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# PDE & Direct Stiffness Method by COMSOL

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#### OUTLINE

- Lecture Goals
  - ✓ COMSOL을 이용한 편미분방정식의 유한요소 해석 시뮬레이션
     및 후처리 과정 전반을 실습하고 직접 강성법 예제를 통해 유한
     요소 해석의 시스템 행렬과 벡터의 개념을 고찰한다.
- Content
  - ✓ PDE Examples
  - ✓ Direct Stiffness Method: Truss
  - ✓ Assignment

- PDE Examples
  - ✓ Laplace equation
  - ✓ Heat conduction equation

m + 1, n + 1

# LAPLACE EQUATION

– PDE → algebraic difference equation



y4

0, n + 1

 $[K_{ij}]$ : coefficient matrix,  $\{T_i\}$ : solution vector,  $\{f_i\}$ : force vector

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# SETTING



# **GEOMETRY CREATION**



Geometry 1 메뉴를 마우스 우클릭 → Rectangle 선택

Width: 4, Height: 4 입력 후 Build Selected 클릭

#### **GEOMETRY CREATION**



# **COEFFICIENT INPUT**



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#### **BOUNDARY CONDITION**



#### **MESH CREATION**



# COMPUTE



# **POST-PROCESSING**



# **POST-PROCESSING**



# **FURTHER CONSIDERATIONS**

- Mesh Type (Free Triangular  $\rightarrow$  Free Quad)
- Solution Type

(Nodal Solution → Element-wise Solution)

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# **MESH CREATION(FREE QUAD)**



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# **MESH CREATION(FREE QUAD)**



# POST PROCESSING(ELEMENT WISE)





# POST PROCESSING(ELEMENT WISE)



#### 후처리를 위한 지배방정식 절점 기반 솔루션 (u) =요소 기반 솔루션 (u2) 요소 기반 솔루션의 경우 한 요소당 하나의 값을 갖고, 요소 간에 불연속한 솔루션 을 갖는다.

- PDE Examples
  - ✓ Laplace equation
  - ✓ <u>Heat conduction equation</u>

# HEAT CONDUCTION EQUATION

Hot

Cool

heat stored in the element over a unit time period  $\Delta t = (In) - (Out)$ 

$$q(x)(\Delta y \Delta z) \Delta t - q(x + \Delta x)(\Delta y \Delta z) \Delta t = \rho C (\Delta x \Delta y \Delta z) \Delta T$$

$$\frac{q(x) - q(x + \Delta x)}{\Delta x} = \rho C \frac{\Delta T}{\Delta t} \xrightarrow{\text{taking the limit}} - \frac{\partial q}{\partial x} = \rho C \frac{\partial T}{\partial t} \xrightarrow{q=-k\rho C \frac{\partial T}{\partial x}} k \frac{\partial^2 T}{\partial x^2} = \frac{\partial T}{\partial t}$$

$$\begin{cases} k = 0.835 \text{ cal/}(\text{s} \cdot \text{cm} \cdot ^\circ \text{C}) \\ \Delta x = 2 \text{ cm} \\ \Delta t = 0.1 \text{ s} \end{cases}$$

$$\begin{cases} \text{Boundary condition} \\ T(0,t) = 100^\circ \text{C} \\ T(10,t) = 50^\circ \text{C} \end{cases} \begin{cases} \text{Initial condition} \\ T(i,t=0) = 0^\circ \text{C} \end{cases}$$

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# SETTING



### **GEOMETRY CREATION**



Geometry 1 우클릭 → Interval 선택

Left: 0, Right: 10 입력 후 Build Selected 클릭

# **COEFFICIENT INPUT**



## **BOUNDARY CONDITION**



#### **MESH CREATION**



# COMPUTE



#### **POST-PROCESSING**



# **POST-PROCESSING**



- Direct Stiffness Method: Truss
  - ✓ <u>Geometry creation</u>
  - ✓ Material property
  - Cross section property
  - ✓ Boundary condition
  - ✓ Nodal force
  - ✓ Analysis

# **EXAMPLE TRUSS STRUCTURE**



Physical structure

Idealization as a pin-jointed bar assemblage



Geometric, material and fabrication properties



Support conditions and applied loads

#### **MODEL WIZARD**

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# **DIMENSION SELECTION**



**M** ~.

# **PHYSICS SELECTION**

		_ 🍟 Structural Mechanics 모
	Untitled.mph - COMSOL Multiphysics	I Truss physics 선택
Model       Definitions       Geometry       Materials         Select Physics            P Chernical Species Transport             P Acoustics           P Acoustics             P Electrochernistry           P Electrochernistry             P Heat Transfer           P Optics             P Plasma           P Plasma             P Plasma           P Plate (plate)             P Plate (plate)           P Plate (plate)             P NULLIDOUT OF Plate (plate)           P Plate (plate)             P Added physics interfaces:           Added physics interfaces:	Physics Mesh Study Results         Image: Search mark         Search mark         The Truss interface is used for modeling slender elements that can only sustain axial forces it can be used for analyzing truss works where the edges are straight, or to model sagging cables like the deformation of a wire exposed to gravity. It is available in 3D and 2D. Geometric nonlinearity can be taken into account. The material is assumed to be linearly elastic.         Image: Mesh Study Results         Image: Remove	Add 클릭
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# **PHYSICS SELECTION**

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Select Physics Recently Used Control Species Transport Control Species T	▶ Study 클릭
548 MB   595 MB	

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# **STUDY TYPE SELECTION**



# **GEOMETRY CREATION**



2 Bezier Polygon 클릭
# **GEOMETRY CREATION**



# **GEOMETRY CREATION**



Control points 시작점 (0,0) 끝나는 점 (10,0) 을 입력

#### 옆의 숫자 1 은 시작점 좌표, 2는 끝나는 점을 의미

<mark>2</mark> Build Selected 클릭

# **GEOMETRY CREATION**





같은 방식으로 총 3개의 직

#### ELEMENT ORDER CHANGING



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#### ELEMENT ORDER CHANGING



Truss physics 클릭

Displacement field 를 Linear 로 변경

- Direct Stiffness Method: Truss
  - ✓ Geometry creation
  - ✓ <u>Material property</u>
  - Cross section property
  - ✓ Boundary condition
  - ✓ Nodal force
  - ✓ Analysis





Geometric, material and fabrication properties





- Direct Stiffness Method: Truss
  - ✓ Geometry creation
  - ✓ Material property
  - ✓ Cross section property
  - ✓ Boundary condition
  - ✓ Nodal force
  - ✓ Analysis



Geometric, material and fabrication properties





Geometric, material and fabrication properties



Geometric, material and fabrication properties

- Direct Stiffness Method: Truss
  - ✓ Geometry creation
  - ✓ Material property
  - Cross section property
  - ✓ **Boundary condition**
  - ✓ Nodal force
  - ✓ Analysis









Prescribed Displacement



Support conditions and applied loads



- Direct Stiffness Method: Truss
  - ✓ Geometry creation
  - ✓ Material property
  - Cross section property
  - ✓ Boundary condition
  - ✓ <u>Nodal force</u>
  - ✓ Analysis

# **POINT LOAD**



# **POINT LOAD**



- Direct Stiffness Method: Truss
  - ✓ Geometry creation
  - ✓ Material property
  - Cross section property
  - ✓ Boundary condition
  - ✓ Nodal force
  - ✓ Analysis









#### COMPUTE



- Stiffness matrix
  - ✓ Global stiffness matrix by hand
  - ✓ Global stiffness matrix by COMSOL



Support conditions and applied loads

$\mathbf{f} = \mathbf{f}^{(1)} + \mathbf{f}^{(2)} + \mathbf{f}^{(3)} = \left(\mathbf{K}^{(1)} + \mathbf{K}^{(2)} + \mathbf{K}^{(3)}\right)\mathbf{u} = \mathbf{K}\mathbf{u}$								
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$f_{x1}$		20	10	-10	0	-10	-10	<i>u</i> <sub>x1</sub>
$f_{y1}$		10	10	0	0	-10	-10	$u_{y1}$
$f_{x2}$	_	-10	0	10	0	0	0	$u_{x2}$
$f_{y2}$	_	0	0	0	5	0	-5	$u_{y2}$
$f_{x3}$		-10	-10	0	0	10	10	<i>u</i> <sub>x3</sub>
$f_{y3}$		10	-10	0	-5	10	15	<i>u</i> <sub>y3</sub>

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- Stiffness matrix confirm
  - ✓ Global stiffness matrix by hand
  - ✓ Global stiffness matrix by COMSOL





<sup>[</sup>Other에서 Assemble 클릭





#### SYSTEM MATRIX


### SYSTEM MATRIX



#### COMPARISON



Support conditions and applied loads

$$\mathbf{f} = \mathbf{f}^{(1)} + \mathbf{f}^{(2)} + \mathbf{f}^{(3)} = \left(\mathbf{K}^{(1)} + \mathbf{K}^{(2)} + \mathbf{K}^{(3)}\right)\mathbf{u} = \mathbf{K}\mathbf{u}$$

$$\begin{bmatrix} f_{x1} \\ f_{y1} \\ f_{x2} \\ f_{y2} \\ f_{y2} \\ f_{x3} \\ f_{y3} \end{bmatrix} = \begin{bmatrix} 20 & 10 & -10 & 0 & -10 & -10 \\ 10 & 10 & 0 & 0 & -10 & -10 \\ 10 & 10 & 0 & 0 & 0 & 0 \\ 0 & 0 & 10 & 0 & 0 & 0 \\ 0 & 0 & 0 & 5 & 0 & -5 \\ -10 & -10 & 0 & 0 & 10 & 10 \\ -10 & -10 & 0 & -5 & 10 & 15 \end{bmatrix} \begin{bmatrix} u_{x1} \\ u_{y1} \\ u_{x2} \\ u_{y2} \\ u_{x3} \\ u_{y3} \end{bmatrix}$$

#### **COMSOL** Result

Load Vector

Stiffness matrix

0	20.000	10.0000	-10.0000	0.0000	-10.0000	-10.0000
0	10.0000	10.0000	0.0000	0.0000	-10.0000	-10.0000
0	-10.0000	0.0000	10.0000	0.0000	0.0000	0.0000
0	0.0000	0.0000	0.0000	5.0000	0.0000	-5.0000
2	-10.0000	-10.0000	0.0000	0.0000	10.0000	10.0000
1	-10.0000	-10.0000	0.0000	-5.0000	10.0000	15.000

### LOCAL STIFFNESS MATRIX



Stiffness matrix by COMSOL

10.0000	0.0000	-10.0000	0.0000
0.0000	0.0000	0.0000	0.0000
-10.0000	0.0000	10.0000	0.0000
0.0000	0.0000	0.0000	0.0000

0.0000	0.0000	0.0000	0.0000
0.0000	5.0000	0.0000	-5.0000
0.0000	0.0000	0.0000	0.0000
0.0000	-5.0000	0.0000	5.0000

10.0000	10.0000	-10.0000	-10.0000
10.0000	10.0000	-10.0000	-10.0000
-10.0000	-10.0000	10.0000	10.0000
-10.0000	-10.0000	10.0000	10.0000

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## LOCAL STIFFNESS MATRIX



# LOCAL STIFFNESS MATRIX





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į	-10.	000	-10	0.000	10.	000	10.0	00	

#### **REDUCED STIFFNESS MATRIX**

$$\begin{cases} \text{Displacement BCs: } u_{x1} = u_{y1} = u_{y2} = 0 \\ \text{Force BCs: } f_{x2} = 0, \ f_{x3} = 2, \ f_{y3} = 1 \end{cases}$$

$$\rightarrow \begin{bmatrix} 20 & 10 & -10 & 0 & -10 & -10 \\ 10 & 10 & 0 & 0 & -10 & -10 \\ -10 & 0 & 10 & 0 & 0 & 0 \\ 0 & 0 & 0 & 5 & 0 & -5 \\ -10 & -10 & 0 & 0 & 10 & 10 \\ -10 & -10 & 0 & -5 & 10 & 15 \end{bmatrix} \begin{bmatrix} u_{x1} \\ u_{y1} \\ u_{x2} \\ u_{y2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} f_{x1} \\ f_{y1} \\ f_{x2} \\ f_{y2} \\ f_{x3} \\ f_{y3} \end{bmatrix}$$

Strike out rows and columns pertaining to known displacements:

$$\begin{bmatrix} 10 & 0 & 0 \\ 0 & 10 & 10 \\ 0 & 10 & 15 \end{bmatrix} \begin{bmatrix} u_{x2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} f_{x2} \\ f_{x3} \\ f_{y3} \end{bmatrix} = \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix} \Leftrightarrow \hat{\mathbf{K}}\hat{\mathbf{u}} = \hat{\mathbf{f}}$$

Solve by Gauss elimination for unknown node displacements

Eliminated Stiffness matrix

10.000	0.0000	0.0000
0.0000	10.000	10.000
0.0000	10.000	15.000

Eliminated Load vector

0	
2	
1	ſ

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#### NODAL DISPLACEMENT



#### NODAL DISPLACEMENT



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#### NODAL DISPLACEMENT



### NODAL REACTION FORCE



#### NODAL REACTION FORCE



COMSOL의 Load벡터는 Reaction force와 B.C인 Point load를 구분해서 출력

Reaction force, x component (N), Point: 1	Reaction force, y component (N), Point: 1
-2.0000	-2.0000
Reaction force, x component (N), Point: 2	Reaction force, y component (N), Point: 2
0.0000	1.0000
Reaction force, x component (N), Point: 3	Reaction force, y component (N), Point: 3
0.0000	0.0000

#### Type filter text

- Component 1
  - Definitions
  - Geometry
  - Truss
    - Acceleration and velocity
    - Displacement
    - Energy and power
    - Geometry
    - Load
      - truss.FpMag Point load magnitude
      - Point load

truss.Fpx - Point load, x component truss.Fpy - Point load, y component

Point load, x component (N), Point: 3 Point load, y component (N), Point: 3 2.0000 1.0000

#### **EXAMPLE TRUSS STRUCTURE**



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## **BOUNDARY CONDITION**



기존 경계조건인 pinned 와 symmetry 조건 삭제 후 Prescribed Displacement 경계조건 2 개 생성

## **BOUNDARY CONDITION**



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### **BOUNDARY CONDITION**



#### COMPUTE



#### RESULT

Transfer effect of known displacements to RHS, and delete columns:

$$\begin{bmatrix} 10 & 0 & 0 \\ 0 & 10 & 10 \\ 0 & 10 & 15 \end{bmatrix} \begin{bmatrix} u_{x2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix} - \begin{bmatrix} (-10) \times 0 + 0 \times (-0.5) + 0 \times 0.4 \\ (-10) \times 0 + (-10) \times (-0.5) + 0 \times 0.4 \\ (-10) \times 0 + (-10) \times (-0.5) + (-5) \times 0.4 \end{bmatrix} = \begin{bmatrix} 0 \\ -3 \\ -2 \end{bmatrix}$$

Solving gives



In summary, the only changes to the SDM is in the application of displacement boundary conditions before solve

Nodal displacement by COMSOL

Displacement field, x component (m), Point: 1	Displacement field, x component (m), Point: 2	Displacement field, x component (m), Point: 3
0.0000	0.0000	-0.50000

Displacement field, y component (m), Point: 1	Displacement field, y component (m), Point: 2	Displacement field, y component (m), Point: 3
-0.50000	0.40000	0.20000

#### ASSIGNMENT



E = 210 GPa $A = 6 \times 10^{-4} \text{ m}^2$ 

 $\therefore d_{1y} = 0.0337 \text{ m}$ 

① derive K matrix

- 2 calculate y-displacement at node 1
- ③ compare with COMSOL result

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