS	Rearward Facing Child Restraint	TSP
DUD	System	Π
RHD	Right Hand Drive	TTB
RID	Rear Impact Dummy	TTC
S		TTD
S.O	Statutory Order	
SA SA	Safety Assist (Euro NCAP)	TTP/
SAE	Society of Automotive	TTP/
0,12	Engineers	TTS
SAS	Speed Assistance System	U
SAT	Safety Assist Technology	U.S. I
SB	Seat Back	0.3.1
SBR	Seat Belt Reminder	UAR⁻
SCOE	Standing Committee on	UAR
-	Implementation of Emission	UBM
	Legislation	UMT
SEAS	Secondary Energy Absorbing	UNI
	Structure	
SgRP	Seating Reference Point	UN
SID	Side Impact Dummy	014

SINCAP	Side Impact New Car Assessment Program (U.S. NCAP)
SLD	Speed Limitation Device
SLIF	Speed Limit Information Function
SMA	Shape Memory Alloy
SOB	Small Overlap Barrier (IIHS)
SRA	Swedish Road Administration
SRP	Seat Reference Point
SRS	Supplementary Restraint System
SSF	Static Stability Factor (U.S. NCAP)
SSR	Speed Sign Recognition
ST	Sensing Time
STATS19	British Accident Statistics
STNI	Soft Tissue Neck Injury
SUV	Sports Utility Vehicle
SWR	Strength-to-weight ratio (roof crush)
т	
TCMV	Technical Committee - Motor Vehicles (EU)
TDM	Time Division Multiplex
TDMA	Time Division Multiple Access
TEG	Technical Evaluation Group
TF BTA	Task Force Bumper Test Area
ThCC	Thoracic Compression
	Criterion, also TCC
THOR	Test Device for Human Occupant Restraint
THUMS	Total Human Model for Safety

	Occupant Restraint
THUMS	Total Human Model for Safety
TIPT	Thorax Injury Prediction Tool
TREAD	Transportation Recall,
	Enhancement, Accountability
	and Documentation
TRL	Transport Research Laboratory
	(UK)
TRT	Total Reaction/Response Time
TSP	Top Safety Pick (IIHS)
Π	Top Tether
TTB	Time to Brake
TTC	Time to Collision
TTD	Time to Decision
TTI	Thoracic Trauma Index
TTP/A	Time-Triggered Protocol Class A
TTP/C	Time-Triggered Protocol Class C

TS Time to Steer

U.S. NCAP United States New Car Assessment Program UART Universal Asynchronous Receiver Transmitter UBM Upper Body Mass UMTRI University of Michigan Transportation Research Institute UN United Nations

USCAR	The United States Council for Automotive Research			
v				
VAN	Vehicle Area Network			
VC	Viscous Criterion			
VDC	Vehicle Dynamics Control			
VERPS	Vehicle Related Pedestrian Safety			
vFSS	Advanced Forward Looking Safety Systems (Working Group)			
VNT	Vertical Negative deviation from Target cell load			
VR	Virtual Reality			
VRTC	Vehicle Research & Test Center (NHTSA)			
VRU	Vulnerable Road User			
VSS	Vehicle Safety Score (U.S. NCAP)			
w				
WAD (1)	Wrap Around Distance			
WAD (2)	Whiplash Associated Disorders			
WG	Working Group			
WP	Working Party			
WPI	Worchester Polytechnic			
	Institute			
WS	World SID			

World SID 5th%ile Female

Wayne State University Tolerance Curve

Wayne State University

Dummy

WS5F

WSTC

WSU

UPDATE

SAFETY WISSEN



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All prices mentioned in this publication are exclusive of VAT.

Imprint

Published by

carhs.training gmbh, Siemensstrasse 12, D-63755 Alzenau, Germany Tel. +49 (0) 6023-9640-60, Fax +49 (0) 6023-9640-70 Managing Director: Rainer Hoffmann; Commercial Register: Aschaffenburg HRR 961

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	Echrucary	March	April	May	June
January	February		April	May	
1 Su New Year		1 We	1 Sa	1 Mo Labor Day	1 Th
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3 Tu		3 Fr	3 Mo	3 We	3 Sa
4 We	4 Sa	4 Sa	4 Tu Side Impact p.71	4 Th	4 Su Pentecost
5 Th	5 Su	5 Su	5 We automotive CAE	5 Fr	5 Mo Pentecost
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10 Tu	10 Fr p.104	10 Fr Design Summit Regulations p.16	10 Mo		10 Sa
11 We	11 Sa 1	11 Sa	11 Tu		11 Su
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14 Sa	14 Tu p.137 1	14 Tu Frontal Crashes www	14 Fr Good Friday	14 Su	14 We Safety of Vehicles p.15
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22 Su	22 We Certification Q-Dummies www 2	22 We Crash Safety of Alternative	22 Sa	22 Mo	22 Th NCAP / Active Safety
23 Mo	Titti Bacigio ana, Hacace	23 Th Propulsion Vehicles p.20	23 Su	23 Tu Product Liability in the	23 Fr DCAP / ACLIVE Salety p.118
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3 Mo Autonomous Driving,	3 Th	3 Su	3 Tu German National Holiday	3 Fr p.118	3 Su
4 Tu Advanced Driver Assistance p.115	5 4 Fr	4 Mo Whiplash p.86	4 We Functional Safety	4 Sa	4 Mo Dummy Training THOR
5 We	5 Sa	5 Tu Modeling of Joints www	5 Th ISO 26262 www	5 Su	5 Tu p.104
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11 Tu Restraint Systems p.6:	11 Fr	11 Mo Knee Mapping Workshop p.32	11 We PraxisConference 📃	11 Sa	11 Mo
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13 Th	13 Su	13 We Robust Design p.137	13 Fr Child Protection www	13 Mo Car Body Design for Analysis	13 We
14 Fr	14 Mo	14 Th International Safety and	14 Sa	14 Tu Engineers p.132	14 Th
15 Sa	15 Tu Assumption Day	15 Fr Crash-Test Regulations p.16	15 Su	15 We PraxisConference Rear	15 Fr
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19 We	19 Sa	19 Tu Automotive Design www	19 Th Introduction to Data	19 Su	19 Tu
20 Th	20 Su	20 We Improving Efficiency and	20 Fr Acquisition in Safety Testing p.94	20 Mo Introduction to Passive	20 We
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22 Sa	22 Tu	22 Fr Commercial Vehicle Safety www	22 Su	22 We	22 Fr
23 Su	23 We	23 Sa	23 Mo Advanced Frontal Restraints www	23 Th Lightweight Design Strate-	23 Sa
24 Mo	24 Th	24 Su	24 Tu Material Models of Plastics	24 Fr gies for Car Bodies p.134	24 Su Christmas Eve
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26 We	26 Sa	26 Tu SafetyUpDate Graz2016	26 Th Mat. Models of Metals p.142	26 Su	26 Tu Christmas
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28 Fr	28 Mo	28 Th PraxisConference AEB	28 Sa	28 Tu Cida Import	28 Th
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30 Su	30 We	30 Sa	30 Mo	30 Th	30 Sa
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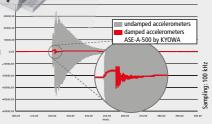
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