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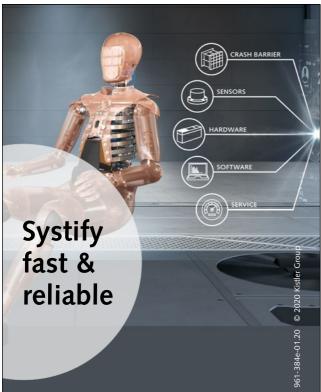
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Safety**Companion** 2021



Passive Safety

Dummy & Crash Test



Page 116 - 128

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Page 129 - 165



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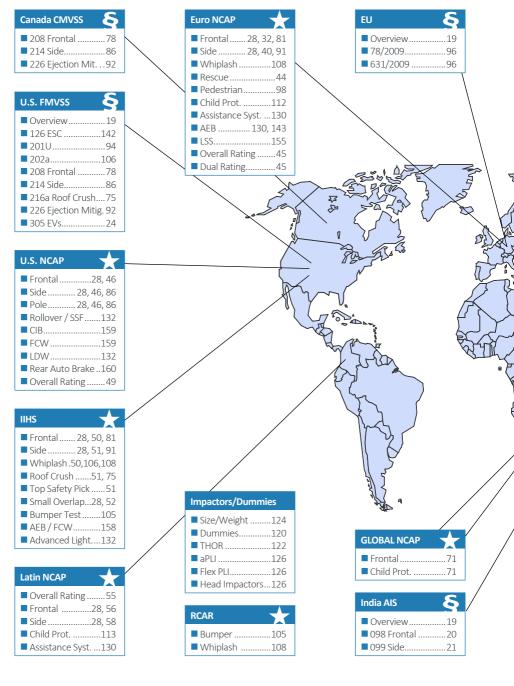






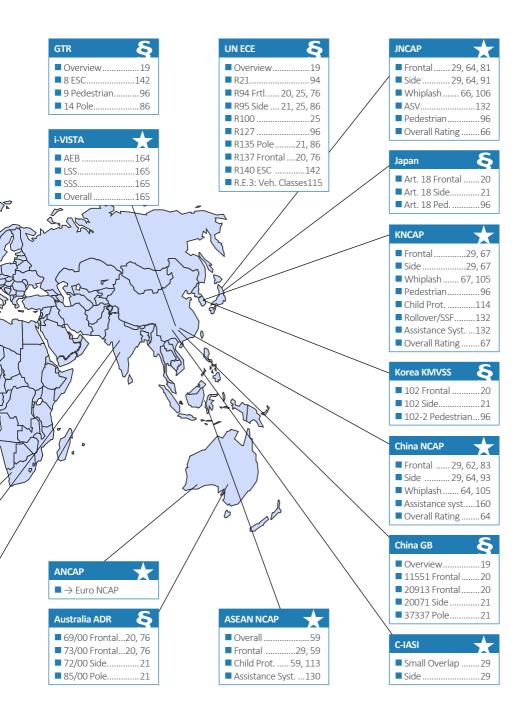


SafetyWissen Navigator











Seminar Guide

Here you find the courses you need to get your job done!



Frontal Impact

- Workshop Euro NCAP MPDB Frontal Crash p. 37
- Knee Mapping Workshop p. 38
- Development of Frontal Restraint Systems p. 77
- Rear Seat Occupant Protection in Frontal Impact p. 84
- Child Protection in Front and Side Impacts p. 111
- Automotive Safety Summit Shanghai p. 13
- SafetyUpDate p. 15
- Introduction to Passive Safety p. 16
- International Safety and Crash-Test Regulations p. 18
- NCAP New Car Assessment Programs p. 30
- Crashworthy and Lightweight Car Body Design p. 74
- Crash-Sensing and Intelligent Restraint Systems p. 85
- Passenger Cars in Low-Speed Crashes p. 104



Side Impact

- Side Impact Requirements and Development Strategies p. 90
- Child Protection in Front and Side Impacts p. 111
- Automotive Safety Summit Shanghai p. 13
- SafetyUpDate p. 15
- Introduction to Passive Safety p. 16
- International Safety and Crash-Test Regulations p. 18
- NCAP New Car Assessment Programs p. 30
- Crashworthy and Lightweight Car Body Design p. 74

Restraint Systems

- Development of Frontal Restraint Systems p. 77
- Development of Frontal Restraint Systems -Advanced p. 79
- Early Increase of Design Maturity of Restraint System Components in the Reduced Prototype Vehicle Development Process p. 80
- Rear Seat Occupant Protection in Frontal Impact p. 84
- Crash-Sensing and Intelligent Restraint Systems p. 85
- Automotive Safety Summit Shanghai p. 13
- SafetyUpDate p. 15
- Introduction to Passive Safety p. 16
- Introduction to Impact Biomechanics and Human Body Models p. 168

Pedestrian Protection

- PraxisConference Pedestrian Protection p. 97
- Pedestrian Protection Strategies p. 102
- Workshop Pedestrian Protection and Low Speed Crash p. 103
- Pedestrian Protection Test Procedures p. 128
- Pedestrian Protection Workshops p. 128
- Automotive Safety Summit Shanghai p. 13
- SafetyUpDate p. 15
- Introduction to Passive Safety p. 16
- International Safety and Crash-Test Regulations p. 18
- NCAP New Car Assessment Programs p. 30
- Crashworthy and Lightweight Car Body Design p. 74
- Passenger Cars in Low-Speed Crashes p. 104

Rear Impact



- PraxisConference Rear Impact Seats -Whiplash p. 107
- Whiplash Testing and Evaluation in Rear Impacts p. 109
- SafetyUpDate p. 15
- Introduction to Passive Safety p. 16
- International Safety and Crash-Test Regulations p. 18
- NCAP New Car Assessment Programs p. 30



Dummies + Crash Test

- SafetyTesting p. 116
- Introduction to Data Acquisition p. 117
- Dummy Training p. 125
- Automotive Safety Summit Shanghai p. 13
- SafetyUpDate p. 15
- Introduction to Passive Safety p. 16
- Introduction to Impact Biomechanics and Human Body Models p. 168

Legend

- Seminar/Event that focusses on this topic
- Seminar/Event that deals with this topic (among others)





Regulations and Requirements

- International Safety and Crash-Test Regulations p. 18
- Vehicle Safety under Self-Certification p. 26
- Crash Safety of Hybrid- and Electric Vehicles p. 22
- Euro NCAP Update p. 27
- NCAP New Car Assessment Programs p. 30
- Product Liability in the Automobile Industry p. 72
- Briefing on the Worldwide Status of Automated Vehicle Policies p. 137
- Automotive Safety Summit Shanghai p. 13
- SafetyUpDate p. 15
- Introduction to Passive Safety p. 16
- PraxisConference Safety Assist p. 136

Car Bodies

- Crashworthy and Lightweight Car Body Design p. 74
- Robust Design and Stochastics for Car Body Development p. 172
- Automotive Safety Summit Shanghai p. 13
- Introduction to Passive Safety p. 16
- Lightweight Design Summit p. 170



Interiors

- Knee Mapping Workshop p. 38
- Head Impact on Vehicle Interiors p. 95
- Whiplash Testing and Evaluation p. 109



Tools & Methods

- Introduction to Artificial Intelligence and Machine Learning for Advanced Driver Assistance Systems and Automated Driving Functions p. 140
- Scenario-, Simulation- and Data-based Development, Validation and Safeguarding of Automated Driving Functions p. 141
- automotive CAE Grand Challenge p. 166
- Introduction to Impact Biomechanics and Human Body Models p. 168
- Introduction to the Python Programming Language p. 181
- Python based Machine Learning with Automotive Applications p. 182

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Accident Avoidance, Automated Driving

- Automotive Safety Summit Shanghai p. 13
 SafetyWeek p. 14
- Introduction to Active Safety p. 129
- Advances in Sensors for Automated Driving p. 135
- PraxisConference Safety Assist p. 136
- Briefing on the Worldwide Status of Automated Vehicle Policies p. 137
- Auto[nom]Mobil p. 139
- Introduction to Artificial Intelligence and Machine Learning for Advanced Driver Assistance Systems and Automated Driving Functions p. 140
- Scenario-, Simulation- and Data-based Development, Validation and Safeguarding of Automated Driving Functions p. 141
- Automotive Safety Summit Shanghai p. 13
- SafetyUpDate p. 15
- NCAP New Car Assessment Programs p. 30

Crash Simulation



- Introduction to Impact Biomechanics and Human Body Models p. 168
- Design of Composite Structures p. 176
- Material Models of Composites p. 177
- Material Models of Metals p. 178
- Material Models of Plastics and Foams p. 179
- Modeling of Joints in Crash Simulation p. 180
- Crashworthy and Lightweight Car Body Design p. 74
- Automotive CAE Grand Challenge p. 166
- Robust Design and Stochastics for Car Body Development p. 172





SafetyCompanion 2021

- 4 SafetyWissen Navigator
- 6 Seminar Guide
- 10 Preface
- 11 Seminars at carhs.training Your Benefits
- 12 In-house Seminars

Passive Safety

- 13 Event: Automotive Safety Summit Shanghai
- 14 Event: SafetyWeek
- 15 Event: SafetyUpDate
- 16 Seminar: Introduction to Passive Safety of Vehicles
- 17 Seminar: Safety of Commercial Vehicles
- 18 Seminar: International Safety and Crash-Test Regulations
- 19 **SafetyWissen:** Crash-Regulations: Europe, United Nations, USA, China and India
- 20 SafetyWissen: Rules and Regulations on Occupant Protection
- 22 Seminar: Crash Safety of Hybrid and Electric Vehicles
- 24 SafetyWissen: FMVSS 305: Safety Requirements for Electric Vehicles
- 25 SafetyWissen: UNECE: Safety Requirements for Electric Vehicles
- 26 Seminar: Vehicle Safety under Self-Certification
- 27 Euro NCAP UpDate 2020
- 28 **SafetyWissen:** NCAP-Tests in Europe, America and Australia
- 29 SafetyWissen: NCAP-Tests in Asia
- 30 Seminar: NCAP New Car Assessment Programs
- 32 SafetyWissen: Euro NCAP / ANCAP
- 37 Seminar: Euro NCAP MPDB Frontal Crash Workshop
- 38 Seminar: Euro NCAP Knee Mapping Workshop
- 46 SafetyWissen: U.S. NCAP: Tests and Criteria
- 50 SafetyWissen: IIHS Rating
- 55 SafetyWissen: Latin NCAP Rating: 2020 2024
- 59 SafetyWissen: ASEAN NCAP
- 60 SafetyWissen: C-NCAP
- 64 SafetyWissen: JNCAP
- 67 SafetyWissen: KNCAP
- 71 SafetyWissen: GLOBAL NCAP #SAFERCARSFORAFRICA #SAFERCARSFORINDIA
- 72 **Seminar:** Product Liability in the Automobile Industry
- 73 Seminar: Static Vehicle Safety Tests in Automotive Development
- 74 Seminar: Crashworthy and Lightweight Car Body Design
- 75 SafetyWissen: Roof Crush Requirements
- 76 SafetyWissen: Protection Criteria for Frontal Impact Tests

- 77 **Seminar:** Development of Frontal Restraint Systems meeting Legal and Consumer Protection Requirements
- 78 SafetyWissen: FMVSS 208: Frontal Impact Requirements: In-Position
- 78 FMVSS 208: Frontal Impact Requirements: Out of Position
- 79 Seminar: Development of Frontal Restraint Systems - Advanced
- 80 **Seminar:** Early Increase of Design Maturity of Restraint System Components in the Reduced Prototype Vehicle Development Process
- 81 SafetyWissen: Frontal Impact Protection Criteria Compared
- 83 **SafetyWissen:** Safety Requirements for Rear Seats and Restraint Systems
- 84 **Seminar:** Rear Seat Occupant Protection in Frontal Impact
- 85 **Seminar:** Crash-Sensing and Intelligent Restraint Systems
- 86 SafetyWissen: Side Impact Test Procedures
- 88 SafetyWissen: Seat Adjustments for Side Impact Tests
- 90 Seminar: Side Impact Requirements and Development Strategies
- 91 SafetyWissen: Side Impact Protection Criteria Compared
- 92 SafetyWissen: FMVSS 226, CMVSS 226 Ejection Mitigation
- 94 SafetyWissen: Regulations for Head Impact on Vehicle Interiors
- 95 Seminar: Head Impact on Vehicle Interiors: FMVSS 201 and UN R21
- 96 SafetyWissen: Test Procedures and Protection Criteria for Pedestrian Protection
- 97 Event: PraxisConference Pedestrian Protection
- 98 SafetyWissen: Pedestrian Protection Impact Areas
- 100 SafetyWissen: Head and Leg Impact Grid Method
- 102 **Seminar:** Pedestrian Protection Development Strategies
- 103 **Seminar:** Workshop Pedestrian Protection and Low Speed Crash
- 104 Seminar: Passenger Cars in Low-Speed Crashes
- 105 SafetyWissen: RCAR Insurance Tests
- 106 SafetyWissen: Whiplash Requirements Front Seats
- 107 Event: PraxisConference Rear Impact Seats -Whiplash
- 108 SafetyWissen: Euro NCAP / ANCAP Front Seat Whiplash Assessment
- 108 SafetyWissen: Static Geometry Assessment by IIWPG / IIHS
- 109 **Seminar:** Whiplash Testing and Evaluation in Rear Impacts





- 110 SafetyWissen: Euro NCAP / ANCAP Rear Seat Whiplash Assessment
- 111 Seminar: Child Protection in Front and Side Impacts
- 112 SafetyWissen: Euro NCAP / ANCAP Child Occupant Protection
- 113 SafetyWissen: Latin NCAP Child Occupant Protection
- 113 SafetyWissen: ASEAN NCAP Child Occupant Protection 2021 - 2025
- 114 SafetyWissen: KNCAP Child Occupant Protection
- 115 SafetyWissen: UNECE Vehicle Classification

Dummy & Crash Testing

- 116 Event: SafetyTesting
- 117 **Seminar:** Introduction to Data Acquisition in Safety Testing
- 118 SafetyWissen: Highspeed Camera Recording Settings
- 120 SafetyWissen: Current Dummy Landscape
- 122 SafetyWissen: THOR 50 % Male
- 124 **SafetyWissen:** Dummies: Weights, Dimensions and Calibration
- 125 Seminar: Dummy-Trainings
- 126 SafetyWissen: Impactors for Pedestrian Protection
- 128 Seminar: Pedestrian Protection Test Procedures
- 128 Seminar: Pedestrian Protection Workshop: aPLI
- 128 **Seminar:** Pedestrian Protection Workshop: Vehicle Mark-Up

Active Safety & Automated Driving

- 129 Seminar: Introduction to Active Safety of Vehicles
- 130 SafetyWissen: NCAP Tests for Active Safety and Driver Assistance
- 134 SafetyWissen: NCAP Assistance System Rating Matrix
- 135 Seminar: Advances in Sensors for Automated Driving
- 136 Event: Praxis Conference Safety Assist
- 137 **Seminar:** Briefing on the Worldwide Status of Automated Vehicle Policies
- 138 SafetyWissen: Levels of Driving Automation
- 139 Event: Auto[nom]Mobil
- 140 **Seminar:** Introduction to Artificial Intelligence and Machine Learning for Advanced Driver Assistance Systems and Automated Driving Functions
- 141 **Seminar:** Scenario-, Simulation- and Data-based Development, Validation and Safeguarding of Automated Driving Functions
- 142 SafetyWissen: Test of ESC Systems in UN R140, GTR 8 and FMVSS 126
- 143 **SafetyWissen:** Euro NCAP / ANCAP Test Method for AEB VRU-Pedestrian
- 146 SafetyWissen: Euro NCAP / ANCAP Test Method for AEB VRU-Cyclist

- 149 SafetyWissen: Test Method for AEB PTW
- 150 **SafetyWissen:** Test Method for Lane Support Systems PTW
- 152 SafetyWissen: Euro NCAP / ANCAP Test Method for AEB Car-to-Car
- 155 **SafetyWissen:** Euro NCAP / ANCAP Test Method for Lane Support Systems
- 157 Seminar: NCAP New Car Assessment Programs
- 158 SafetyWissen: IIHS AEB / Front Crash Prevention Test
- 158 SafetyWissen: IIHS Test Scenarios for AEB Pedestrian
- 159 SafetyWissen: U.S. NCAP Crash Imminent Braking
- 159 SafetyWissen: U.S. NCAP Forward Collision Warning
- 160 SafetyWissen: U.S. NCAP Rear Automatic Braking
- 161 SafetyWissen: C-NCAP Active Safety Rating
- 164 SafetyWissen: i-VISTA Intelligent Vehicle Integrated Systems Test Area

Simulation & Engineering

- 166 Event: automotive CAE Grand Challenge
- 168 **Seminar:** Introduction to Impact Biomechanics and Human Body Models
- 170 Event: Lightweight Design Summit
- 170 Leichtbaugipfel
- 172 **Seminar:** Robust Design Vehicle Development under Uncertainty
- 173 **Seminar:** Interior Development Fundamentals, Materials, Design, Manufacturing
- 174 **Seminar:** Structural Optimization in Automotive Design
- 175 **Seminar:** Improving Efficiency and Reducing Risk in CAE Driven Product Development
- 176 Seminar: Design of Composite Structures
- 177 **Seminar:** Material Models of Composites for Crash Simulation
- 178 **Seminar:** Material Models of Metals for Crash Simulation
- 179 **Seminar:** Material Models of Plastics and Foams for Crash Simulation
- 180 Seminar: Modeling of Joints in Crash Simulation
- 181 **Seminar:** Introduction to the Python Programming Language
- 182 **Seminar:** Python based Machine Learning with Automotive Applications
- 183 SafetyWissen: Important Abbreviations
- 186 Terms & Conditions
- 187 Index
- 189 Seminar Calendar





Safety as the Prerequisite for Automated Driving

"One of the biggest challenges ahead for the industry will be to determine when autonomous vehicles are safe enough for road use," says Michael Ramsey, senior director analyst at Gartner¹.

It is hard to say when the vehicle safety development as we know it today started. However the year 1959 saw two important milestones that determined the way safety went. In 1959 Volvo introduced the 3-point safety belt invented by Nils Bohlin and in 1959 Mercedes-Benz started with systematic crash testing. More than 60 years have passed and safety has reached a high standard. And that is Passive safety.

SAFETY COMPANION SafetyWissen on 88 pages More than 110 seminars & events

In terms of safety for automated and autonomous cars, we are back at the beginning. Despite the huge amounts of money that have been invested, no automated or autonomous cars, i.e. SAE Level 3 or higher are on the market yet. The recently passed UN Regulation 157 on Automated Lane Keeping Systems (ALKS) is a first small step. But we are still far away from realizing the big potentials and expectations raised by the automation of vehicles.

What does it take to assess and certify the safety of Automated Driving Systems (ADS)? In fact we don't know yet. Lawmakers around the world are struggling to define the procedures for assessment and regulations. What we know already is that established procedures to ensure safety like the UN Regulations on Passive Safety or NCAP assessments for assistance functions will not be sufficient to bring the safety of ADS to the level we want to see: to be better than a human driver. Instead it will be necessary to evaluate many possible driving scenarios, maybe hundreds of millions to find the problematic ones and ensure safety.

Furthermore the development of a car will not be over, once it enters the market. Life Cycle Management will become a critical aspect of cars with ADS to ensure that future knowledge will become available even to a vehicle already on the road.

At carhs.training we are following the international developments in rule making and assessment protocols very closely and support you in their interpretation for your work through our attractive training programs consisting of seminars, hands-on conferences and events, the SafetyWissen.com online platform and last but not least by means of the SafetyCompanion that you hold in your hands right now.

The 2021 SafetyCompanion is now more interactive than ever: We have added QR-codes that give you direct access to the wealth of information on SafetyWissen.com. The PDF Version of the SafetyCompanion goes even further: Wherever a reference to a regulation text or a protocol is given, by just clicking on the reference, the full document is available for you.

But documents are only the basis: Our trainers and speakers have the expertise to turn information into knowledge that helps you accelerate the successful development of new cars meeting all the requirements.

In order to make it even easier for you to participate in our events, we now offer these events both as on site and online events. So every participant has the possibility to choose their preferred way of attending.

For the whole team of carhs.training

Rainer Hoffmann President & CEO

all but

Ralf Reuter Executive Vice President

¹ "Gartner Forecasts More Than 740,000 Autonomous-Ready Vehicles to Be Added to Global Market in 2023", Press Release Gartner Group, STAMFORD, Conn., November 14, 2019



Seminars at carhs.training - Your Benefits



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References

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NEW Customer Specific Online-Seminars

Instead of an in-house-seminar, customers can now book our seminars as a customer specific online-seminar. This gives customers the option to choose the date, duration & pace of the seminar and enables them to let staff from multiple locations take part without extra travel expenses.



Active & Passive Safety Event

AUTOMOTIVE Safety Summit Shanghai 2021

Safety Technologies for the intelligent, autonomous and electrified Automobile of the Future.

The »Automotive Safety Summit Shanghai« is attracting more than 300 automotive safety experts from China and beyond to discuss the latest requirements and innovations in active and passive safety. Accompanied by a comprehensive trade show with the worldwide vendors in development technologies and services, the summit is the leading event for everyone involved in automotive safety. The 2021 event will focus on automotive safety in the context of current Megatrends: NEV, ADAS and AD.

Join »Automotive Safety Summit Shanghai« at the Kerry Hotel in Pudong, Shanghai, China.

Keynotes from international experts, presentations on requirements and innovations, the latest developments in testing and simulation for active and passive systems will make this event a true highlight for every decision maker and engineer in the fields of active and passive safety. With the rapid rise of New Energy Vehicles (EV, PHEV and FCV), new challenges are surfacing for the safety community. The »Automotive Safety Summit Shanghai« is setting a focal point on Safety of New Energy Vehicles, discussing requirements, technologies and validation aspects for safety of NEVs.

The event will have dedicated sessions on the following topics:

- Safety in Autonomous Driving Systems
- Legal Requirements for Level 3 and beyond
- Advances in World-wide NCAP Programs
- Safety of New Energy Vehicles
- Vulnerable Road Users
- New Testing Technology for ADAS and ADS
- Safety Simulation for Autonomous Driving
- Human Modeling and Simulation for Safety

Who should attend?

»Automotive Safety Summit Shanghai« is addressing decision makers and engineers at all stages of the development phase, managers during the conceptual phase who need to understand upcoming global requirements, design engineers, testing and simulation specialists.

DATE VENUE HOMPAGE LANGUAGE 15.-16.07.2021

Shanghai, CHINA <mark>& ONLINE</mark>

www.carhs.de/safetysummit

English / Chinese with simultaneous translation















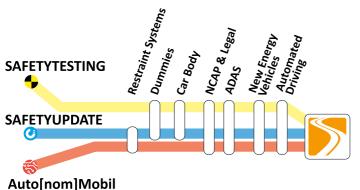


Supporting automotive development engineers to further improve automotive safety, that is the essence of SafetyWeek.

In a unique combination of knowledge congress, events and exhibition, SafetyWeek offers participants and visitors the opportunity, to bring their expertise up-to-date and to learn about the latest developments and technologies in product development and product verification.

In 2021 SafetyWeek will feature numerous highlights:

- The knowledge congress **SafetyUpDate***+active* with the most current updates on requirements and solutions in active and passive safety. ⊃ page 15
- The SafetyTesting+active with the innovations from the Leaders in Testing and Simulation of components and systems in active and passive safety.
 ⇒ page 116
- Auto[nom]Mobil, the expert forum on safe urban mobility **>** page 139
- The accompanying exhibition SafetyExpo, the meeting point for suppliers and decision makers in automotive safety.





SafetyWeek is the meeting point for everyone involved in vehicle safety. This includes developers as well as test and simulation engineers from OEMs and suppliers, manufacturers of test systems, representatives of governments and consumer protection organizations and researchers from universities and research institutes.



date Venue

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LANGUAGE

31.08.-02.09.2021

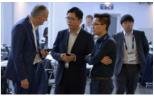
Würzburg, GERMANY & ONLINE

GE www.carhs.de/safetyweek

English or German with translation into English













Active & Passive Safety Event

SAFETYUPDATE

The concept is familiar: To keep software up-to-date you regularly make an update. The same is true for automotive safety engineering: To keep yourself up-to-date you have to attend the SafetyUpDate on a regular basis. Here you get a comprehensive overview of all relevant news in automotive safety.

Active + Passive Safety = SafetyUpDate+active

The SafetyUpDate reflects the close integration of active and passive safety and combines both topics in one event. General topics such as the NCAP consumer tests are dealt with in plenary presentations, whereas specific topics such as testing are presented in parallel session on active respectively passive safety.

Conference Topics include:

- Regulations for active & passive safety and assisted, automated & autonomous driving
- NCAP consumer protection tests
- Development tools: Test & simulation
- Development strategies & solutions
- Biomechanics & accident research

From Experts for Experts

The speakers are leading experts from government agencies, consumer protection organizations, industry and universities. We consider it important that the UpDate presentations are product-neutral and practical.

Meeting Point: Expert Dialog

In addition to the presentations the SafetyUpDate encourages the communication among experts. After the presentations the speakers are available for discussions at the MeetingPoint.

Who should attend?

DATE

VENUE

HOMPAGE

LANGUAGE

The SafetyUpDate is aimed at automotive developers, who are interested in active or passive vehicle safety and want to bring their knowledge up-to-date. In addition to the knowledge update, SafetyUpDate offers excellent opportunities to build and maintain contacts in the safety community.









Facts

01.-02.09.2021

Würzburg, GERMANY & ONLINE

www.carhs.de/update

German with translation into English

20.-21.09.2021 Graz, AUSTRIA

www.carhs.de/gsu







Introduction to Passive Safety of Vehicles

Course Description

Ever increasing requirements regarding vehicle safety have led to rapid developments, with major innovations in the field of Active and Passive Safety. Especially legal requirements in the USA (FMVSS 208, 214), the consumer information tests U.S. NCAP, Euro NCAP and IIHS, as well as pedestrian protection should be mentioned here. So far an end of this development is not in sight.

The seminar provides an introduction to Passive Safety of Vehicles. Passive Safety is about initiatives and legal provisions for the limitation of injuries following an accident. All important topics are covered in the seminar, from accident statistics and injury-biomechanics, which are decisive parts of accident research, to the crash-rules and regulations that are derived from the latter, and also to consumer information-tests with protection criteria and test procedures, and eventually to crash tests, where the compliance with the compulsory limits is tested and proven in test procedures. Specific attention is given to dummies, with which the potential loads on a person in an accident can be measured. Finally the basic principles of occupant protection are explained, and the components of occupant protection systems, respectively restraint-systems in motor vehicles such as airbags, belt-system, steering wheel, seat, interior, stiff passenger compartment and others, as well as their increasingly complex interaction, also in terms of new systems, will be discussed.

Course Objectives

It is the primary objective of this seminar to communicate an understanding for the entire field of Passive Safety with all its facets and correlations, but also for its limits and trends. In the seminar you are going to learn about and understand the most important topics and can then judge their importance for your work. With the extensive, up-to-date documentation you obtain a valuable and unique reference book for your daily work.

Who should attend?

The seminar addresses everybody who wants to obtain an upto-date overview of this wide area. It is suited for novices in the field of Passive Safety of Vehicles such as university graduates, career changers, project assistants, internal service providers, but also for highly qualified technicians from the crash-test lab.

Course Contents

- Introduction to vehicle safety
 - Overview active and passive safety
 - Crash physics
- Accident research
 - General accident research
 - Classifications
 - Statistics
- Biomechanics
 - Human anatomy
 - Injury mechanisms
 - Injury criteria
- Dummy technology
 - Dummy family
- Crash testing
 - Crash test systems and components
 - Test methods
- Crash regulations and NCAP tests
 - Institutions
 - Passive safety regulations
 - NCAP tests
 - Insurance tests (IIHS, RCAR, C-IASI, ...)
 - Protection principles, occupant protection systems
 - Protection principles of passive safety
 - Occupant protection systems
 - Passenger compartment, interior with steering wheel and steering column, seat
 - OOP, pre crash, post crash, sensor system, vehicle body
 - Optimization of restraint systems, adaptive systems
 - Integrated safety



Ralf Reuter (carhs.training gmbh) studied mechanical engineering and business administration at the technical universities of Darmstadt and Eindhoven. Since 1997 he has worked for carhs in various management positions. He deals with vehicle safety issues intensively, in particular with the latest developments in rules and regulations as well as consumer testing. As he is in charge of the SafetyWissen which has been published by carhs for many years, he keeps his knowledge up-to-date and profits from the inputs of carhs' trainer and expert network.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
ő	2326.02.2021	17/3769	Online ¹	4 Days	790,- EUR till 26.01.2021, thereafter 940,- EUR	
	1417.06.2021	17/3751	Online ¹	4 Days	790,- EUR till 17.05.2021, thereafter 940,- EUR	
	1516.06.2021	17/3770	Landsberg am Lech	2 Days	1.340,- EUR till 18.05.2021, thereafter 1.590,- EUR	
	31.0801.09.2021	17/3771	Tappenbeck	2 Days	1.340,- EUR till 03.08.2021, thereafter 1.590,- EUR	
	2324.11.2021	17/3772	Alzenau	2 Days	1.340,- EUR till 26.10.2021, thereafter 1.590,- EUR	

¹ Online Seminar with reduced content





Auf Deutscl



Safety of Commercial Vehicles

Course Description

Due to increasing transport services in road freight traffic and the comparatively high number of fatal accidents, vehicle safety in commercial vehicles is increasingly becoming the focus and initial successes have already been recorded. The number of accident victims in accidents with heavy commercial vehicles has fallen by around 35% since the turn of the millennium. With current adjustments in European legislation on active and passive commercial vehicle safety, there are also development requirements that go far beyond the previous level. A major step towards improving active safety is, for example, the adoption of the UN regulations UN R130 and UN R131, which have introduced autonomous emergency braking systems (Advanced Emergency Braking Systems, AEBS) and Lane Departure Warning (LDW) since November 1, 2015 for all heavy-duty vehicles. Both systems have great potential for avoiding rear-end, two-way traffic and rollover accidents or at least for reducing the consequences of an accident. Activities are currently underway to further tighten UN R131 and the UN R151 regulation on Blind Spot Information Systems (Turning assistance) is being introduced into the approval regulations of the UN ECE member states. However, the design of direct and indirect fields of vision (e.g. also via cameras), the cab structure, load securing and underride protection systems are still of major importance with regard to commercial vehicle safety. In this context, among other things, the regulation UN R29 on the crash behavior of the cab structure and the UN R58.03 on the rear underrun protection are of central importance.

Course Objectives

In this seminar you will get an overview of the requirements and regulations of different vehicle classes and types in the commercial vehicle sector. There is a consideration of today's legal requirements in the areas of passive and in particular active vehicle safety. Based on the requirement profile, the current state-of-the-art as well as current trends are shown.

Who should attend?

The seminar is focused on specialists and experts from the passenger car and commercial vehicle sector, engineers and technicians from calculation and testing, project engineers and managers, who want to get an overview of the requirements and technological solutions for the development of safety-relevant systems for commercial vehicles and the resulting conclusions to provide compatibility with other road users.

Course Contents

- Requirements for commercial vehicle development
 - Vehicle classes and types for commercial vehicles
 - Design of heavy commercial vehicles
 - Drivers in the development of commercial vehicles
- Measures for passive safety
 - Overview of regulations and test methods for passive commercial vehicle safety
 - Effects of the regulations on vehicle design
 - Technological feasibility
 - Protection potential and limits of passive safety measures
- Measures for active safety
 - Overview of regulations and test methods for active commercial vehicle safety
 - Effects of the regulations on vehicle design
 - Technological feasibility
 - Protection potential and limits of active safety measures
 - Development strategies
 - Energy management
 - Structural design for passive safety
 - Compatibility considerations
 - Solution approaches for conflicting objectives
 - Simulation of driving sequences in active safety



Prof. Dr. Harald Bachem (Ostfalia University of Applied Sciences) has been in charge of teaching and research in vehicle safety at the Ostfalia University of Applied Sciences since 2011. Prior to joining the university he held various management positions in industry where he was in charge of development and testing of vehicle safety functions. His last management position was head of cab body development at MAN Truck & Bus AG. Prof. Bachem is chairman of the Wolfsburg Institute for Research, Development and Technology Transfer e. V.

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Ď	0912.02.2021	158/3792	Online	4 Days	790,- EUR till 12.01.2021, thereafter 940,- EUR	
	03.11.2021	158/3791	Alzenau	1 Day	790,- EUR till 06.10.2021, thereafter 940,- EUR	







International Safety and Crash-Test Regulations Current Status and Future Developments

Course Description

Since the 1960's, the regulation of vehicle safety performance has had a major impact on vehicle and system design. As automotive manufacturing has evolved into an integrated global system, understanding and anticipating legal requirements has become an immense challenge. Regulators collaborate and diverge in how they address road-safety policy goals. Regulatory changes in a single market can translate into global customer requirements. And these requirements are continuously evolving. In a compact program, this two-day seminar provides a worldwide update on the passive safety landscape, covering local, national, regional, and international policy and rulemaking developments.

The first segment of the seminar focuses on regulatory institutions and processes. By understanding the regulatory environment, including the trend towards an integrated global regulatory system, businesses can better prepare for changes that impact competitiveness and customer satisfaction.

The second segment applies this knowledge to current and future regulatory requirements. The seminar covers crashworthiness (frontal, side, rear impact, etc.) as well as pedestrian protection and new technologies.

Course Objectives

This course informs participants of recent developments and discussions within the global regulatory community concerning passive safety. The seminar explores differences in regulatory systems and philosophies, in compliance and enforcement, and in the forces behind the regulation of vehicle safety. The course provides participants with a broad understanding of current regulatory directions and guidance on how to follow, and even influence, future requirements.

Who should attend?

This seminar should be of interest to anyone involved with meeting and anticipating legal requirements for vehicle safety performance across international markets. The course provides a compact review of changes in passive safety requirements and current priorities across the international regulatory community. Moreover, the course provides knowledge critical to understanding differences in the way regulators establish and enforce these legal requirements.

Course Contents

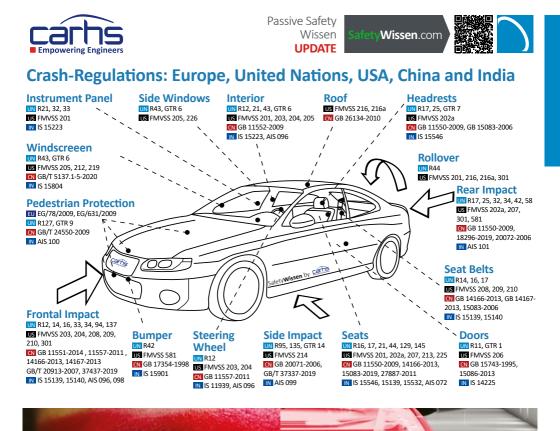
- History of safety regulation and development of legal regimes (e.g., self-certification, type approval, product liability, in-use surveillance)
- Regulatory agencies and rulemaking processes (e.g., UN, European Union, U.S. NHTSA, etc.)
- Regulatory drivers and priorities
- Types and purposes of regulations (UN Regulations, GTR, FMVSS, EU Regulations and Directives, etc.)
- Developments in crashworthiness and occupant protection requirements (frontal impact, side impact, pole-side impact, full width barrier, ODB, MPDB, etc.)
- Vulnerable road user (VRU) protection (e.g., pedestrian safety, cyclist safety)
- Safety of new propulsion technologies (electric vehicles, hydrogen fuel-cells, minimum vehicle noise levels)
- Passive safety implications of new safety technologies (e.g., emergency call systems, collision avoidance, VRU detection, automated driving)



John Creamer (GlobalAutoRegs.com) is the founder of GlobalAutoRegs.com and a partner in The Potomac Alliance, a Washington-based international regulatory affairs consultancy. In his client advisory role, Mr. Creamer is regularly involved with meetings of the UN World Forum for the Harmonization of Vehicle Regulations (WP.29). Previously, he has held positions with the US International Trade Commission and the Motor & Equipment Manufacturers Association (representing the US automotive supplier industry), as the representative of the US auto parts industry in Japan, and with TRW Inc. (a leading global automotive safety systems supplier).



Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	0910.02.2021	16/3802	Online	2 Days	790,- EUR till 12.01.2021, thereafter 940,- EUR	
	0105.03.2021	16/3739	Online	5 Days	790,- EUR till 01.02.2021, thereafter 940,- EUR	
	290608.072021	16/3738	Online	8 Days	1.340,- EUR till 01.06.2021, thereafter 1.590,- EUR	
	0809.11.2021	16/3803	Alzenau	2 Days	1.340,- EUR till 11.10.2021, thereafter 1.590,- EUR	







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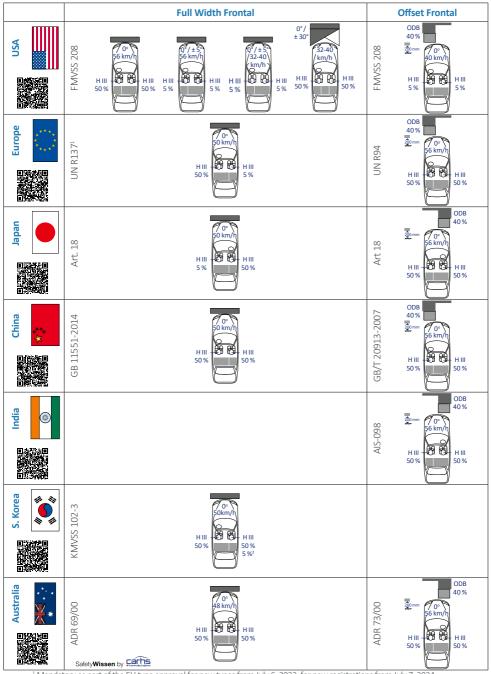




Passive SafetyWissenUPDATE



Rules and Regulations on Occupant Protection



¹ Mandatory as part of the EU type approval for new types from July 6, 2022, for new registrations from July 7, 2024.



UPDATE

afetyWissen.com



Ground clearance of the lower edge of the deformable barrier

	Side Barrier	Side Pole	Pedestrian	Rear	Head Impact	Rollover
FMVSS 214	SID IIS	5ID IIs/ ES-2 re Pole		FMVSS 202a FMVSS 301	FMVSS 201	Roof Crush: FMVSS 216a Ejection Mitigation: FMVSS 226
UN R95	50 mm ES-2 90° MDB EEVC, 950 kg	WS 50 % SET NO Pole WS 50 % ST ST ST ST ST ST ST ST ST ST	R (EC) 78/2009 ² R (EC) 631/2009 ² UN R127 R (EU) 2019/2144	UN R34	UN R21	
Art. 18	ES-2 50 km/h 50 km/h MDB EEVC, 950 kg	32 km/h 75* 81 12 4 254 mm Pole	Article 18	Article 22-4	Article 20	
GB 20071-2006	50 km/h 90° MDB EEVC, 950 kg	610C7-LEE 254 mm Pole	GB/T 24550-2009	GB 20072-2006	GB11552-2009	Roof Crush: GB26134-2010
AIS-099	ES-1/ ES-2 50 km/h 50 km/h MDB EEVC, 950 kg		AIS-100	AIS-101	IS15223	
KMVSS 102	ES-1/ Somm ES-2 50 km/h 90° MDB EEVC, 950 kg	7 WS 50 % 75° 254 mm Pole	KMVSS 102-2		KMVSS 88	
ADR 72/00	E5-2 50 mm 50 mm MDB EFVC, 950 kg	00/58 WO V So %			ADR 21	SafetyWissen by

¹ Mandatory as part of the EU type approval for new types from July 6, 2022, for new registrations from July 7, 2024.

² Expires on July 5, 2022







Crash Safety of Hybrid and Electric Vehicles

Course Description

During recent years, electric vehicles have achieved an ever-increasing importance for the automotive market. In addition, established OEM suffer increasing pressure by new competitors with innovative vehicle concepts. A compliance of restrictions for CO2 emissions in EU from 2020 on will not be possible without electrified power trains. All mayor OEM offer an increasing variety of hybrid vehicles (HEV), plug-in hybrid vehicles (PHEV) and pure electric vehicles (BEV). Also a first offer of fuel cell electric vehicles (FCEV) is in the market. Market acceptance and consumer demands exceed delivery capacity for some models. In 2019 more than 2 million electrified vehicles (BEV and PHEV) were sold worldwide. For 2020 more than 5 million are expected. The breakthrough of the automotive electrification is evident. For the development of future vehicle generations, the integration of electrified powertrains has not to be considered, it's the baseline.

Nevertheless, several challenges for vehicle safety arise with new these technologies. Electric shock risks on high-voltages systems, fire hazards in case of lithium-ion batteries and risks of rupture in case of gas tanks are the most important issues here. For every mode of drive, specific drive components and their particular safety requirements are described. In addition to common rules and standards, specific needs based on reallife accidents are being discussed.

For all relevant vehicle components the respective safety requirements, safety concepts and exemplary safety initiatives will be discussed. The state of the art concerning test standards, verification methods and possibilities for virtual safety will be shown. Future trends will be presented with the help of current research projects and results. Practical experience of rescuing, recovering and towing of electric vehicles complete the spectrum of accident safety.

Course Objectives

Participants will get an overview about automotive safety of electric vehicles and will learn the special challenges and solutions which come along. Participants will be able to apply test methods and safeguarding concepts and to pursue development strategies in a target-oriented way.

Who should attend?

The seminar addresses development and research engineers as well technicians in the fields of testing and engineering with electric vehicles. Due to its current relevance the course suits young professionals as well as experienced engineers who want to deepen their knowledge in this field.

Course Contents

- Overview alternative drive systems: hybrid, electric vehicles, fuel cell, gas vehicles
- Challenges for vehicle safety
- Legal requirements and standards, safety requirements for real-world accidents
- Safety of high voltage systems
- Battery safety
- Gas tank safety
- Fuel cell safety
- Structural safety
- Safety concepts
- Rescuing, recovering and towing of electric vehicles



Rainer Justen (Mercedes-Benz AG) has more than 30 years of experience in the field of vehicle safety. After his studies in mechanical engineering with a focus on automotive engineering he started his career in the automotive development at Daimler AG in 1987. Several career milestones in the fields of vehicle safety, project management, safety concepts and active safety / driver assistance systems made him an expert on all relevant topics of automotive safety. Since 2008 he is working in the field of safety for alternative drive systems. Rainer Justen is author of numerous publications and papers on this topic. In 2015 Rainer Justen received the SAE Automotive Safety Award for his work on the Safety of Li-Ion Batteries in Electric Vehicles from the American Society of Automotive Engineers (SAE).

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	2023.04.2021	173/3799	Online	4 Days	1.340,- EUR till 23.03.2021, thereafter 1.590,- EUR	
	2223.06.2021	173/3801	Alzenau	2 Days	1.340,- EUR till 25.05.2021, thereafter 1.590,- EUR	
	0910.11.2021	173/3800	Alzenau	2 Days	1.340,- EUR till 12.10.2021, thereafter 1.590,- EUR	



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- Launchers for Pedestrian Protection & Component test
- Crash Simulation Test Labs (Sleds)
- Seat Belt Anchorage Test systems
- Head Restraint Performance Test systems
- Roof Crush & Side Intrusion Test systems

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FMVSS 305: Safety Requirements for Electric Vehicles

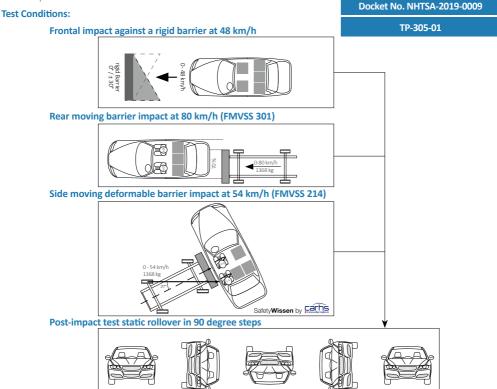
Scope:

Cars, busses, trucks with a GVWR of 4536 kg or less that use electrical components with working voltages higher than 60 volts direct current (VDC) or 30 volts alternating current (VAC), and whose speed attainable is more than 40 km/h.

Post-crash Requirements:

Under the test conditions described below (impact test and subsequent static rollover)

- max. 5 litres of electrolyte may spill from the batteries,
- there shall be no evidence of electrolyte leakage into the passenger compartments,
- all components of the electric energy storage / conversion system must be anchored to the vehicle,
- no battery system component that is located outside the passenger compartment shall enter the passenger compartment,
- each HV source in the vehicle must meet one of the 3 following electrical safety requirements
 - (1) electrical isolation must be greater than or equal to:
 - 500 ohms/V for an AC HV source,
 - 100 ohms/V for an AC HV source if it is conductively connected to a DC HV source, but only if the AC HV source meets the physical barrier protection requirements specified in the first 3 sub-items of (3)
 - 100 ohms/V for all DC HV sources,
 - (2) the**voltage level** $of the HV source (Vb, V1, V2) must be <math>\leq$ 30 VAC for AC components or 60 VDC for DC components.
 - (3) physical barrier protection against electric shock shall be demonstrated by meeting the following conditions:
 - the HV source meets protection degree IPXXB
 - resistance between exposed conductive parts of the electrical protection barrier (EPB) of the HV source and the electrical chassis is
 0.1 ohms
 - resistance between an exposed conductive part of the EPB of the HV source and any other simultaneously reachable exposed conductive parts of EPBs within 2.5 meters of it must be < 0.2 ohms
 - voltage between exposed conductive parts of the EPB of the HV source and the electrical chassis is ≤ 30 VAC or 60 VDC
 - voltage between an exposed conductive part of the EPB of the HV source and any other simultaneously reachable exposed conductive parts of EPBs within 2.5 meters of it must be ≤ 30 VAC or 60 VDC





UNECE: Safety Requirements for Electric Vehicles



Passive Safety

Wissen UPDATE

After crash tests according to UN R94 and R95 vehicles with a high voltage electrical powertrain (> 60 V DC or > 30 V AC) must meet the following requirements:

1. Protection against Electrical Shock

at least one of the four criteria specified below shall be met:

■ Absence of high voltage: The voltages $V_{b'}$, V_1 and V_2 shall be \leq 30 V AC or \leq 60 V DC : Electrical Chassis

Wissen.com

Low electrical energy:

The total energy (TE) on the high voltage buses shall < 2.0 J. Prior to the impact a switch S_1 and a known discharge resistor R_e is connected in parallel to the relevant capacitance . Not earlier than 5 s and not later than 60 s after impact S_1 shall be closed while the voltage V_b and the current I_e are recorded. From this TE is caluclated as follows:

$$TE = \int_{tc}^{th} V_{b} \times I_{e} dt$$

with tc = time of closing S_1 th = time when voltage drops below 60 V DC

Physical protection:

For protection against direct contact with high voltage live parts, the protection IPXXB shall be provided.

Isolation resistance:

- If the AC HV buses and the DC high voltage buses are galvanically isolated from each other, isolation resistance between the HV bus and the electrical chassis shall be \geq 100 Ω /V of the working voltage for DC buses, and \geq 500 Ω /V of the working voltage for AC buses.
- If the AC HV buses and the DC HV buses are galvanically connected isolation resistance between the HV bus and the electrical chassis shall be \geq 500 Ω /V of the working voltage. (if the protection IPXXB is satisfied for all AC HV buses or the AC voltage is \leq 30 V after the vehicle impact, the isolation resistance shall be R_i \geq 100 Ohm/V)

2. Electrolyte Spillage

In the period from the impact until 30 minutes after no electrolyte from the REESS (Rechargeable Electrical Energy Storage System) shall spill into the passenger compartment and no more than 7 % of electrolyte shall spill from the REESS.

3. REESS Retention

REESS located inside the passenger compartment shall remain in the location in which they are installed and REESS components shall remain inside REESS boundaries. No part of any REESS that is located outside the passenger compartment for electric safety assessment shall enter the passenger compartment during or after the impact test.

UN R100:

M and N class vehicles with a maximum speed > 25 km/h must also comply with UN R100 02 series.







Empowering Engineers

Vehicle Safety under Self-Certification Principles, Obligations, Enforcement and Remedies

Course Description

When looking at regulatory requirements across different markets, it's common to think in terms of technical specifications, checking for differences in test procedures and performance criteria. However, failure to consider how the regulations are used can be a fatal mistake because safety authorities differ in how they apply and enforce their requirements.

This seminar looks at the self-certification compliance and enforcement system which focuses heavily on monitoring the performance of vehicles in use. Compliance with the legal standards is only one part of a much larger, more complex system requiring the assurance of safety throughout the lifetime of every vehicle on the road. Manufacturers must have systems in place to detect possible safety concerns regardless of whether they relate to compliance with specific standards and must communicate continuously with safety authorities or run the risk of damaging recalls that can place the company in peril.

Course Objectives

This seminar provides a review of self-certification compliance and enforcement mechanisms toward helping manufacturers avoid expensive recalls, costly penalties, and lost reputation.

Who should attend?

The seminar is aimed at employees from the development departments of automobile manufacturers and suppliers who develop vehicles for the U.S. market as well as all employees in the areas of product strategy, sales and warranty and defect management for the U.S. market.

Course Contents

- Background and origins of self-certification
- Players and processes in U.S. rulemaking
- Principles of U.S. safety compliance and enforcement
- Role of product liability laws
- Role of Federal Motor Vehicle Safety Standards (FMVSS)
- NHTSA and FMVSS compliance
- NHTSA and safety monitoring
- Non-regulatory methods to ensure safety
- Safety defects and motor vehicle recalls
- Manufacturer roles and responsibilities
- Outlook for U.S. safety policies









John Creamer (GlobalAutoRegs.com) is the founder of GlobalAutoRegs.com and a partner in The Potomac Alliance, a Washington-based international regulatory affairs consultancy. In his client advisory role, Mr. Creamer is regularly involved with meetings of the UN World Forum for the Harmonization of Vehicle Regulations (WP.29). Previously, he has held positions with the US International Trade Commission and the Motor & Equipment Manufacturers Association (representing the US automotive supplier industry), as the representative of the US auto parts industry in Japan, and with TRW Inc. (a leading global automotive safety systems supplier).

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Ď	1923.04.2021	183/3741	Online	5 Days	790,- EUR till 22.03.2021, thereafter 940,- EUR	
	1213.10.2021	183/3740	Alzenau	2 Days	1.340,- EUR till 14.09.2021, thereafter 1.590,- EUR	



Active & Passive Safety Event

Euro NCAP UpDate 2021

Get ready for Euro NCAP's latest rating revision! \star



The Road Map 2025 systematically expands and updates all areas of the Euro NCAP rating. After a series of new and changed assessment procedures had already been implemented in 2020, many innovations are scheduled for 2023. At the Euro NCAP UpDate, experts from the respective working groups provide detailed information on the current status of these new procedures:

- Find out the current state of discussion on the upcoming protocols.
- Take advantage of the discussion with the experts active in the Euro NCAP working groups.

Contents

- Roadmap 2025
 - AEB/LSS Car-to-Powered Two Wheelers
 - New Car-to-Car AEB scenarios (Junction & Crossing, Head-on)
 - Automatic Emergency Steering AES
 - New test method for pedestrian and cyclist impact (new leg impactor aPLI and extended head impact zone)
 - Rescue, Extrication & Safety
 - Child Presence Detection
 - Driver Monitoring
 - Virtual Testing
 - Scenario based assessment
- Roadmap 2030

acts

- #TestingAutomation
 - Assessment of automated driving functions
- Field reports on the current test procedures

Who should attend?

The Euro NCAP UpDate is suited for everyone who wants to be prepared for Euro NCAP's upcoming requirements.









1.490,- EUR till 16.11.2021, thereafter 1.750,- EUR, ONLINE 990,- EUR



IIHS

Latin NCAP

ODB

40 %

нш 88 нш

50%

Frontal ODB

CRS - Installation

Side MDB

LATCH (Lower Anchors and

Tethers for Children)

Booster Seat Rating

200

1 0° 54 km

8 B Q3

50%

Q1.5

0 0 Get familiar with all NCAP tests in just 2 days with 56 km our seminar: NCAP - New Car Assessment Programs: нш 8 нш нш 89 89 нш R 5% 5% THOR 5% Tests, Assessment Methods, Ratings 89 нш нш 50 % 5% 5% learn more on ∋ page 30 MPDB 1400 kg OMDB, 2486 kg ODB SOB 25 % DF HO 0°, 50 % 40% 15°, 35 % 50 km/h 200 1**5**0 mn 0° 0 1 km $0 \, \text{km}$ 88 THOR THOR нш A THOR нш 8 нш 50 % Q6 50 % 50% 50 % 50 % Q10 81 😚 50% нш 5%

U.S. NCAP

Euro NCAP / ANCAP

Full Width

308 / SOB

	WS 50% AE-MDB, 1400 kg, 1400 k	SS km/h MDB, SID IIS 1368 kg	50 km/fi 50 km/fi 1500 kg 1900 kg SID IIs	BOMM ES-2 MDB EEVC 501km// 900' 900' 900' 900' 900' 900' 900' 90
	 WS 50 % Z54 mm Pole Far Side Occupant Protection 	32 km/h 75° 254 mm Pole		254 mm Pole
Pollower		SSF	■ Roof Crush	
Dodoctrian	 Flex PLI, aPLI Upper Legfom Headforms AEB/AES VRU Ped., Cyclist, PTW 	 Flex PLI Upper Legforn Headforms AEB Pedestrian Page 4: terretic Braking 	AEB Pedestrian	 Flex PLI Upper Legform Headforms AEB VRU

Child Safety Side MDB

AEB Reverse Pedestrian

Frontal MPDB

CRS - Installation

Rear Automatic Braking



Passive Safety

Wissen UPDATE afetyWissen.com



NCAP-Tests in Asia

Items written in italics are not part of the overall rating

2021 2022 **2023** 2024

	JNCAP	Items written in italics are	C-IASI	KNCAP	21 2022 2023 2024 ASEAN NCAP
Full Width	H III 5 % H III 5 %	H III 50 km/t H III 50 % H III 5 %		H III 5 %	
ODB / SOB	00B 40% 54 km/r 55% ■ MPDB	ODB 40% 0° 0°,50% 0° 44 km/h 0° 50 km/h 4 km/h 10° 50 km/h 50 km/h 50 km/h	SOB 25 % P150 mm Sol 28 km/t Sol 28 km/t H III Sol 28 km/t Sol 2	ODB 40 % # mm 64 km/r H III 50 % Q6 Car-to-Car	DDB 40 % 40 % 40 % 40 % 40 % 40 % 40 % 40 %
MDB	WS 20 mm 50 % # AF-MDB, F300 kg 55 km/h 5 km/h	WS SO % AF-MOB, SO km/t SO	SID IIS MDB IIHS SO km/7 SID IIS SID IIS	MS S0% AE-MDB, 1400 kg 00 km/h 90° 1400 kg 00 km/h 90° 1400 kg 00 km/h 1400 kg 00	E5-2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
Pole		WS 50 % 254 mm Pole EV/HEV only		32 km/h 75* 254 mm Pole	
Rollover		 Curtain Airbag 	Roof Crush	■ SSF	
Pedestrian	 Flex PLI Headforms <i>AEB Pedestrian</i> 	 Flex PL, aPLI Headforms AEB Pedestrian 	 Flex PLI Upper Legfom Headforms AEB Pedestrian AEB Cyclist 	 Flex PLJ, aPLJ Upper Legform Headforms AEB Pedestrian AEB Cyclist 	■ Flex PLI■ Headforms
Child Safety	CRS Rating	 Q3 in Full Width Frontal Q10 in MPDB CRS - Installation <i>CRS Rating</i> 		Frontal ODBSide MDB	 Frontal ODB Side MDB CRS - Installation Veh. Based Assmt. CPD
Whiplash	■ Dynamic (1 Pulse)	Dynamic (1 Pulse)Rear Seats Dynamic	 Static Dynamic (1 Pulse) 	 Static Dynamic (1 Pulse) Rear Seats Static 	
Other	SBR, AEB, LSS, Rear View, Headlights, eCall, Pedal Misapplication	 ESC, SBR, AEB, FCW, LDW, BSD, SLIF, SAS, LKA, eCall, V2X, Headlights 	 AEB, FCW, LSS, eCall, Headlights, Low Speed Bumper 	■ SBR, FCW, LDW, SLD, AEB, BSD, LKA, RCTA, ISA, Airbag, ESF	 BST, Rear View, AHB, HPT, Safety Assist Technologies
	page 64	page 60		page 67	⊃ page 59 29









NCAP - New Car Assessment Programs Tests, Assessment Methods, Ratings

Course Description

In 1979 the first New Car Assessment Program (NCAP) was established by NHTSA in the United States. The goal was to motivate competing car manufacturers to enhance the safety level of their cars beyond the minimum safety standards defined by regulations. The same approach has been followed globally by other organizations (e.g. by Euro NCAP, IIHS, ANCAP, JNCAP, KNCAP, C-NCAP, ...). Euro NCAP which has been established in 1997 has taken a leading role and has significantly influenced other countries and regions. The NCAP programs in many cases are highly dynamic, especially in comparison with rulemaking activities. In order to reach the goal to continuously improve the safety level of cars, the requirements need to be permanently adapted to the state of technology. Developers in the automotive industry need to know about upcoming changes at an early stage in order to be able to design or equip their vehicles accordingly.

In this seminar attendees get an overview of the organizations in charge of the NCAP programs and become familiar with the various test and assessment methods.

The seminar is conducted several times a year with changing focuses:

- Focus passive safety: Here the focus is on test and assessment methods for passive safety. Frontal and side impact, whiplash, child protection and pedestrian protection are discussed in detail. Tests for active safety are only mentioned in as far as they are relevant for the overall rating.
- Focus active safety: Here the focus is on active safety systems such as AEB or lane assistance. The tests and assessments for these systems are explained in detail. Tests for passive safety are only mentioned in as far as they are relevant for the overall rating.

In both focusses the current overall rating methods are described and explained. In addition to that an outlook is given on the roadmaps and future developments of the NCAP programs.

Who should attend?

The seminar addresses design, simulation, testing and project engineers as well as managers who want to get a current overview on the global range of NCAP programs with an outlook on upcoming topics and trends from an insider. Depending on the focus of their work attendees should chose the appropriate focus of the seminar.

Course Contents

- New Car Assessment Programs overview
- U.S. NCAP
- IIHS
- Euro NCAP
- ANCAP
- JNCAP
- KNCAP
- C-NCAP
- C-IASI
- Latin NCAP
- ASEAN NCAP
- Bharat NCAP
- Global NCAP



Direktor and Professor Andre Seeck (German Federal Highway Research Institute)

is head of the division "Vehicle Technology" with the German Federal Highway Research Institute (BASt). In this position he is responsible for the preparation of European Safety Regulations. Furthermore he represents the German Federal Ministry of Transport and Digital Infrastructure in the Board of Directors of Euro NCAP and he is the chairman of the strategy group on automated driving and of the rating system. These positions enable him to gain deep insight into current and future developments in vehicle safety. In 2017 NHTSA awarded him the U. S. Government Special Award of Appreciation.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
ă	1922.04.2021	164/3818	Online ¹	4 Days	790,- EUR till 22.03.2021, thereafter 940,- EUR	
	2324.06.2021	164/3819	Alzenau	2 Days	1.340,- EUR till 26.05.2021, thereafter 1.590,- EUR	
	2728.10.2021	164/3820	Alzenau	2 Days	1.340,- EUR till 29.09.2021, thereafter 1.590,- EUR	

¹ Online Seminar with reduced content



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Euro NCAP / ANCAP MPDB Frontal Impact

Assessment Procedure:

1. Calculation of **points for each measured criterion** (**○** p. 33) ①:

Where a value falls between the **higher** (2) and **lower** (3) **performance limit**, the score is calculated by linear interpolation. The maximum score is 4 points. Exceeding the **capping limit** (4) leads to loss of all points related to that tests.

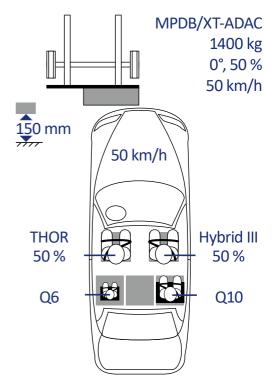
- Calculation of **points for each body region** (5): The lowest scoring criterion is used to determine the performance of each region. There are four body regions:
 - Head and neck
 - Chest and abdomen
 - Pelvis, femur and knee
 - Lower leg and foot
- 3. The **Modifiers** (6) are deducted from the body region score.
- Calculation of **point for the test**: For each body region the lowest score of driver (7)

or passenger ⑧ is used to determine the score. The maximum score for the test is 16 points.

- When a **door opens** in the test, a minus one-point modifier for each opening door will be applied to the score for that test.
- 6. The **Compatibility assessment** (**c** page 34) comprises:
 - Homgenity of barrier deformation (9)
 - Barrier bottoming out 10
 - Occupant Load Criterion OLC (1)

It is applied as a modifier (12) to the total test score. The dedcution is limited to 8 points. In 2020 and 2021 the deduction is halved and limited to 4 points.

 For the overall rating (
 → page 45) the score of the MPDB test is scaled by a factor of 0.5, i.e. a maximum of 8 points is available.



Empowering Engine

Protocols

Testing	MPDB Testing Protocol Version 1.1.1
Assessment	Assessment Protocol AOP Version 9.1.2
Dummy	Technical Bulletin 026 Version 1.2
Barrier	Technical Bulletin 022 Version 1.2
Compatibility	Technical Bulletin 027 Version 1.1.1





Passive Safety Wissen

UPDATE

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Euro NCAP / ANCAP: MPDB Frontal Impact

Assessment Protocol AOP Version 9.1.2

	5	1	2	3	(4)	6
Dummy	Region	Criteria	4 Points	0 Points	Capping	Modifiers
Frontal Impact against MPDB with 50 % Overlap @ 50/50 km/h						
Driver: THOR 50 % SBL-B (7)	Head ¹	HIC ₁₅	< 500	> 700	> 700	Unstable airbag/steering wheel contact (-1 pt) Hazardous airbag deployment (-1 pt) Incorrect airbag deployment (-1 pt) Steering column displ. (-1 pt)
		a _{3ms} (g)	< 72	> 80	> 80	
		SUFEHM/BrIC		Monitoring		
	Neck	My, extension (Nm)	< 42	> 57	> 57	
		Fz,tension (kN)	< 2.7	> 3.3	> 3.3	
		F _{x,shear} (kN)	< 1.9	> 3.1	> 3.1	
	Chest	Deflection R _{max} (mm)	< 35	> 60	> 60	A-pillar displacement (-2 pt) Compartment deformed (-1 pt) Steering wheel contact (-1 pt) Incorrect airbag deployment (-1 pt) Shoulder belt load > 6 kN (-2 pt)
	Abdo- men	Deflection (mm)	-	> 88	-	
	Pelvis	Acetabulum _{Com} - pression (kN)	< 3.28	> 4.1	-	Incorrect airbag deployment (-1 pt) Submarining ² (-4 pt) Variable contact (-1 pt) Concentrated loading (-1 pt)
	Femur	Axial Force (kN)	< 3.8	> 9.07 > 7.56 @ 10 ms	-	
	Knee	Displacement (mm)	< 6	> 15	-	
	Tibia	Tibia Index	< 0.4	> 1.3	-	Z–displacement of worst pedal (-1 pt) Footwell rupture (-1 pt) Pedal blocking (-1 pt)
		Axial Force (kN)	< 2	> 8	-	
	Foot	x–Displacement pedal (mm)	< 100	> 200	-	
Pas- senger: Hybrid III 50 % (8)	Head ¹	HIC ₁₅	< 500	> 700	> 700	Unstable airbag contact (-1 pt) Hazardous airbag deployment (-1 pt) Incorrect airbag deployment (-1 pt)
		a _{3ms} (g)	< 72	> 80	> 80	
	Neck	My, extension (Nm)	< 42	> 57	> 57	
		F _{z,tension} (kN)	< 2.7 @ 0 ms	> 3.3 @ 0 ms	> 3.3 @ 0 ms	
			< 2.3 @ 35 ms	> 2.9 @ 35 ms	> 2.9 @ 35 ms	
			< 1.1 @ 60 ms	> 1.1 @ 60 ms	> 1.1 @ 60 ms	
		F _{x,shear} (kN)	< 1.9 @ 0 ms < 1.2 @ 25-35 ms	> 3.1 @ 0 ms > 1.5 @ 25-35 ms	> 3.1 @ 0 ms > 1.5 @ 25-35 ms	
			< 1.1 @ 45 ms	> 1.1 @ 45 ms	> 1.1 @ 45 ms	
	Chest	Deflection (mm)	< 22	> 42	> 42	Incorrect airbag deploymt. (-1 pt) Shoulder belt load > 6 kN (-2 pt)
		VC (m/s)	< 0.5	> 1.0	> 1.0	
	Femur	Axial Force(kN)	< 3.8	> 9.07 > 7.56 @ 10 ms	-	Variable contact (-1 pt) Concentrated loading (-1 pt) Incorrect airbag deployment (-1 pt)
	Knee	Displacement (mm)	< 6	> 15	-	
	Tibia	Tibia Index	< 0.4	> 1.3	-	
		Axial Force(kN)	< 2	> 8	-	
For each door that opens during the test a -1 point modifier will be applied to the score of the test.						

For each door that opens during the test a -1 point modifier will be applied to the score of the test.

¹ If there is no hard contact (i.e. ares, peak < 80 g and no other evidence of hard contact) a score of 4 points is awarded.

² When any of the two iliac forces drops within 1 ms and when the submarining is confirmed on the high speed film.



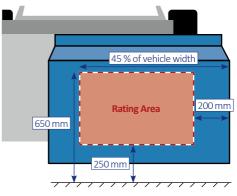


Technical Bulletin 027 Version 1.1.1

Euro NCAP / ANCAP: MPDB Frontal Impact Compatibility Assessment

Homogenity Assessment based on the Standard Deviation of the post-test Barrier Deformation within the Rating Area of the PDB Front Face (9)

- Scanning the deformed PDB front and generating a mesh with a maximum element size of 10 mm from the resulting point cloud.
- Creation of a point grid centered on the undeformed PDB front with uniform spacings of 20 mm (1400 grid points).
- Projection of the grid points on the mesh and calculation of the intrusion at each of the points in the rating area.
- Calculation of the standard deviation s [mm] of the intrusion (i.e. the deviation from the mean intrusion within which 68.2 % of the intrusion values fall).
- Calculation of the homogenity factor **h** [%]:
 - for s < 50 mm: h = 0
 - for 50 mm \le s \le 150 mm: h = (s 50 mm) / 100 mm
 - for s > 150 mm: h = 100 %



Bottoming out of the PDB (10)

A 2 point modifier **MBO** is applied if a barrier face penetration depth of 630 mm in an area that is larger than 40 mm x 40 mm occurs.

Calculation of the Occupant Load Criterion OLC (1)

 Determine velocity course of the MPDB by integrating the measured X-acceleration (a_X) on the centre of gravity of the MPDB (filtered with CFC 180):

$$v_{v}(t) = \int a_{x}(t) dt + v_{0}$$

with $v_0 =$ initial velocity of the MPDB.

OLC, t₁ and t₂ can be calculated with solving the following equation system:

$$\int_{t=0}^{t=t_1} v_0 \, dt - \int_{t=0}^{t=t_1} v_v(t) \, dt = 0.065$$

$$\int_{t=t_1}^{t=t_2} (v_0 - 0LC \cdot (t - t_1)) dt - \int_{t=t_1}^{t=t_2} v_v(t) dt = 0.235$$

$$v_0 - OLC \cdot (t_2 - t_1) = v_v(t_2)$$

with t_1 = end of the free-flight-phase of a virtual dummy on the barrier along a displacement of 65 mm

- t_2 = end of the restraining-phase of a virtual dummy on the barrier along a displacement of 235 mm after the free-flight-phase (i.e. a total displacement of 300 mm)
- For compatibility assessment OLC shall be converted from SI units into g.



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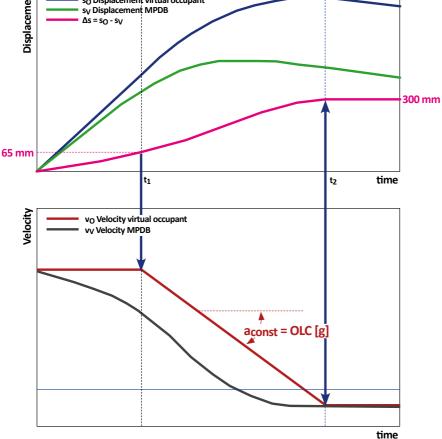
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Calculation of the Compatibility Modifier (12)

- for *OLC* < 25 g:
- Mcompat = -2·h MBO for $25 \text{ g} \le OLC \le 40 \text{ g}$:
- M_{Compat} = -2·OLC/15 + 10/3 h ·((4·OLC/10 8) (2·OLC/15 10/3)) M_{BO} Mcompat is limited to -8 points
- for *OLC* > 40 g: Mcompat = -2 - 6·h - MBO MCompat is limited to -8 points
- in 2020 2022 MCompat is multiplied with 0.5 (i.e. MCompat is limited to -4 points)
- MCompat is deducted from the total score (max. 16 points) of the MPDB frontal crash



Passive Safety Seminar





with Praxis Session

Euro NCAP MPDB Frontal Crash Workshop



In 2020 Euro NCAP introduced the MPDB (Moving Progressive Deformable Barrier) frontal crash. With this new crash test, Euro NCAP wants to assess not only the self-protection of vehicles, but also partner protection, i.e. compatibility.

The new test procedure poses a number of challenges: the test with 2 moving objects (vehicle + barrier car) is much more demanding than a test against the crash block. In addition there is the use of the new THOR dummy. Due to the new compatibility evaluation, the test evaluation also goes beyond the previous scope. For example, the energy input into the barrier and the deformation pattern must be evaluated.

The MPDB Workshop shows the new test procedure from test preparation (trolley, barrier and dummy seating). The workshop will be held at the ADAC Technical Centre in Landsberg, where the new test procedure was developed to a large extent, and will ensure the greatest possible practical relevance.

Course Objectives

Course participants will become familiar with the practical preparation, execution and evaluation of the MPDB crash. ADAC experts will answer questions about the new Euro NCAP test procedure.

Who should attend?

The workshop is aimed at all those who design vehicles for this load case or test vehicles to that effect.

Course Contents

- Overview of the MPDB Test
 - Roadmap / schedule
 - Development of the test and assessment procedure
 - Current status of the working group
 - Integration into the overall rating (scores, modifiers)
- Trolley and barrier
 - Specifications
 - Test preparation
- THOR dummy
- Dummy specifications (build level)
- Experiences from the round robin test
- Praxis: Seating procedure
- Injury criteria, limit values, modifiers
- Explanation of head injury assessment with SUFEHM
- Compatibility rating
 - Compatibility modifier components
 - Determining the OLC
 - Praxis: Evaluation of barrier deformation (barrier scan)





Volker Sandner (ADAC Technik Zentrum Landsberg) has been head of the Vehicle Safety Department of ADAC, which includes active safety, passive safety and accident research, since 2010. Before that, from 1999-2007 he was in charge of the construction of ADAC's crash test lab as a team manager. From 2007-2010 he lead the Passive Safety Department of ADAC. At Euro NCAP he is a member of the Board of Directors and chairman of the frontal impact working group. In addition to that he is member of the side impact working group, the technical working group and the ratings group of Euro NCAP. He is also lecturer for vehicle safety at the University of Applied Sciences in Munich.

Ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	1617.03.2021	182/3778	Landsberg am Lech	2 Days	1.340,- EUR till 16.02.2021, thereafter 1.590,- EUR	
	1617.11.2021	182/3779	Landsberg am Lech	2 Days	1.340,- EUR till 19.10.2021, thereafter 1.590,- EUR	



Passive Safety Seminar



Euro NCAP Knee Mapping Workshop

Course Description

Euro NCAP plays a leading role among the tests assessing the passive safety of vehicles in Europe. Its influence now also extends to other countries. Recently the knee impact test procedure within the Euro NCAP frontal impact test was modified, the goal being a less subjective assessment. A hard contact or a sharp edge in the knee area implies the danger for a car manufacturer to be punished with a so-called knee modifier (reduction in points). The knee modifier is the most frequent penalty within the Euro NCAP and impairs some vehicles' otherwise 5-star ratings. The allocation of a knee modifier often is a controversial decision. If a knee modifier has been allocated by the Euro NCAP inspector the car manufacturer has the possibility of proving - by means of a complex sled test procedure - that the modifier was not justified.

After a short introduction the main focus of the workshop is on the current Euro NCAP assessment procedure for frontal impact in the knee area (knee mapping). The current requirements will be explained in detail, in particular the knee modifiers 'Variable Contact' and 'Concentrated Loading', the areas of inspection and the threshold values. Positive / negative examples will facilitate the participants' understanding of the requirements and the assessment procedure. Participants will learn how to avoid a modifier. The sled test procedure will also be explained and discussed in detail.

In the afternoon a demo vehicle, which can be provided by participants, will be analyzed. Volker Sandner, a trained Euro NCAP inspector, can give valuable hints here.

A perspective regarding the future development of the test procedure will be given at the end of the seminar.

Who should attend?

The seminar addresses specialists from the field of crash, engineers and technicians from numerical simulation and testing, project engineers and managers who want to have a first-hand, up-to-date information and hints on how to avoid knee modifiers in Euro NCAP.

Course Contents

- Overview of Euro NCAP crash tests
- Euro NCAP requirements in the knee area
- Knee modifier, knee mapping test procedure
- Sled test procedure for knee impact
- Discussion of the assessment procedure and possibilities of interpretation
- Workshop with analysis of test vehicles, which can be provided by participants
- Future development of the test procedure

The workshop was very informative and relevant. The final analysis of a test vehicle was very helpful."

Ray Longbottom SAIC Motor UK Technical Centre Ltd., UK



Volker Sandner (ADAC Technik Zentrum Landsberg) has been head of the Vehicle Safety Department of ADAC, which includes active safety, passive safety and accident research, since 2010. Before that, from 1999-2007 he was in charge of the construction of ADAC's crash test lab as a team manager. From 2007-2010 he lead the Passive Safety Department of ADAC. At Euro NCAP he is a member of the Board of Directors and chairman of the frontal impact working group. In addition to that he is member of the side impact working group, the technical working group and the ratings group of Euro NCAP. He is also lecturer for vehicle safety at the University of Applied Sciences in Munich.

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
۵	14.09.2021	57/3780	Landsberg am Lech	1 Day	790,- EUR till 17.08.2021, thereafter 940,- EUR	



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Euro NCAP / ANCAP Protection Criteria in Frontal Impact

Dummy	Region	Criteria	4 Points	0 Points	Capping	Modifiers					
Fronta	Frontal-Impact against Rigid Wall with 100 % Overlap @ 50 km/h										
	Head ¹	HIC ₁₅	< 500	> 700	> 700	Unstable airbag/steering wheel contact (-1 pt)					
		a _{3ms} (g)	< 72	> 80	> 80	Hazardous airbag deployment (-1 pt)					
	Neck ²	My, extension (Nm)	< 36	>49	> 574	Incorrect airbag deployment (-1 pt)					
Hybrid III 5 %		Fz,tension (kN)	< 1.7	> 2.62	> 2.94	Steering column displacement (-1 pt)					
5 70		F _{x,shear} (kN)	< 1.2	> 1.95	> 2.74	Rear seat: head forward excursi- on (-4 pt)					
	Chast	Deflection (mm)	< 18	> 425	> 42 ⁵	Steering wheel contact (-1 pt)					
	Chest	VC (m/s)	< 0.5	> 1.0	> 1.0	Incorrect airbag deployment (-1 pt) Shoulder belt load > 6 kN (-2 pt)					
	Femur	Axial Force (kN)	< 2.6	> 6.2	-	Submarining ³ (-4 pt)					

¹ If there is no hard contact (i.e. a_{res, peak} < 80 g and no other evidence of hard contact) a score of 4 points is awarded. For the rear passenger in the rigid wall impact the score is based on a_{3ms} only, if there is no hard contact.

² For the rear passenger, the neck score is the sum of all three criteria, with the following maximum score per criterion: Shear 1 point, Tension 1 point, Extension 2 points

³ When any of the two iliac forces drops within 1 ms and when the submarining is confirmed on the high speed film.

⁴ Driver only

5 from 2023: 34 mm

Assessment Protocol Version 9.1.2

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Euro NCAP / ANCAP Protection Criteria in Side Impact

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Assessment Protocol Version 9.1.2

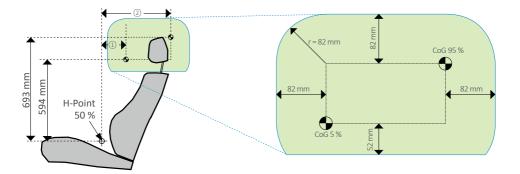
Dummy	Region	Criteria	4 Points	0 Points	Capping	Modifiers				
Barrie	Barrier Side Impact (AE-MDB) @ 60 km/h &									
Pole Side Impact @ 32 km/h										
	Lloadi	HIC ₁₅	< 500	> 700	> 700	incorrect airbag deployment				
	Head ¹	a _{3ms} (g)	< 72	> 80	> 80	(-1 point) door opening (-1 point/door)				
World SID 50 %	Chest	Deflection (mm)	< 28	> 50	> 50 (MDB) > 55 (Pole)	lateral shoulder force > 3.0 kN (deduction of all chest points) VC > 1.0 m/s (deduction of all				
	Abdo- men	Deflection (mm)	< 47	> 65	> 65	chest/abdomen points) head protection device assess-				
	Pelvis	Pubic Symphysis Peak Force (kN)	< 1.7	> 2.8	> 2.8	ment (-4 points)				

¹ Pole: no sliding scale, only capping if $HIC_{15} > 700$ or $a_{res, peak} > 80$ g or direct head contact with the pole.

Modifier Side Head Protection Device

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Inside the ,Head Protection Device Assessment Zone' (green) the head protection system's coverage is assessed. If the coverage is insufficient a 4 point modifier is applied the overall pole impact score. Areas outside the Daylight Opening (FMVSS 201) are excluded from assessment. Seams are not penalized if the un-inflated area is no wider than 15 mm. Any other un-inflated areas that are no larger than 50 mm in diameter (or equivalent area) are not penalized.



The head protection device (HPD) evaluation zone (green) is defined as a rounded rectangle around the head CoG box (defined by the head CoGs of the 5 % female and 95 % male occupants) at a distance of 82 mm from the upper and fore/aft edges and 52 mm below the bottom edge. The x-position of the CoG is defined relative to the H-Point of the 50 % male: Front seats:

(1) = H-Point(x) + 126 mm - seat travel (5th%ile- 50th%ile)

 $\overline{(2)}$ = H-Point(x) + 147 mm + seat travel (50th%ile-95th%ile)

Rear seats:

1 = H-Point(x) + 126 mm - remaining seat travel

2 = H-Point(x) + 147 mm + remaining seat travel



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Euro NCAP / ANCAP Far Side Occupant Protection in Side Impacts

Test Procedure

Test & Assessment Protocol Version 2.0.1

2 sled tests on acceleration based sled rig
 Pulses:

 Test 1: AX, SLED = AY, VEHICLE (AE-MDB @ 60 km/h) × 1.035
 Test 2: AX, SLED = AY, VEHICLE (Pole @ 32 km/h) × 1.035

 BIW mounted with centerline angled 75° towards direction of travel
 Spacers (EPP60) fitted in gaps between the struck side and the passenger seat and the passenger seat and center console
 WorldSID 50 % on driver seat

Assessment

- Prerequisites:
 - Structural stability of doors, hinges, roof rail and sill in MDB and pole crash. No opening of doors on struck side in MDB and pole crash.
 - Total score from MDB and pole crash \geq 10 points out of 12.
 - No failure of restraint systems for side impact protection in MDB and pole crash.
- Dummy Criteria:

Dummy	Region	Criteria	Max. Points	0 Points	Capping				
Far Sid	Far Side Occupant Protection Sled Test								
Head		HIC ₁₅ (with direct contact only)	< 500	> 700	> 700				
	пеай	a3ms (g)	< 72	> 80	> 80				
	Neck	Upper Neck Tension Fz (kN)	< 3.74	> 3.74	-				
		Upper Neck Lateral Flexion M_XOC (Nm)	< 162	> 248	-				
World		Upper Neck Extension neg. MyOC (Nm)	< 50	> 50	-				
SID 50 %		Lower Neck Tension F _z (kN)	< 3.74	> 3.74	-				
		Lower Neck Lateral Flexion $M_{X}\left(Nm\right)$	< 162	> 248	-				
		Lower Neck Extension neg. M_{y} (Nm) [*]	-	> [100]*	-				
	Chest & Abdomen	Chest Lateral Compression (mm)	< 28	> 50	> 50				
		Abdomen Lateral Compression (mm)	< 47	> 65	> 65				

* Monitoring for 2020 - 2022

 Max Points are depending on Peak Head Excursion and Far Side Countermeasures: The maximum available points for each body region depends on the amount of head excursion and the availability of a far side countermeasure.

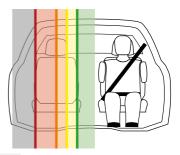
		Peak Head Excursion in Zone					
Region	Zone Countermeasure	Capping	Re ≤ 125 mm	d* > 125 mm	Orange	Yellow	Green
11	with	0	0	2	3	4	4
Head	without	0	0		1	2	4
Neck	with	0	4	4	3	4	4
NECK	without	0	:	1	1	2	4
Chest &	with	0	0	0	3	4	4
Abd.	without	0	()	1	2	4
Max Dum-	with	0	4	6	9	12	12
my Score	without	0	:	1	3	6	12

* score is depending on wether the red excursion line is > 125 mm outboard of the orange excursion line or not



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- Excursion Lines:
 - Red Line: Maximum post test intrusion of the interior door panel from AE-MDB (60 km/h) and 75° pole impacts respectively.
 - Orange Line: Seat centerline of the struck side seat
 - Yellow Line: 125 mm inboard from struck side seat centerline
 - Green Line: 250 mm inboard from struck side seat centerline
- Excursion Zones:
 - Capping Zone: Outboard from the Red Line
 - Red Zone: Between Red Line and Orange Line
 - Orange Zone: Between Orange Line and Yellow Line
 - Yellow Zone: Between Yellow Line and Green Line
 - Green Zone: Inboard from Green Line
 Pelvis and Lumbar Spine Modifiers



Empowering Engin

	Pefor-	
Criteria	mance	Modifier
	Limit	
PSPF (kN)	> 2.8	
Lumbar Fy (kN)	> 2.0	-4 Points applied to the dummy
Lumbar F _z (kN)	> 3.5	score for each test
Lumbar M _x (Nm)	> 120	

Total Score:

The total score (max. 12 from test 1 + 12 from test 2 = 24 points) will be scaled down to a maximum of **4 points** and is part of the AOP score.

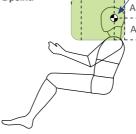
Occupant to Occupant Protection:

If the vehicle is equipped with a countermeasure, it must prove that the measure prevents occupant to occupant (O2O) interaction. This is verified in the full scale pole side impact (in 2020-2022 alternatively in the MDB impact). This test will be exectued with an additional WS 50 % dummy on the front passenger seat.

Criteria for O2O head protection:

- No exceedance of the head lower performance criteria
- No evidence of direct contact between the far side occupants head and any part of the nearside occupant (from 2023 onwards)
- For an assymetric countermeasure the OEM must provide evidence that it provides protection in impacts from both sides
- Protection must be offered in a protection zone:

If the countermeasure fails to meet these criteria, the total far side score (max. 4 points) will be **reduced by 1 point.**



B

R

-CoG marking from passenger in pole test position

A = 120 mm

B = 82 mm

C = Distance between driver (mid + 20 mm) and passenger (rearmost) head CoG locations





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Euro NCAP / ANCAP Rescue, Extrication & Safety Assessment





Rescue Sheet Naming Conventions 1.0 Rescue Sh	eet Checklist 1.0
Rescue Sheet Requirements	Penalty for not meeting the requirements
Rescue Sheet availability	-2
Rescue Sheet should be provided in PDF format as a unique document i.e. one file per model variant	
Rescue Sheet should be no more than four A4 sized pages	
Commercial licenses and/or exclusive publishing rights may not infringe on the rights of Euro NCAP and its members to make Rescue Sheets available at no cost to the general public	
Rescue Sheets must be supplied in at least the following languages: English, German, French and Spanish.	-1
From 2023: Rescue Sheets must be supplied in at least one of the official languages of each EU country + UK $$	
Rescue sheet must meet ISO 17840 Part 1 format and should include a summary following ISO 17840 Part 3 $$	
Rescue sheet content must be correct (checked in post-crash inspection)	

Extrication

Extrication Requirements	Penalty for not meeting the requirements
Automatic Door Locking (ADL): All side doors must be unlocked after frontal crash tests and non- struck side doors must be unlocked after side crash tests	
Post crash side door opening force < 750 N	
Post crash hinged side door opening angle \geq 45°	
Post crash sliding side door opening ≥ 500 mm	
Electric retracting door handles: After all full scale crash tests, the handles of all side doors must be in the extended/ready to open position or remain in retracted position but allow to be grabbed nevertheless by the first responder without any tool	-1
Seat belt buckle unlatching force \leq 60 N on seats occupied during frontal crashes	
Seat belt buckle unlatching force on seats occupied during side crashes is monitored in 2020 - 2022 and will be limited from 2023	
Max. total penalties from Rescue Sheet & Extrication	-2

Post Crash Technology

Prerequisite for scoring: no penalties for Rescue Sheet requirements

Post Crash Technology Requirements	Score for meeting the requirements
Advanced eCall system providing the likely number of occupants	0.5
Advanced eCall system providing the recent vehicle locations N1 and N2	0.5
 Multi Collision Brake (MCB) verified by destruction-free demonstration of braking caused by the MCB trigger signal documentation showing that the MCB trigger signal is sent during a crash test 	1
	0



2





UPDATE

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Euro NCAP / ANCAP Rating: 2020 - 2024

Overall Rating Protocol 9.0.1

<u>.</u>			<u></u>			Ŕ					
Adult Occupant Protection		Child Occupant Protection									
Adult Occupat	2020 -	2023 -	Child Occupar	2020 -	2023 -	VRU Protectio	2020 -	2023 -	Safety Assist		2023 -
	2020 - 2022	2023 - 2024		2020 - 2022	2023 - 2024		2020 - 2022	2023 - 2024		2020 - 2022	2023 - 2024
	max.	points		max.			max.	points		max.	points
MPDB Frontal Impact	8	8	Dyn. Tests Frontal	16	16	Head Impact	24	18	Occupant Sta- tus Monitoring	3	3
Full-width Frontal Impact	8	8	Dyn. Tests Side	8	8	Leg Impact	6	18	Speed Assis- tance Systems		3
Side impact (MDB)	6	6	CRS Installation	12	12	Upper Leg Impact	6	18	Lane Support Systems		3
Side Impact (Pole)	6	6	Vehicle Based Assessment	13	13	AEB VRU-Pe	9	9	AEB Car-to-Car	6	9
Side Impact (Far Side Oc- cupants MDB & Pole)	4	4				AEB VRU-Cy	9	9			
Whiplash Front Seats	3	3				AEB Junction Assist PTW		6			
Whiplash Rear Seats	1	1				LSS PTW		3			
Rescue	2	4									
max. points (1)	38	40	max. points (1)	49	49	max. points (1)	54	63	max. points (1)	16	18
normalised score (2)		points (1)	normalised score (2)		points (1)	normalised score (2)		points (1)	normalised score (2)		points (1)
weighting (3)	40)%	weighting (3)	20) %	weighting (3)	20)%	weighting (3)	20)%
weighted score (4)	(2)	x (3)	weighted score (4)	(2)	x (3)	weighted score (4)	(2)	x (3)	weighted score (4)	(2)	x (3)
		Bala	ncing: minimum n	ormalise	d score (2) by box for the r	respectiv	e star rat	ing ¹ :		
	80 %	80 %		80 %	80 %		60 %	70 %		70 %	70 %
	70 %	70 %		70 %	70 %		50 %	60 %		60 %	60 %
	60 %	60 %	+	60 %	60 %	+	40 %	50 %	+	50 %	50 %
	50 %	50 %	•	50 %	50 %	•	30 %	40 %	•	40 %	40 %
*	40 %	40 %		40 %	40 %		20 %	30 %		30 %	30 %
				O	verall sco	re (5) = ∑(4)					
		Th	e overall score is u	sed only	for rankii	ng the results withi	in vehicle	categori	es.		

Bold figures indicate changes with respect to the previous year

¹ A vehicle that meets all of the balance criteria for a 5-star overall rating cannot have any critical red body region (after modifiers are applied). In case of a red critical body region, the vehicle is limited to a maximum of 4-stars.

Dual Rating

VSSTR Protocol Version 7.4.2

Euro NCAP Logo Guidelines

Euro NCAP issues a base rating for standard equipment only. Fitment rates for safety assist technologies are no longer considered. Optionally manufacturers of cars that have achieved at least 3 stars can apply for a secondary rating of a model equipped with an optional safety package that meets a certain market installation rate (an average of 25 % in the first 3 years and of 55 % in the subsequent 3 years). The safety package must be actively promoted by the manufacturer. The safety package must be available, at least as an option, on all variants in the model range.

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U.S. NCAP: Tests and Criteria

Docket No. NHTSA-2006-26555

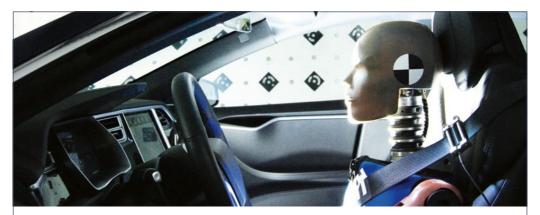
Hybrid III	Hybrid III 5% III 5% III	SID IIS SID IIS Rigid 254 mm Pole
Injury Criteria	Injury Ris	
	against Rigid Wall with 100 % Overlap @ 56 kr	
Dummy	Hybrid III 50 % (Driver)	Hybrid III 5 % (Passenger)
Head (HIC ₁₅)	$P_{head} (AIS3+) = \Phi \left(\frac{\ln(HIC15) - 7.45231}{0.73998} \right)$ where Φ = cumulative normal distribution	$P_{head} (AIS3+) = \Phi \left(\frac{\ln(HIC15) - 7.45231}{0.73998} \right)$ where Φ = cumulative normal distribution
Chest (Deflection in mm)	$P_{chest_defl}(AIS3+) = \frac{1}{1 + e^{10.5456 - 1.568^{\circ}(ChestDefl)^{0.4612}}}$	$P_{chest_defl}(AIS3+) = \frac{1}{1 + e^{10.5456 - 1.7212*(ChestDefl)^{0.4612}}}$
Femur (Force in kN)	$P(AIS \ 2+) = \frac{1}{1 + e^{5.795 - 0.5196 \ Femur} \ Force}$	$P(AIS 2+) = \frac{1}{1 + e^{5.7949 - 0.7619Femur_Force}}$
Neck (N _{ij} and Tension/ Compression in kN)	$P_{ncck_Nij}(AIS3+) = \frac{1}{1+e^{3.2269-1.9688.Nij}}$ $P_{ncck_Tens}(AIS3+) = \frac{1}{1+e^{10.9745-2.375.Ncck_Tension}}$ $P_{ncck_Comp}(AIS3+) = \frac{1}{1+e^{10.9745-2.375.Ncck_Compression}}$ $P_{ncck} = \max inuum(P_{ncck_Nij}, P_{ncck_Tens}, P_{ncck_Comp})$	$\begin{split} P_{neck_Nij}(AIS3+) &= \frac{1}{1+e^{3.2269-1.9688.Nij}} \\ P_{neck_Tens}(AIS3+) &= \frac{1}{1+e^{10.958-3.770Neck_Tension}} \\ P_{neck_Comp}(AIS3+) &= \frac{1}{1+e^{10.958-3.770Neck_Compression}} \\ P_{neck} &= \max imum(P_{neck_Nij}, P_{neck_Tens}, P_{neck_Comp}) \end{split}$
Overall	$P_{joint} = 1 - (1 - P_{head}) \times (1 - P_{r})$	$(1-P_{chest}) \times (1-P_{femur})$
Side Impact (M	DB & Pole Test)	
	ES-2re 50 %	SID-IIs 5 %
Head (HIC ₃₆)	$P_{head}(AIS3+) = \Phi\left(\frac{\ln(HIC36) - 7.45231}{0.73998}\right)$ where Φ = cumulative normal distribution	$P_{\text{head}} (\text{AIS 3+}) = \Phi \left(\frac{\ln(HIC36) - 7.45231}{0.73998} \right)$ where Φ = cumulative normal distribution
Chest (Rib Deflection in mm)	$P_{chest}(AIS3+) = \frac{1}{1 + e^{5.3895 - 0.0919 * \text{max. rib deflection}}}$	
Abdomen (Abdominal Force in N)	$P_{abdomen}(AIS3+) = \frac{1}{1 + e^{6.04044 - 0.002133*F}}$ where F = total abdominal force (N) in ES-2re	
Pelvis (Force in N)	$P_{pelvis}(AIS3+) = \frac{1}{1 + e^{7.5969 - 0.0011^*F}}$ where F is the public force in the ES-2re in Newtons	$p_{pelvis}(AIS2+) = \frac{1}{1+e^{6.3055-0.00094*F}}$ where F is the sum of acetabular and iliac force in the SID – IIs dummy in Newtons
Overall	$P_{joint} = 1 - (1-P_{head}) \times (1-P_{chest}) \times (1-P_{abdomen}) \times (1-P_{pelvis})$	$P_{joint} = 1 - (1-P_{head}) \times (1-P_{pelvis})$

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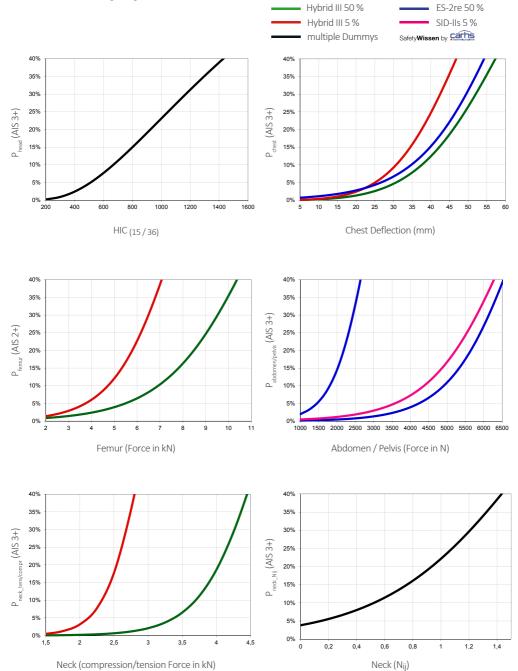
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U.S. NCAP: Injury Risk Curves





Passive Safety Wissen

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U.S. NCAP: Rating Scheme

Frontal C	rash Test	Side Pole Test Side MD		DB Test	Rollover Test			
Driver	Passenger	Front Seat	Front Seat	Rear Seat				
Injury Criteria	Injury Criteria	Injury Criteria	Injury Criteria	Injury Criteria				
Probabilty of In- jury (Risk Curves) P _{joint}	▼ Probabilty of In- jury (Risk Curves) P _{joint}	Probabilty of In- jury (Risk Curves) P _{joint}	▼ Probabilty of In- jury (Risk Curves) P _{joint}	Probabilty of In- jury (Risk Curves) P _{joint}	Probabilty of Rollover P _{roll}			
RR*=P _{joint} /base**	RR*=P _{joint} /base**	RR*=P _{joint} /base**	RR*=P _{joint} /base**	RR*=P _{joint} /base**	RR*=P _{roll} /base**			
Driver Stars (50 %)	▼ Passenger Stars (50 %)	Stars (20 %) Front Se (50	Stars (80 %) eat Stars %)	Rear Seat Stars (50 %)	• Overall Rollover Star Rating (3/12)			
	Overall Frontal Star Rating (5/12)Overall Side Star Rating (4/12)							
	Vehicle Safety Score (VSS)							

*RR = relative risk; **base = baseline risk = 15 %

Rating procedure

Using the Injury Risk Curves on \bigcirc page 46 and page 48, the risk of a serious injury (AIS 3+) can be calculated from the injury criteria measured in the crash test. The joint risk for an occupant can be determined using the following formulae:

$$\label{eq:Frontal Impact: P_joint} \text{Frontal Impact: P_joint} = 1 - (1 - \text{P}_{\text{head}}) \times (1 - \text{P}_{\text{neck}}) \times (1 - \text{P}_{\text{chest}}) \times (1 - \text{P}_{\text{femur}})$$

Side Impact: $P_{joint} = 1 - (1 - P_{head}) \times (1 - P_{chest}) \times (1 - P_{abdomen}) \times (1 - P_{pelvis})$

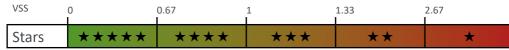
This risk is compared to a so called baseline risk which was set to 15 %. This ratio is called relative risk (RR) from which the star rating is determined using the following table:

RR	0	0.67	1	1.33	2.67
Stars	****	****	***	**	*

The rollover star rating is determined using the following table:

RR(roll)	0	0.67	1.33	2.0	2.67
Stars	****	****	***	**	*

The Vehicle Safety Score (VSS) is calculated as follows: $(5/12) \times RR(front) + (4/12) \times RR(side) + (3/12) \times RR(roll)$. The VSS star rating is determined using the following table:







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Testing Protocol Version XVIII (Jul 2017)

Rating Guidelines September 2014

				- Color	ng Guidennes Sep	ternser Lou-
Dummy	Region	Criteria	Good	Acceptable	Marginal	Poor
Front	al Impa	ct against ODB with 40	0 % Overlap	@ 64 km/h		
		HIC ₁₅	≤ 560	≤ 700	≤ 840	> 840
		N _{ij}	≤ 0.80	≤ 1.00	≤ 1.20	> 1.20
	Head & Neck	F _{z,tension} (kN)	≤ 2.6	≤ 3.3	≤ 4.0	> 4.0
		F _{z,compression} (kN)	≤ 3.2	≤ 4.0	≤ 4.8	> 4.8
		a _{res peak} (g)		Values > 70 resul	t in downgrading	
		a _{3ms} (g)	≤ 60	≤ 75	≤90	> 90
		Deflection (mm)	≤ 50	≤ 60	≤ 75	> 75
H III 50 %	Chest	Deflection rate (m/s)	≤ 6.6	≤ 8.2	≤ 9.8	> 9.8
		VC (m/s)	≤ 0.8	≤ 1.0	≤ 1.2	> 1.2
		Femur Axial Force (kN)	≤ 7.3 @ 0 ms	≤ 9.1 @ 0 ms	≤ 10.9 @ 0 ms	> 10.9 @ 0 ms
		(Force duration corridors)	≤ 6.1 @ 10 ms	≤ 7.6 @ 10 ms	≤ 9.1 @ 10 ms	> 9.1 @ 10 ms
	Legs &	Knee Displacement (mm)	≤12	≤ 15	≤ 18	> 18
	Feet	TI (upper, lower)	≤ 0.80	≤ 1.00	≤ 1.20	> 1.20
		Tibia Axial Force (kN)	≤ 4.0	≤ 6.0	≤ 8.0	> 8.0
		Foot acceleration (g)	≤ 150	≤ 200	≤ 260	> 260
				F	Protocol Version V	′l (Nov 2020)
Dummy	Region	Criteria	Good	Acceptable	Marginal	Poor
Seat/	Head R	estraints: Static Assess	sment (⊃ pa	age 108)		
HRMD	Head	Backset (mm)	≤ 70	≤ 90	≤110	> 110
ΠΝΙΝΙΟ	& Neck	Distance from top of head (mm)	≤ 60	≤ 80	≤ 100	> 100
Seat/	Head R	estraints: Dynamic Ass	sessment			
BioRID	Head	Vector sum of the standardized shear (FX) and tension (FZ) values $\label{eq:F_x} (F_x/315)^2 + \{(F_z-234)/1131\}^2$	< {0.450} ²	≤ {0.825}²	> {0.825}²	
llg	& Neck	Time to head restraint contact	for value	es > 70 ms the rational second s	ng is reduced by o	ne level*
		T1 acceleration (g)	for valu	ues > 9.5 the rating	g is reduced by on	e level*
				* only if both exce	ed the given level	

The overall rating equals the static or dynamic rating, whichever is worse.

Exceptions: If the static rating is "Acceptable" but the backset is sufficient for a "Good" rating and the dynamic rating is "Good" then the overall rating is also "Good". If the static rating is "Marginal" or "Poor" no dynamic test is made and the overall rating is "Poor".

Empowe		eers	Passive Sa Wis UPD	sen SafetyW	/issen.com			
IIHS F	Rating	R	ating Guidelines N	lov 2016 Testi	ing Protocol Versi	on X (Jul 2017)		
Dummy		Criteria	Good	Acceptable	Marginal	Poor		
Barrie	er Side	Impact (IIHS MDB) @	50 km/h					
		HIC ₁₅	≤ 623	≤ 779	≤ 935	> 935		
	Head/ Neck	F _{z,tension} (kN)	≤ 2.1	≤ 2.5	≤ 2.9	> 2.9		
		F _{z,compression} (kN)	≤ 2.5	≤ 3.0	≤ 3.5	> 3.5		
		Shoulder deflection (mm)		Values > 60 resul	t in downgrading			
		Ø Rib deflection (mm)	≤ 34	≤ 42	≤ 50	> 50		
	Chest/ Torso	Worst Rib deflection (mm)			51 - 55	> 55		
		Deflection rate (m/s)	≤ 8.20	≤ 9.84	≤ 11.48	> 11.48		
		VC (m/s)	≤ 1.00	≤ 1.20	≤ 1.40	> 1.40		
SID-IIs 5 %		Acetabulum force (kN)	≤ 4.0	≤ 4.8	≤ 5.6	> 5.6		
		Ilium force (kN)	≤ 4.0	≤ 4.8	≤ 5.6	> 5.6		
					Combined acetabulum and ilium force (kN)	≤ 5.1	≤ 6.1	≤7.1
	Pelvis/ Left	Femur A-P force (3 ms clip, kN)	≤ 2.8	≤ 3.4	≤ 3.9	> 3.9		
	Femur	Femur L-M force (3 ms clip, kN)	≤ 2.8	≤ 3.4	≤ 3.9	> 3.9		
		Femur A-P bending moment (3 ms clip, Nm)	≤ 254	≤ 305	≤356	> 356		
		Femur L-M bending moment (3 ms clip, Nm)	≤ 254	≤ 305	≤356	> 356		
Structure	2	Intrusion: B-pillar to driver seat centerline distance (mm)	≥ 125	≥ 50	≥0	< 0		
				Test	ing Protocol Versi	on III (July 2016)		
		Criteria	Good	Acceptable	Marginal	Poor		
Roof	Crush (⊃ page 75)						
Stiffness ratio (SW	to weight 'R)	F _{max} / m x g	≥ 4.00	≥ 3.25	≥ 2.50	< 2.5		

IIHS TOP SAFETY *PICK* **IIHS TOP SAFETY** *PICK*+

		TSP+ Criteria				
2021	 Crash tests: "Good" Crash tests: "Good" Front Crash Prevention & AEB Pedestrian: at Front Crash Prevention 	& AFR Pedestrian: at least				
2022	least "Advanced" ¹ "Advanced" ¹					
	- Hold clush revenuence AED redestrian at - I for clush revenuent					

¹ optional or standard

ratio (SWR)

² only available with acceptable- or good-rated headlights





IIHS Rating: Small Overlap

Testing Protocol Version VI (Jul 2017)

Rating Protocol Version V (Jul 2017)

Dummy	Region	Criteria	Good	Acceptable	Marginal	Poor
Front	al Impa	ict against Small Overla	ap Barrier w	vith 25 % Ov	erlap @ 64	km/h
	int	lower hinge pillar (resultant)				
	Jartme	footrest (resultant)				
0 (u	t Comp	left toepan (resultant)	≤ 150	≤ 225	≤ 300	> 300
ım) sno	Lower Occupant Compartment	brake pedal (resultant)				
ntrusio	ver Oc	parking brake pedal (resultant)				
Structure Rating: Intrusions (mm) O	Lov	rocker panel (lateral)	≤ 50	≤ 100	≤ 150	> 150
ture Ra	t t	steering column (longitutinal)	≤ 50	≤ 100	≤ 150	> 150
Struc	Upper Occupant Compartment	upper hinge pillar (resultant)				
	oper O Compa	upper dash (resultant)	≤ 75	≤ 125	≤ 175	> 175
	50	left instrument panel (resultant)				
		HIC ₁₅	≤ 560	≤ 700	≤ 840	> 840
	Head	N _{ij}	≤ 0.80	≤ 1.00	≤ 1.20	> 1.20
	& Neck 2	F _{z,tension} (kN)	≤ 2.6	≤ 3.3	≤ 4.0	> 4.0
		Fz,compression (kN)	≤ 3.2	≤ 4.0	≤ 4.8	> 4.8
		a _{3ms} (g)	≤ 60	≤ 75	≤ 90	> 90
	Chest/	Deflection (mm)	≤ 50	≤ 60	≤ 75	> 75
H III 50 %	Torso	Deflection rate (m/s)	≤ 6.6	≤ 8.2	≤ 9.8	> 9.8
		VC (m/s)	≤ 0.8	≤ 1.0	≤ 1.2	> 1.2
	Femur	KTH Injury Risk (%)	≤5	≤15	≤ 25	> 25
		Knee Displacement (mm)	≤ 12	≤ 15	≤ 18	> 18
	Leg & Foot	TI (upper, lower)	≤ 0.80	≤ 1.00	≤ 1.20	> 1.20
	9	Tibia Axial Force (kN)	≤ 4.0	≤ 6.0	≤ 8.0	> 8.0
		Foot Acceleration (g)	≤ 150	≤ 200	≤ 260	> 260

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IIHS Rating: Small Overlap

Frontal Impact against Sr	nall Overlap B	arrier with 25 S	% Overlap @ 6	64 km/h
Restraints & Dummy Kinematics Rati	ng			SafetyWissen by
Rating system based on a demerit syst	Demerits			
Frontal Head Protection				
Partial frontal airbag interaction				1
Minimal frontal airbag interaction				2
Excessive lateral steering wheel move	ment (> 100 mm)			1
Two or more head contacts with struc	ture			1
Late deployment or non deployment of	of frontal airbag			automatic Poor
Lateral Head Protection				
Side head protection airbag deployme	ent with limited forwa	rd coverage		1
No side head protection airbag deploy	rment			2
Excessive head lateral movement				1
Front Chest Protection				
Excessive vertical steering wheel move	ement (> 100 mm)			1
Excessive lateral steering wheel move	ment (> 150 mm)			1
Occupant containment and miscellar	neous			
Excessive occupant forward excursion	(> 250 mm)			1
Occupant burn risk				1
Seat instability				1
Seat attachment failure	automatic Poor			
Vehicle door opening				automatic Poor
Restraints & Kinematics O	Good	Acceptable	Marginal	Poor
Sum of Demerits	≤1	≤3	≤ 5	> 5

Small Overlap Overall Rating

Rating system based on a demerit system. Demerits result from the injury, structure and restraints & kinematics ratings.

Component Rating	Good	Acceptable	Marginal	Poor
Vehicle Structure Rating 0	0	2	6	10
Head/Neck Injury Rating 🛛	0	2	10	20
Chest Injury Rating	0	2	10	20
Thigh and Hip Injury Rating ④	0	2	6	10
Leg and Foot Injury Rating 🖲	0	1	2	4
Restraints / Kinematics Rating 6	0	2	6	10
The overall rating depends on the sum	of demerits:			SafetyWissen by
Overall Rating	Good	Acceptable	Marginal	Poor
Sum of demerits	≤ 3	≤ 9	≤ 19	> 19



UPDATE

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Latin NCAP Rating: 2020 - 2024

							MAS9	7
And Decement				Pedestrian and VRU		Safety Assist Systems		
Adult Occupant Protection		Child Occupant Protection		Pedestrian Protection		Safety Assist		
	2020 - 2024		2020 - 2024		2020 - 2024		2020 - 2022	2023 2024
	max. points		max. points		max. points		max. points	max. points
Offset Frontal Impact	16	Dyn. Tests Frontal	16	Head Impact	24	Seat Belt Reminder	10	10
Side Impact (MDB)	8	Dyn. Tests Side	8	Lower Leg Impact	6	Speed Assistance Systems	3	3
Side Impact (Pole)	8	CRS Installation	12	Upper Leg Impact	6	AEB Inter-Urban ²	9	9
Whiplash Front Seats	3	Vehicle Based	13	AEB VRU ²	12	ESC	15	15
AEB City ²	3					Lane Support Syst. (LDW, LKA, RED) ²	3	3
Rear End Impact UN R32	1					Blind Spot Detection ²	3	3
Rescue Sheet	1					eCall		(2) ³
max. points (1)	40	max. points (1)	49	max. points (1)	48	max. points (1)	43	43
normalised score (2)	actual points / (1)	normalised score (2)	actual points / (1)	normalised score (2)	actual points ¹ /(1)	normalised score (2)	actual points /(1)	actual points /(1)
	Bal	l <mark>ancing:</mark> minimum norr	malised s	core (2) by box for the	respectiv	ve star rating:		
	75 %		80 %		40 %		75 %	
	70 %		65 %		35 %		65 %	
	60 %	+	50 %	+	30 %	+	50 %	
	50 %	•	30 %		20%	•	40 %	
	40 %		15 %		10 %		10 %	
	80 %		80 %		50 %			80 %

¹ In 2020 and 2021 the total Pedestrian Protection score is calculated as follows: (Head score + Upper Leg score + Lower Leg score) x 1.15 + AEB score x 0.55

² System will be assessed if it is offered in all Latin NCAP markets as option and meets the following fitment rates:

70 %

55 %

40 %

20 %

40 %

30 %

25 %

10 %

System	2020	2021	2022	2023	2024
AEB City	10 %	10 %	10 %	30 %	30 %
AEB VRU	10 %	10 %	10 %	30 %	30 %
AEB Inter-Urban	10 %	10 %	10 %	30 %	30 %
BSD + LDW + LKA + RED combined	25 %	25 %	35%	45 %	55 %

Protocol Version 1.1.2

³ BONUS POINTS DO NOT INCREASE THE MAX. TOTAL POINTS

70 %

60 %

50 %

40 %

Bold figures indicate changes with respect to the previous year

70 %

60 %

50 %

50 %



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Passive Safety

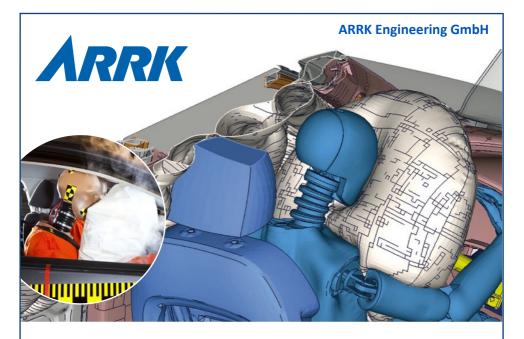
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Dummy	Region	Criteria	4 Points	0 Points	Capping	Modifiers						
Fronta	Frontal Impact against ODB with 40 % Overlap @ 64 km/h											
		HIC ₁₅	< 500	> 700	> 700							
		a _{3ms} (g)	< 72	> 80	> 80	Unstable airbag/steering wheel						
		My, extension (Nm)	< 42	> 57	> 57	contact (-1 pt) Hazardous airbag deployment						
			< 2.7 @ 0 ms	> 3.3 @ 0 ms	> 3.3 @ 0 ms	(-1 pt)						
	Head ^{1,2}	F _{z,tension} (kN)	< 2.3 @ 35 ms	> 2.9 @ 35 ms	> 2.9 @ 35 ms	Incorrect airbag deployment						
	Neck		< 1.1 @ 60 ms	> 1.1 @ 60 ms	> 1.1 @ 60 ms	(-1 pt)						
			< 1.9 @ 0 ms	> 3.1 @ 0 ms	> 3.1 @ 0 ms	Steering column displacement						
		F _{x,shear} (kN)	< 1.2 @ 25-35	> 1.5 @ 25-35	> 1.5 @ 25-35	(-1 pt) Passenger head contact w/						
		x,snear (NN)	ms	ms	ms	dashboard (-1 pt)						
			< 1.1 @ 45 ms	> 1.1 @ 45 ms	> 1.1 @ 45 ms	,						
Hybrid III 50 %	Chest	Deflection (mm)	< 22	> 42	> 42	A-pillar displacement (-2 pt) Compartment integrity (-1 pt) Steering wheel contact (-1 pt)						
	Chest	VC (m/s)	< 0.5	> 1.0	> 1.0	Incorrect airbag deployment (-1 pt) Shoulder belt load > 6 kN (-2 pt)						
				> 9.07	-							
	Femur			Femur Knee	Axial Force (kN)	< 3.8	> 7.56 @ 10 ms	-	Variable contact (-1 pt) Concentrated loading (-1 pt) Incorrect airbag deployment			
	KIEE	Displacement (mm)	< 6	>15	-	(-1 pt)						
		Tibia Index	< 0.4	> 1.3	-	Z–displacement of worst pedal						
	Tibia	Axial Force (kN)	< 2	>8	-	(-1 pt)						
	Foot	x–Displacement pedal (mm)	< 100	> 200	-	Footwell rupture (-1 pt) Pedal blocking (-1 pt)						
door opening (-1 pt/door) fuel leakage (-1 pt)												

¹ If there is no hard head contact (i.e. $a_{res, peak} < 80$ g and no other evidence of hard contact) a score of 4 points is awarded. ² If no steering wheel airbag is fitted and HIC15 < 700 and $a_{3ms} < 80$ g, 2 headform tests according to UN R12 are carried out (hub/ spoke junction and rim spoke junction). Assessment is based on the following criteria:

Dummy	Region	Criteria	2 Points	0 Points	Capping
UN R12	UN R12 6.8 kg Head headform	HIC ₁₅			> 700
6.8 kg		a _{3ms} (g)	< 65	> 80	> 80
headform		ares, peak (g)	< 80	> 120	> 120



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Dummy	Region	Criteria	4 Points	0 Points	Capping	Modifiers				
Barrie	Barrier Side Impact @ 50 km/h &									
Pole Side Impact @ 29 km/h										
	Head ¹	HIC ₁₅	< 500	> 700	> 700					
	neau-	a _{3ms} (g)	< 72	> 88	> 88	incorrect airbag deployment (-1 pt)				
ES-2 Chest Abdo- men Pelvis	Charat	Deflection (mm)	< 22	> 42	> 42	backplate loading Fy 1.0 4.0 kN (02 pt)				
	Cnest	VC (m/s)	< 0.32	> 1.0	> 1.0	T12 F _y 1.5 2 kN / M _x 150 200 Nm (02pt)				
		Force _{compression} (kn)	< 1.0	> 2.5	> 2.5	head protection device assess- ment (-2 pt front, -2 pt rear ²)				
	Pelvis	Pubic Symphysis Peak Force (kN)	< 3.0	> 6.0	> 6.0	_				
door opening (-1 pt/door) fuel leakage (-1 pt)										

Passive Safety

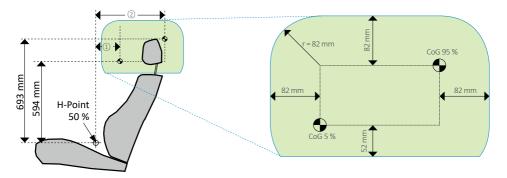
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¹ Pole: no sliding scale, only capping if HIC15 > 700 or ares, peak > 80 g or direct head contact with the pole.

² From 2022: - 4 pt rear

Modifier Side Head Protection Device

Inside the ,Head Protection Device Assessment Zone' (green) the head protection system's coverage is assessed for both front and rear seats. If the coverage is insufficient a -2 point modifier is applied to the overall AOP score. Areas outside the Daylight Opening (FMVSS 201) are excluded from assessment. Seams are not penalized if the un-inflated area is no wider than 15 mm. Any other un-inflated areas that are no larger than 50 mm in diameter (or equivalent area) are not penalized.



The head protection device (HPD) evaluation zone (green) is defined as a rounded rectangle around the head CoG box (defined by the head CoGs of the 5 % female and 95 % male occupants) at a distance of 82 mm from the upper and fore/aft edges and 52 mm below the bottom edge. The x-position of the CoG is defined relative to the H-Point of the 50 % male: Front seats:

(1) = H-Point(x) + 126 mm - seat travel (5th%ile- 50th%ile)

(2) = H-Point(x) + 147 mm + seat travel (50th%ile-95th%ile)

Rear seats:

(1) = H-Point(x) + 126 mm - remaining seat travel

(2) = H-Point(x) + 147 mm + remaining seat travel

car	NS
Empowering	Engineers

ASEAN NCAP

Overall Rating 2021 - 2025



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UPDATE





Overall Assessment Protocol Version 2.1

	Adult Occupant Protection			ccupant ection	Safety	Assist	Motorcyc	list Safety	
	Offset Frontal I	mpact 16	Frontal Impact	16	Seat Belt Remi	nder 6	Blind Spot (BST	Г) 8	
	Side Impact (M	IDB) 8	Side Impact		ABS / ESC		Rear View (ARV	√) 4	
	HPT	8	CRS Installation	n 12	AEB		Auto High Bear	m (AHB) 2	
			Vehicle-based	Assmt. 13	Advanced SATs		Pedestrian Pro	tection 2	
			CPD	2			Advanced MST	(2)1	
max. points (1)		32		51		21		16	
normalized score (2)	actual po	oints / (1)	actual points / (1)		actual points / (1)		actual points / (1)		Overall
weighting (3)	40	%	20)%	20) %	20 %		score (5)
weighted score (4)	(2) >	(3)	(2)	(2) x (3)		x (3)	(2) x (3)		∑(4)
Rating	Ba	alancing: minir	num normaliz	ed score (2) p	er box require	d for the respe	ective star ratir	ng:	
	score	points	score	points	score	points	score	points	
****	80 %	25.60	75 %	38.25	70 %	14.70	50 %	8.00	
****	70 %	22.40	60 %	30.60	50 %	10.50	40 %	6.40	
***	60 %	19.20	30 %	15.30	40 %	8.40	30 %	4.80	
**	50 %	16.00	25 %	12.75	30 %	6.30	20 %	3.20	
*	40 %	12.80	15 %	7.65	20 %	4.20	10 %	1.60	

¹ Bonus points do not increase the max. total points

Adult Occupant Protection

AOP Assessment Protocol Version 2.0

Dummy	Region	Points	Criteria	
Fronta	l Impact ag	ainst C	DB with 40 % Overlap @ 64 km/h	
Head, Ne	Hood Nock	4	HlC ₁₅ < 500; a _{3ms} < 72 g M _{y,extension} < 42 Nm F _{z,tension} < 2.7 kN @ 0 ms / < 2.3 kN @ 35 ms / < 1.1 kN @ 60 ms F _{x,shear} < 1.9 kN @ 0 ms / < 1.2 kN @ 25 – 35 ms / < 1.1 kN @ 45 ms	
	nedu, Netk	0	HlC15 > 700; a3 _{ms} > 80 g M _{y,extension} > 57 Nm F _{z,tension} > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms F _{x,shear} > 3.1 kN @ 0 ms / > 1.5 kN @ 25 – 35 ms / > 1.1 kN @ 45 ms	16 points
H III 50 %	Chest	4	Deflection < 22 mm; VC < 0.5 m/s	6 pc
front	Chest	0	Deflection > 42 mm; VC > 1.0 m/s	×. 1
	Femur,	4	Axial Force _{compression} < 3.8 kN Knee Displacement < 6 mm	тах.
	Knee	0	Axial Force _{compression} > 9.07 kN @ 0 ms / > 7.56 @ 10 ms Knee Displacement > 15 mm	
	Tibia	4	TI < 0.4; Axial Force _{compression} < 2 kN Pedal rearward displacement < 100 mm	
Foot	Foot	0	TI > 1.3; Axial Force _{compression} > 8 kN Pedal rearward displacement > 200 mm	

Barrier Side Impact (MDB) @ 50 km/h

Lined	Head	4	HIC ₃₆ < 650; a _{3ms} < 72 g	
	пеац	0	HIC ₃₆ > 1000; a _{3ms} > 88 g	~~~
Chest ES-2	Chast	4	Deflection < 22 mm; VC < 0.32 m/s	points ²
	Chest	0	Deflection > 42 mm; VC > 1.0 m/s	
E3-2	Abdomen	4	Force _{compression} < 1.0 kN	. 16
Pelvis	Abuomen	0	Force _{compression} > 2.5 kN	пах.
	Dolvic	4	PSPF < 3.0 kN	⊆
	0	PSPF > 6.0 kN		

² scaled down to 8 points in the overall rating





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Management Regulation 2021 (valid from 1/2022)

C-NCAP

Dummy	Region	Points	Criteria	
Fronta	l Impact wi	ith 100	% Overlap @ 50 km/h	
		5	$HIC_{15} \le 500; a_{3ms} \le 72 g$	
	Head	0	HIC ₁₅ ≥ 700; a _{3ms} ≥ 80 g	
	Neels	2	$M_{y,extension} ≤ 42 Nm$ $F_{z,tension} ≤ 2.7 kN @ 0 ms / ≤ 2.3 kN @ 35 ms / ≤ 1.1 kN @ 60 ms$ $F_{x,shear} ≤ 1.9 kN @ 0 ms / ≤ 1.2 kN @ 25 – 35 ms / ≤ 1.1 kN @ 45 ms$	
H III 50 %	Neck	0	$M_{y,extension} \ge 57 \text{ Nm}$ F _{z,tension} ≥ 3.3 kN @ 0 ms / ≥ 2.9 kN @ 35 ms / ≥ 1.1 kN @ 60 ms F _{x,shear} ≥ 3.1 kN @ 0 ms / ≥ 1.5 kN @ 25 – 35 ms / ≥ 1.1 kN @ 45 ms	
front	Chest	5	Deflection \leq 22 mm; VC \leq 0.5 m/s	S
	Chest	0	Deflection \geq 50 mm; VC \geq 1.0 m/s	oint
	Femur	2	Axial Force _{compression} ≤ 3.8 kN; Knee Displacement ≤ 6 mm	0 b(
	Knee	0	Axial Force _{compression} \geq 9.07 kN @ 0 ms / \geq 7.56 @ 10 ms; Knee Displacement \geq 15 mm	max. 20 points
		2	TI ≤ 0.4; Axial Force _{compression} ≤ 2 kN	
	Tibia	0	TI ≥ 1.3; Axial Force _{compression} ≥ 8 kN	
		1.6	HIC ₁₅ \leq 500; a _{3ms} \leq 72 g	
	Head	0	$HIC_{15} \ge 700; a_{3ms} \ge 80 g$	
H III 5 %		0.4	$F_{x,shear} \le 1200 \text{ N}; F_{z,tension} \le 1700 \text{ N}; M_{y,extension} \le 36 \text{ Nm}$	
rear	Neck	0	$F_{x,shear} \ge 1950 \text{ N}; F_{z,tension} \ge 2620 \text{ N}; M_{v,extension} \ge 49 \text{ Nm}$	
	Chest	2	Deflection \leq 18 mm; VC \leq 0.5 m/s	
		0	Deflection \ge 42 mm; VC \ge 1.0 m/s	
Fronta	l Imnact ag	ainst N	1PDB with 50 % Overlap @ 50/50 km/h	
TTOTIC			$HIC_{15} \leq 500$; $a_{3ms} \leq 72$ g	
		4	$M_{v,extension} \le 42$ Nm; $F_{z,tension} \le 2.7$ kN; $F_{x,shear} \le 1.9$ kN	
	Head, Neck		$HIC_{15} \ge 700; a_{3ms} \ge 80 g$	
		0	$M_{y,extension} \ge 57 \text{ Nm}; F_{z,tension} \ge 3.3 \text{ kN}; F_{x,shear} \ge 3.1 \text{ kN}$	
THOR	Chest, Abdo-	4	Chest Deflection ≤ 35 mm	
50 %	men	0	Chest Deflection ≥ 60 mm; Abdomen Deflection ≥ 88 mm	
front driver	Pelvis, Femur	4	Acetabulum _{Compression} \leq 3.28 kN; Femur Axial Force _{compression} \leq 3.8 kN; Knee Displacement \leq 6 mm	
	Knee	0	Acetabulum _{Compression} \ge 4.1; kN; Femur Axial Force _{compression} \ge 9.07 kN @ 0 ms / \ge 7.56 @ 10 ms; Knee Displacement \ge 15 mm	max. 20 points ¹
		4	TI \leq 0.4; Axial Force _{compression} \leq 2 kN	20
	Tibia	0	TI \geq 1.3; Axial Force _{compression} \geq 8 kN	lax.
		4 front	$HIC_{15} \le 500; a_{3ms} \le 72 g$	2
	Hood Nock	/ 2 rear	$M_{y,extension} \le 36 \text{ Nm}; F_{z,tension} \le 1.7 \text{ kN}; F_{x,shear} \le 1.2 \text{ kN}$	
H III 5 % front/	Head, Neck	0	$HIC_{15} \ge 700; a_{3ms} \ge 80 g$ My, extension ≥ 49 Nm; Fz, tension ≥ 2.62 kN; Fx, shear ≥ 1.95 kN	
rear		4/2	Deflection ≤ 18 mm; VC ≤ 0.5 m/s	
passen-	Chest	0	Deflection ≥ 42 mm; VC ≥ 1.0 m/s	
ger		4/-	Axial Force _{compression} \leq 2.6 kN	
	Femur	0	Axial Force _{compression} \geq 6.2 kN	
1.10	C 11 0 C 1			

¹ 16 points for driver & front passenger (worst body region of either driver or passenger counts), 4 points for rear passenger 60

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Management Regulation 2021 (valid from 1/2022)

C-NCAP

Dummy	Region	Points	Criteria	
Front	al Impact ag	ainst N	1PDB with 50 % Overlap @ 50/50 km/h	
	lload	2	$HIC_{15} \le 500; a_{3ms} \le 60 g$	
	Head,	0	$HIC_{15} \ge 700; a_{3ms} \ge 80 g$	ints
Q10	Neck	1	$F_{z,tension} \leq 1555 N$	4 points
rear	NECK	0	$F_{z,tension} \ge 2840 \text{ N}$	max. 4
	Chest	1	a _{3ms} ≤ 41 g	Ĕ
	chest	0	a _{3ms} ≥ 55 g	
Compat	ibility Assessmen	t (see page	e 34 for more details)	in
Homoge	enity	02(-1) ¹	Standard deviation of barrier deformation: 50 mm 150 mm	(-3) ¹ points
Bottomi	ng out	-2(-1) ¹	Barrier penetration \geq 630 mm in an area of \geq 40 x 60 mm) ¹ pc
High intrusion		-1	For vehicles with longitudinal member above 508 mm: Intrusion of 6 consecu- tive 20 x 20 mm cells above the 650 mm upper boundary of the rating area ≥ 480 mm	max6 (-3
Occupai	nt Load Criterion	02(-1) ¹	OLC 2540 g	~
¹ In Phase	1-2022			

Barrier Side Impact (AE-MDB) @ 50 km/h (traditional energy vehicles only) Pole Side Impact @ 32 km/h (new energy vehicles only)

	Head	4	$HIC_{15} \le 500; a_{3ms} \le 72 g$	
	пеац	0	HIC ₁₅ ≥ 700; a _{3ms} ≥ 80g	
WS 50	Chest	4	Deflection ≤ 28 mm	(Pole)
front	Chest	0	Deflection \ge 50 mm; VC \ge 1.0 m/s; Shoulder Lateral Force \ge 3.0 kN	(Pe
none	Abdomen	4	Deflection ≤ 47 mm	points
	Abuomen	0	Deflection \ge 65 mm; VC \ge 1.0 m/s	bo
	Pelvis	4	$PSPF \leq 1.7 \text{ kN}$	/ 16
	PEIVIS	0	$PSPF \ge 2.8 \text{ kN}$	B) /
	Head	1	HIC ₁₅ ≤ 500	points (MDB)
		0	HIC ₁₅ ≥ 700	ts (
SID-IIs	Chest	1	Deflection ≤ 31 mm	oin
rear	Chest	0	Deflection \geq 41 mm; VC \geq 1.0 m/s	20 p
(MDB	Abdomen	1	Deflection ≤ 38 mm	
only)	Abdomen	0	Deflection \geq 48 mm; VC \geq 1.0 m/s	тах.
	Pelvis	1	Force ≤ 3500 N	
	1 61013	0	Force ≥ 5500 N	

Dummy Region

Points

Criteria

Whiplash Test @ ∆v = 20 km/h

		Front	Rear		
	NIC	2	0.8	$\leq 8 \text{ m}^2/\text{s}^2$	
	NIC	0	0	\geq 30 m ² /s ²	points
BioRID II Upper Neck	Upper Neck	1.5	0.6	$F_{x+} \le 340 \text{ N}; F_{z+} \le 475 \text{ N}; M_y \le 12 \text{ Nm}$	
DIORID II	Opper Neck	0	0	$F_{x+} \ge 730 \text{ N}; F_{z+} \ge 1130 \text{ N}; M_y \ge 40 \text{ Nm}$	/2
	Lower Neck	1.5	0.6	$F_{x+} \le 340 \text{ N}; F_{z+} \le 257 \text{ N}; M_y \le 12 \text{ Nm}$	points
	Lower Neck	0	0	$F_{x+} \ge 730 \text{ N}; F_{z+} \ge 1480 \text{ N}; M_y \ge 40 \text{ Nm}$	poi
Max. dyn	. seatback defl.	-2	-0.8	≥ 25.5°	.5
Dyn. seat displacement		-5	-2	≥ 20 mm	тах.
HRMD interference		-2	-0.8	Y/N	



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Static Child Protection Assessment						
	0.5	Applicabilty of belt mounted child restraints				
Vehicle based	0.5	Applicabilty of ISOFIX mounted child restraints	points			
assessment	0.5	Applicabilty of large child restraints				
	0.5	Communication function				
CRS Installation	0.5	Belt mounted child restraints	ma			
	0.5	ISOFIX mounted child restraints				
	0.5 0.5	Communication function Belt mounted child restraints	тах. 3 р			

Seat Belt Reminder					
SBR passenger	-1	no SBR with occupant detection available	-2		
SBR 2 nd row	-1	no SBR available	ax.		
	-0.5	only SBR without occupant detection available	E		

Bonus items			
Ejection Mitigation	2	Curtain meets FMVSS 226 or maintains 50 % of working pressure for 6 s	2
	1	manual emergency call function	ax.
E-Call	1	automatic emergency call function	3

Occupant Protection		Pedestrian Pro	otection	Active Safety		
	max. points		max. points		max. points	
MPDB Frontal Impact	24	Head Impact	10	ESC	8	
Full-width Frontal Impact	24	Leg Impact	5	AEB Car-to-Car	11	
Side Impact (MDB/ Pole)	24 ¹			AEB Car-to-Pedestrian	10	
Child Safety Static	3			AEB Car-to-Two-wheeler	11	
Whiplash Front/Rear	7			LKA	3	
Ejection Mitigation	2			HMI	6	
E-Call	2			BSD Car-to-Car ²	2	
				BSD Car-to-Two-wheeler ²	3	
				SAS ²	2	
				LDW ²	2	
				max. points ADAS (2)	56	
				Headlights Low Beam	6	
				Headlights High Beam	3	
				Headlights Bonus	1	
max. points (1)	86	max. points (1)	15	max. pts. Headlights (3)	10	_
normalised score (4)	actual points / (1)	normalised score (4)	actual points / (1)	normalised score (4)	80% x act. pts. ADAS / (2) + 20% x act. pts. Headl. / (3)	Overall Score
weighting (5)	60 %	weighting (5)	15 %	weighting (5)	25 %	
weighted score (6)	(4) x (5)	normalised score (6)	(4) x (5)	normalised score (6)	(4) x (5)	∑(6)
	-	minimum normalised score		e respective star rating		min. overall score
★★★★☆	95 %		75 %		85 %	92 %
$\star \star \star \star \star$	85 %		65 %		70 %	83 %
****	75 %		50 %		60 %	74 %
***	65 %	+		+		65 %
**	60 %					45 %
+	< 60 %					< 45 %
¹ After scaling MDR v						

¹ After scaling MDB x 1.2 / Pole x 1.5

² Optional test items. Maximal total score for all optional items = 7 points.







Protocol 2019

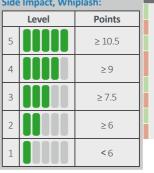
JNCAP

Dummy	Region	Weight	Points	Criteria		
Fronta	al Impac	t against	Rigid \	Wall with 100 % Overlap @ 55 km/h &		
against ODB with 40 % Overlap @ 64 km/h						

				4	HIC ₃₆ < 650	
		Head	0.923	0	HIC ₃₆ > 1000	
				01	Modifier: steering wheel upward displacement 7288 mm	
		Neck	0.231	4	M _{y,extension} < 42 Nm F _{z,tension} < 2.7 kN @ 0 ms / < 2.3 kN @ 35 ms / < 1.1 kN @ 60 ms F _{x,shear} < 1.9 kN @ 0 ms / < 1.2 kN @ 25 – 35 ms / < 1.1 kN @ 45 ms	ting)
		NECK	0.231	0	M _{y,extension} > 57 Nm F _{z,tension} > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms F _{x,shear} > 3.1 kN @ 0 ms / > 1.5 kN @ 25 – 35 ms / > 1.1 kN @ 45 ms	max. 12 points (after weighting)
	HIII			4	Deflection < 22 mm	(aft
	50 %	Chest	0.923	0	Deflection > 42 mm; a _{3ms} > 60 g	nts
				01	Modifier: steering wheel rearward displacement 90110 mm	poi
		Femur	0.923	2	Axial Force _{compression} < 7 kN	12
		remui	0.925	0	Axial Force _{compression} > 10 kN	ax.
		Tibia	0.923	2	TI < 0.4	E
				0	TI > 1.3	
				01	Modifier: Pedal upward displacement 7288 mm	
				01	Modifier: Pedal rearward displacement 100200 mm	
				-1	Modifier: Tibia Axial Force > 8.0 kN	
		Head	0.8	4	HIC ₁₅ < 500	
		neuu		0	HIC ₁₅ > 700	~
		Neck	0.2	4	$\label{eq:Fx,shear} F_{x,shear} < 1200 \ N; \ F_{z,tension} < 1700 \ N; \\ M_{y,extension} < 36 \ Nm$	max. 12 points (after weighting)
			012	0	F _{x,shear} > 1950 N; F _{z,tension} > 2620 N; M _{y,extension} > 49 Nm	er wei
	H III 5 %			4	Deflection < 18 mm	afte
	11111 3 70	Chest	0.8	0	Deflection > 42 mm (ODB) Sallety Wissen by Section 2 and Compared with Section 2 and C	oints (
				4	4 points awarded by default	2 p
		Abdomen	0.8	-2	Modifier: Left belt strap rising (submarining)	×. 1
				-2	Modifier: Right belt strap rising (submarining)	ma
		Fomur	0.4	4	Axial Force _{compression} < 4.8 kN	
		Femur	0.4	0	Axial Force _{compression} > 6.8 kN	

Barrie	r Side In	npact (AE	-MDB)) @ 55 km/h
	Head	1.0	4	HIC ₁₅ < 500
	пеай	1.0	0	HIC ₁₅ > 700
			4	Deflection < 28 mm
WS 50	Chest	1.0	0	Deflection > 50 mm Shoulder Lateral Force > 3.0 kN
front		0.5	4	Deflection < 47 mm
	Abdomen	0.5	0	Deflection > 65 mm
	Pelvis	0.5	4	PSPF < 1.7 kN
	Pelvis	0.5	0	PSPF > 2.8 kN

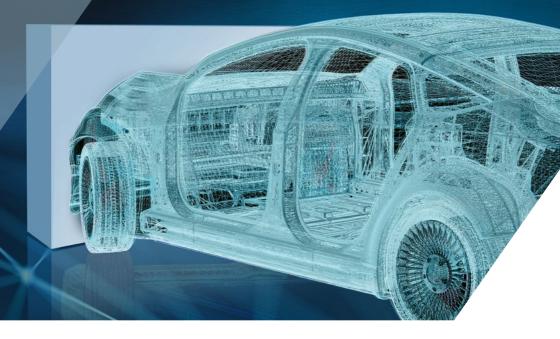
Rating Scheme Frontal & Side Impact, Whiplash:



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Passive Safety Wissen



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Dummy	Criteria		Weight	Points	Limits	
Whip	ash Test					
	NIC		1	4	< 8 m²/s²	
	NIC		T	0	> 30 m²/s²	
	Upper Neck F _{x+}	_		4	< 340 N	
	opper Neck 1 X+	erior		0	> 730 N	
	Upper Neck F _{z+}	crite		4	< 475 N	points (after weighting)
	opper Neck 1 2+	λın		0	> 1130 N	
	Upper Neck My Flexion	on the worst injury criterion		4	< 12 Nm	
				0	> 40 Nm	
BioRID II	Upper Neck My Extension			4	< 12 Nm	
	epper treating Extension		2	0	> 40 Nm	
	Lower Neck F _{x+}	ed		4	< 340 N	
	A.	bas		0	> 730 N	12
	Lower Neck F _{z+}	calculated based		4	< 257 N	max.
		cula		0	> 1480 N	E
	Lower Neck My Flexion	is cal		4	< 12 Nm	
	y riexion			0	> 40 Nm	
	Lower Neck My Extension			4	< 12 Nm	
	y Extension			0	> 40 Nm	

Where a value falls between the upper and lower limit, the score is calculated by linear interpolation (sliding scale).

Passive Safey Rating

		max. weighted		
max. score	weight	score	total	total
n				
12	0.875	10.5		
12	0.875	10.5		
12	0.875	10.5		
12	0.875	10.5	50	100
			29	100
12	0.625	7.5		$\bigstar \bigstar \bigstar \bigstar \bigstar \ge 82^2$
12	0.625	7.5		★★★★ ≥72.5
				★★★≥63 ★★≥53.5
12	0.083	1		★ < 53.5
12	0.083	1		
on (⊃ page 96)				
4	8	32	27	
4	1.25	5	37	
				SafetyWissen by
50	0.04	2	4	
50	0.04	2	4	
	1 12 12 12 12 12 12 12 12 12 1	12 0.875 12 0.875 12 0.875 12 0.875 12 0.875 12 0.875 12 0.875 12 0.625 12 0.625 12 0.625 12 0.625 12 0.083 13 1.25 14 8 15 1.25 15 1.25	max. score weight score 1 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.875 10.5 12 0.625 7.5 12 0.083 1 12 0.083 1 12 0.083 1 12 0.083 1 12 0.083 1 12 0.83 1 12 5 5 13 1.25 5 14 8 32 15 5	max.score weight score total 1 0.875 10.5 12 12 0.875 10.5 12 12 0.875 10.5 12 12 0.875 10.5 12 12 0.875 10.5 12 12 0.875 10.5 12 12 0.625 7.5 12 12 0.625 7.5 12 12 0.625 7.5 12 12 0.625 7.5 12 12 0.083 1 12 12 0.083 1 12 12 0.083 1 12 12 0.083 1 12 12 0.083 1 37 4 1.25 5 37 50 0.04 2 4

¹ For the passenger the same score as for the driver is assumed.

² Downgrade to 4 stars, unless at least level 4 is reached for occupant protection and pedestrian protection.

66



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Category	Impact Safety		Pedestrian Sa	ifety	Driving Safety	
	Full Width Frontal	16	Head Impact	24	Rollover	5
	Offset Deformable Barrier	16	Leg Impact	6	Braking	5
	Barrier Side Impact	16			Basic Active Devices:	
	Child Protection	8			FCW	1
	Whiplash	4			LDW	1
	Pole Side Impact (optional 1)	2			SLD	1
					SBR front	1
					SBR rear	1
					AEB Inter-Urban	2
					AEB City	3
					Additional Active Devices ¹	2
max. total points (1)	60 points		30 points		20 points	
normalized score (2)	actual points / (1)		actual points /	(1)	actual points / (1)	
weighting (3)	60 %		20 %		20 %	
weighted score (4)	(2) × (3)		(2) × (3)		(2) × (3)	

Overall classification: Minimum normalized scores (2) and total score (5) per rating class

1 st Grade	≥ 90.1 %	≥ 60.1 %	-	≥ 86.1 %
2 nd Grade	≥83.1%	≥ 50.1 %	-	≥ 81.1 %
3 rd Grade	≥ 76.1 %	≥ 40.1 %	-	≥ 76.1 %
4 th Grade	≥ 69.1 %	≥ 35.1 %	-	≥ 71.1 %
5 th Grade	≤ 69.0 %	≤ 35.0 %	-	≤ 71.0 %

Star rating per category: Minimum normalized scores (2) for the respective star rating

Category	Impact Safety	Pedestrian Safety	Driving Safety					
****	≥ 93.1 %	≥83.1%	≥ 84.8 %					
****	≥ 90.1 %	≥ 63.1 %	≥ 70.5 %					
***	≥87.1%	≥ 43.1 %	≥ 55.4 %					
**	≥ 84.1 %	≥ 23.1 %	≥ 40.3 %					
*	≤ 84.0 %	≤ 23.0 %	≤ 40.2 %					

¹ Optional items can be assessed upon the manufacturers request. The maximum total points remains the same. ASCC (0.5); BSD (0.5); RCTA (0.5); LKA (0.5); ISA (0.5); AEB Pedstrian (1); Advanced Airbag (1) - Max. total points for Additional Active Devices = 2







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Dummy	Region	Points	Criteria	
Frontal	Impact again	st ODB v	with 40 % Overlap @ 64 km/h	
H III 50 %	Head, Neck	4 0	HIC ₁₅ < 500; a _{3ms} < 72 g; My,extension < 42 Nm; Fz,tension < 2.7 kN; Fx,shear < 1.9 kN HIC ₁₅ > 700 ; a _{3ms} > 80 g; My,extension > 57 Nm; Fz,tension > 3.3 kN; Fx,shear > 3.1 kN	
	Chest	4	Deflection < 22 mm; VC < 0.5 m/s Deflection > 42 mm; VC > 1.0 m/s	
	Femur Knee	4 0	Axial Force _{compr} < 3.8 kN; Knee displacement < 6 mm Axial Force _{compr} > 9.07 kN; Knee displacement > 15 mm	
	Tibia	4	TI < 0.4; Axial Force _{compr} < 2 kN	S
	1010	0 -1 -1 -1 01	TI > 1.3; Axial Force _{compr} > 8 kN Unstable airbag/incorrect airbag deployment (from head score) Excessive head forward excursion (from head score) Steering wheel detachment from steering column (from driver score) Steering wheel upward displacement 7288 mm (from head score)	max. 16 points
Modifiers		01 -1 -2 01 -1	Steering wheel rearward displacement 90110 mm (from head score) Steering wheel contact (from chest score) Shoulder belt load > 6 kN (from chest score) A-pillar rearward displacement 100200 mm (from chest score)	C
	0 0 -1/		Door latch or hinge failure (from chest score) Incorrect airbag deployment (from femur score) Pedal upward displacement 7288 mm (from tibia score) Pedal rearward displacement 100200 mm (from tibia score) Door opening during impact Fuel leakage	
Frontal	Imnact again	st Rigid	Wall with 100 % Overlap @ 56.3 km/h	
Tiontal	Head ¹	4 0	HIC ₁₅ < 500; a _{3ms} < 72 g HIC ₁₅ > 700; a _{3ms} > 80 g	
	Neck ²	4 0	Fx,shear < 1.2 kN; Fz,tension < 1.7 kN; My,extension < 36 Nm Fx,shear > 1.95 kN, Fz,tension > 2.62 kN, My,extension > 49 Nm	
H III 5 %	Chest	4 0	Deflection < 22 mm; VC < 0.5 m/s Deflection > 48 mm; VC > 1.0 m/s	
	Femur	4 0	Axial Force _{compr} < 2.6 kN Axial Force _{compr} > 6.2 kN	ts ⁴
Modifiers -1 -1 -1 -1 -1 -4 -2 -2 -1 -1 -2 -1 -4 -2 -1 -4 -4 -2 -1 -4 -4 -4 -4 -4 -4 -4 -4 -4 -4 -4 -4 -4		-1 -1 -1 -4 -2 -1 -2 -1 -2 -1 -4 -4 -1/door	Unstable airbag/incorrect airbag deployment (from head score) Excessive head forward excursion (from head score) Steering column displacement (from head score) Steering wheel detachment from steering column (from driver score) Rear seat: excessive head forward excursion (from head score) Rear seat: head contact with vehicle interior (from head score) Steering wheel contact (from chest score) Shoulder belt load > 6 kN (from chest score) Incorrect airbag deployment (from femur score) Submarining ³ (from femur score)	max. 16 points ⁴

¹ For the rear passenger in the rigid wall impact the score is based on a_{3ms} only, if there is no hard contact.

² For the rear passenger, the neck score is the sum of all three criteria, with the following maximum score per criterion: Shear 1 point, Tension 1 point, Extension 2 points

³ When any of the two iliac forces drops 1 kN within 1 ms and when the submarining is confirmed on the high speed film.

⁴ The total score is the weighted average of the front seat score (weight = 2) and the rear seat score (weight = 1).

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Dummy	Region	Points	Criteria					
Barrier Side Impact (AE-MDB) @ 55 km/h								
	Head	4	HIC ₁₅ < 500; a _{3ms} < 72 g					
	пеац	0	HIC ₁₅ > 700; a _{3ms} > 80 g					
	Chest	4	Deflection < 28 mm;					
WS 50 %	Chest	0	Deflection > 50 mm; VC \ge 1.0 m/s; Shoulder Force _{Lateral} \ge 3.0 kN	points				
VV5 5U %	Abdomen	4	Deflection < 47 mm;	poi				
		0	Deflection > 65 mm; VC \ge 1.0 m/s	16				
	Pelvis	4	PSPF < 1.7 kN	max.				
	Pelvis	0	PSPF > 2.8 kN	E				
		-1	Incorrect airbag deployment (from head score)					
Modifiers		-1/door	Door opening during impact					
		-1	Fuel leakage					

Pole Side Impact @ 32 km/h							
WS 50 %	Head	2	HIC ₁₅ < 500				
		0	HIC ₁₅ > 700	2 pt			
Modifiers		-1	Incorrect airbag deployment (from head score)	ах. 2			
		-1/door	Door opening during impact	ma			
		-0.5	Fuel leakage				

Whipla	ash Test					
Dynamic	Assessment Front Seat	1.5 Points	0 Points			
	NIC	11.00	24.00		max. 10 points	
	Nkm	0.15	0.55	Its		
BioRID	Rebound velocity (m/s)	3.2	4.8	max. 9 points		
llg	Upper Neck Fx, shear (N)	30	190	94		
ng	Upper Neck Fz,tension (N)	360	750	ах.		
	T1 acceleration ¹ (g)	9.30	13.10	E		
	T-HRC ¹ (ms)	57	82			(4
Geomet	ry Assessment Front Seat	1 Point	-1 Point			to
HRMD	Backset (mm)	40	100	max. 1 pt		led
	Height (mm)	0	80	E 🕂		sca
Geomet	ry Assessment Rear Seat	1 Point	0 Points			ts (
Heff in highest position		≥ 770	< 770			int
(mm)	in worst case position	≥ 720	< 720		ts	14 points (scaled to 4)
		≤ 504.5 • sin (Torso angle-	> 504.5 • sin (Torso angle-	le-		
∆CP X	in highest position	2.6) + 116	2.6) + 116		max. 4 points	nax.
∆СР Х		≤ 504.5 • sin (Torso angle-	> 504.5 • sin (Torso angle-		XE.	
	in worst case position	2.6) + 116	2.6) + 116		Ĕ	
Non-Use	position acc. to KMVSS or no		, i i i i i i i i i i i i i i i i i i i			
Non-Use		yes	no			
Modifier						
	Fixed or integrated head restraint / no height lock -2					
Fixed or i	integrated head restraint / no heigł	nt lock	-2			
	integrated head restraint / no heigł ock failure	it lock	<u>-2</u> -2			

¹ Only the maximum score from either T1 acceleration or head restraint contact time is used in the rating.



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COP Assessment Protocol 1.0

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Adult Occupant Protection

Frontal Impact against ODB with 40 % Overlap @ 64 km/h HIC ₃₆ < 650; a _{3ms} < 72 g My.extension < 42 Nm	
My extension < 42 Nm	
Fz,tension < 2.7 kN @ 0 ms / < 2.3 kN @ 35 ms / < 1.1 kN @ 60 ms	
Head, Neck HIC36 > 1000; a3ms > 88 g 0 HIC36 > 1000; a3ms > 88 g My,extension > 57 Nm Fz,tension > 3.3 kN @ 0 ms / > 2.9 kN @ 35 ms / > 1.1 kN @ 60 ms Fx,shear > 3.1 kN @ 0 ms / > 1.5 kN @ 25 - 35 ms / > 1.1 kN @ 45 ms	S
H III 50 % front 4 Deflection < 22 mm; VC < 0.5 m/s 0 Deflection > 42 mm; VC > 1.0 m/s	17 points
Femur, Knee Displacement < 6 mm	max. 17
Axial Force _{compression} > 9.07 kN @ 0 ms / > 7.56 @ 10 ms Knee Displacement > 15 mm	
Tibia TI < 0.4; Axial Force _{compression} < 2 kN	6
Foot TI > 1.3; Axial Force _{compression} > 8 kN Pedal rearward displacement > 200 mm	
Seat Belt Reminders0.5SBR on driver seat(SBR)0.5/nSBR on front passenger seats (n = number of front passenger seats)	
Total AOP Points $\geq 15^1$ ≥ 11 ≥ 8 ≥ 5 ≥ 2	2

 AOP Star Rating
 $\star \star \star \star \star$ $\star \star \star \star$ $\star \star \star$ $\star \star \star$ -

 ¹ To be eligible for 5 stars the car must score over 14 points in the ODB test (after application of modifiers). In addition, it must have

to be eligible for 5 stars the car must score over 14 points in the ODB test (after application of modifiers). In addition, it must have the full point on SBR, 4 Channel ABS and offer side impact protection demonstrated by a test according to UN R95.

Child Occupant Protection

	Dynamic Assessment: Frontal Impact				Dummy	Q1	1/2	2 Q3	
	Head			points	6	0	6	0	
12 points	ε		no head contact with CRS head contact with CRS	no direct evidence + Head ^a res peak Head a _{res} 3ms	g	< 80 ≤ 72	≥ 88	< 96 ≤ 87	≥ 100
	score from	For	ward Facing CRS		points	6	0	6	0
	scon		forward head excursion	relative to Cr point	mm	< 550	≥ 550	< 550	≥ 550
12 +	worst	Rea	arward Facing CRS		points	6	0	6	0
max. 12	Ň		head exposure	no compressive load on top of head, head fully restrained within CRS		no exposure	exposure	no exposure	exposur
					points	3	0	3	0
	Neck			upper Neck Fz	kN	≤ 1.7	≥ 2.62	≤ 1.7	≥ 2.62
	Chest a _{res 3ms}			g	≤41	≥ 55	≤ 50	≥66	
نہ	CRS Based Assessment								
12 pi	CRS Marking					4 4		4	
	CRS to Vehicle Interface					2 2			
	Vehicle Based Assessment								
٦ts	Airbag Warning /Disabling					5			
points	Three-point Seat Belts					1			
max. 13	Gabarit					1			
.xer	All Passenger Seats Suitable for Universal CRS					1			
		ISOFIX				3			
	Inte	grate	ed CRS					2	

Total COP Points	≥46	≥ 37	≥ 25	≥13	≥0.1	0.0
AOP Star Rating						-









Product Liability in the Automobile Industry

Course Description

In the framework of the ongoing extension of active and passive safety systems automobiles are becoming increasingly complex.

In this context the faultlessness of systems becomes more and more important, as with growing complexity, especially in the field of autonomous vehicles, not only the number but also the severity of possible faults is increasing. Even implemented equal parts strategies can quickly lead to a large number of affected vehicles in case of defects. An indicator for this is the growing number of recalls in recent years.

Each manufacturer holds the responsibility for consequential damages caused by its products when used as intended. This responsibility is defined by law in all countries and has civil and criminal penalties.

Examples include cases of damage and recalls of large numbers of vehicles that several OEMs were obliged to do during the last few years.

Obviously a safety related recall of a mass product may have severe or even existence-threatening consequences.

Consequently, manufacturers must ensure faultlessness throughout their organization. Amongst others, questions may raise like:

- Who in the company is responsible for product safety?
- Is your entire organization set up to avoid safety-related errors or to reduce the risk?
- Is compliance with product liability ensured throughout the company?
- In the case of allegations, can targeted and comprehensive evidence be quickly provided?
- How can unwarranted claims be averted?
- What can be learned from the product liability cases, which are particularly well received by the public?

Course Objectives

The aim of this course is to convey the importance of product liability for businesses and employees as well as an understanding of preventive measures.

Who should attend?

The seminar is aimed at all decision-makers in the automotive development, production and at suppliers who want to learn about the consequences of product liability and want to get familiar with preventive measures.

Course Contents

- Fundamentals of Product Liability
- Civil and criminal responsibility of the company and personal liability of employees
- Liability for Defects
- Product liability in Europe and in the U.S.
- U.S. TREAD ACT, Reporting obligation for OEMs and suppliers
- Motor Vehicle Whistleblower Act (importance to companies)
- EU-Whistleblower Directive
- Importance of norms and standards (e.g. ISO26262 Functional Safety)
- Product liability and advertisement / public relations of companies
- Quality management and its relevance from a product liability point of view
- Product liability in the supply chain
- Consequences of new technologies (driver assistance systems, autonomous vehicles)
- Instructions, warnings
- Risk minimization within the organization, prevention
- Preventive product safety measures during product development
- Product observation and resulting consequences
- Documentation, conclusive evidence
- Insurance of product liability risk
- Recall decision and processing



Hans-Georg Lohrmann was Manager of Reliability & Conformity of Production at ZF TRW Automotive GmbH. He has many years of experience in the field of safety, reliability and product liability in the automotive sector. Since September 2015 he has retired and is still active as a freelance consultant. He specializes in the area of restraint systems for vehicle occupant protection and supports his clients in the areas of reliability, safety planning and methods of verification and litigation support.

ates	DATE	DATE ID VENUE		DURATION	LANGUAGE	
Da	2225.02.2021	116/3789	Online	4 Days	790,- EUR till 25.01.2021, thereafter 940,- EUR	
	0809.06.2021	116/3804	Alzenau	2 Days	1.340,- EUR till 11.05.2021, thereafter 1.590,- EUR	
	2829.09.2021	116/3805	Alzenau	2 Days	1.340,- EUR till 31.08.2021, thereafter 1.590,- EUR	









Static Vehicle Safety Tests in Automotive Development

Course Description

When thinking about vehicle safety testing people first think about dynamic crash tests of the full vehicle or crash simulations performed on a sled test facility. In addition to these dynamic tests, however, numerous other tests on the car body and components such as seats, steering, instrument panel, pillars, bumpers, etc. have to be performed during the development of a car. At first sight, these experiments perhaps are less spectacular, but in practice they are also very complex. The seminar provides an introduction to static vehicle safety testing. Static vehicle safety tests serve the determination of criteria to minimize injury that may occur due to an accident. The seminar covers the entire field of static vehicle safety testing, ranging from biomechanical research to legal regulations and consumer protection related requirements. It discusses the required test equipment (impactors, test facilities) and the typical load cases of the experiments. Finally, the testing specifications, including the protection criteria are explained.

Course Objectives

After participating in the seminar "Static Vehicle Safety Tests in Automotive Development", the participants have gained an overview of the static vehicle safety tests to be performed on the car body and the components. They have acquired knowledge about the essential procedures in Europe and North America as well as their backgrounds and gained insight into equipment necessary to carry out the experiments.

Who should attend?

The seminar is aimed at specialists from crash-related car body and component development, engineers and technicians from test and analysis departments as well as project engineers and managers.

Course Contents

- Introduction
- Static roof crush according to FMVSS 216a
- Static door intrusion according to FMVSS 214
- Test procedures for exterior and interior parts FMVSS 201U, UN R21 & R42
- Testing of seats and head restraints according to FMVSS 202 and UN R17, R21 and R25
- Test procedures on seat-belts according to UN R14 and R21
- Test procedures for steering systems according to FMVSS 203, UN R12
- Test procedures for child seat anchors (ISOFIX) of FMVSS 225





Louis Gautrain (ACTS GmbH & Co. KG) was employed as an engineer at Magna Steyr France from 2008 - 2013. Since 2013 he has been employed at ACTS GmbH & Co. KG in the area of Component & Safety Testing. Since 2018 he has been Senior Test Engineer with ACTS.



Matthias Kunkel (ACTS GmbH & Co. KG) has been with ACTS GmbH & Co. KG in the field of testing since 2000. As a test engineer, he is currently the team leader for component safety tests.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
ã	08.03.2021	140/3705	Alzenau	1 Day	790,- EUR till 08.02.2021, thereafter 940,- EUR	
	2225.11.2021	140/3830	Online	4 Days	790,- EUR till 25.10.2021, thereafter 940,- EUR	









Crashworthy and Lightweight Car Body Design

Course Description

In the development of a car body different - sometimes conflicting - design requirements have to be met. Depending on the intended drive unit, the fulfilling of the crash regulations considering the lightweight principles is a key task. Therefore, it is mandatory that designers have a good understanding of the crash behavior of mechanical structures. The combination of knowledge about mechanics and the ability to use modern design tools allows for an efficient development process without unnecessary design iterations.

Course Objectives

The objective of the seminar is to present new methods for crashworthy car body design. At the beginning of the course the mechanical phenomena of crash events will be discussed. Subsequently modern development methods (CAD design and crash simulation) will be treated. Thereafter modern implementations of safety design measures will be presented. Mathematical optimization of structural design - which is increasingly used in industry - will be covered at the end of the course.

Who should attend?

This 2 day course addresses designers, test and simulation engineers as well as project leaders and managers working in car body development and analysis.

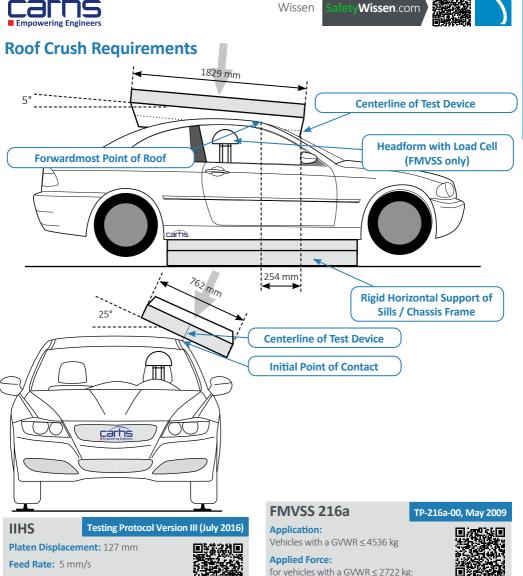
Course Contents

- Mechanics of crash events
 - Accelerations during collisions
 - Structural loading during collisions
 - Examination of real crash events
 - Stability problems
 - Plasticity
- Lightweight principles for the car body design
 - Lightweight design rules
 - Car body design
 - CAE conform design
- Crash simulation
 - Finite Element modeling of a car body
 - Finite Element analysis with explicit methods
 - Possibilities and limitations
 - Technical implementation of safety measures
 - Energy absorbing members
 - Car bodies
 - Electric car bodies
 - Safety systems
 - Pedestrian protection
 - Post crash
- Use of mathematical optimization procedures in real world applications
 - Approximation techniques
 - Optimization software & strategies
 - Shape and topology optimization



Prof. Dr.-Ing. Axel Schumacher (University of Wuppertal) studied mechanical engineering at the universities of Duisburg and Aachen. He received his doctorate on structural optimization from the University of Siegen. Following research projects for Airbus were focused on the optimization of aircraft structures. Thereafter he worked in the CAE methods development department of Adam Opel AG as project leader for structural optimization. From 2003 - 2012 he was a professor at the University of Applied Sciences in Hamburg and taught structural design, passive safety and structural optimization. Since 2012 he has been professor at the University of Muppertal, where he holds the chair for optimization of mechanical structures.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	1215.04.2021	188/3782	Online ¹	4 Days	790,- EUR till 15.03.2021, thereafter 940,- EUR	
	0607.07.2021	188/3783	Alzenau	2 Days	1.340,- EUR till 08.06.2021, thereafter 1.590,- EUR	
	0102.12.2021	188/3784	Alzenau	2 Days	1.340,- EUR till 03.11.2021, thereafter 1.590,- EUR	



Single Side Test: Lab selects worst case

Assessment:

based on Strength-to-weight ratio (SWR) = F_{max} / m x g

SWR	Rating
≥ 4.00	Good
≥ 3.25 till < 4.00	Acceptable
≥ 2.50 till < 3.25	Marginal
< 2.50	Poor

A "Good" rating in the roof crush test is a requirement for the Top Safety Pick award. SafetyWissen by Carhs

for vehicles with a GVWR \leq 2722 kg: $F = 3.0 \times UVW \times 9.8 \text{ m/s}^2$ for vehicles with a GVWR > 2722 kg: $F = 1.5 \times UVW \times 9.8 \text{ m/s}^2$

Feed Rate: ≤ 13 mm/s

Double Sided Test

Requirements:

Platen displacement ≤ 127 mm Load on headform located at head position of 50 % male ≤222 N

UVW = Unloaded Vehicle Weight GVWR = Gross Vehicle Weight Rating



Passive Safety







Passive Safety
 Wissen
 UPDATE



Protection Criteria for Frontal Impact Tests

Configuration Criterion	Criterion		Rigi In-	Rigid Barrier In-Position			Deformable Barrier In-Position	Barrier tion		Out of Position	osition	
		CMVSS 208 (old),	ENAVO	2 200				ENAVICE 200			000	
Requirements		ADR 69/00,		0 200	UN R137	137	011 7.24,				0 200	
		FMVSS 208 (old)	CMIVSS 208	802.9			ADK /3/00	CMIVSS 208		CMVSS 208	807.9	
Dummy		Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	Hybrid III	CRABI
Size		50 % male	50 % male	5 % female	50 % male	5 % female	50 % male	5 % female	5 % female	6 year	3 year	1 year
	HIC ₃₆ / HPC ₃₆ [-]	1000 (FMVSS, ADR)			1000	1000	1000					
Head	HIC ₁₅ [-]	700 (CMVSS)	700	700				700	700	700	570	390
	a _{3ms} [g]				80	80	80					
	N _{ij} [-] (4 Values)		1.0	1.0				1.0	1.0	1.0	1.0	1.0
	F _{x,shear} [kN]				3.1	2.7	3.1 @ 0 ms 1.5 @ 25-35 ms 1.1 @ ≥ 45 ms					
Neck	F _{z,tension} [kN]		4.17	2.62	3.3	2.9	3.3 @ 0 ms 2.9 @ 35 ms 1.1 @ ≥ 60 ms	2.62	2.07	1.49	1.13	0.78
	F _{z,compr.} [kN]		4.0	2.52				2.52	2.52	1.82	1.38	0.96
	M _y [Nm]				57	57	57					
	a _{3ms} [g]	60	60	60				60	60	60	55	50
Chest	Deflection [mm]	76.2 (FMVSS, ADR) 50 (CMVSS)	63	52	42	34	42	52	52	40	34	30 ¹
	VC [m/s]				1.0	1.0	1.0					
Femur	Axial Force [kN]	10	10	6.805	9.07	7	9.07 @ 0 ms 7.58 @ > 10 ms	6.805	6.8			
Knee	Displacement [mm]						15					
Tikin	п[-] п						1.3 (4 Values)				Cofat Minnes	r Cartis
IIDIa	Axial Force _{compr} . [kN]						8.0				Safetywissen by	Dy Traces and the
¹ currently no n	currently no measurement possible	ble										



Passive Safety Seminar





Development of Frontal Restraint Systems meeting Legal and Consumer Protection Requirements

Course Description

Belts, belt-load limiters, airbags, steering column, knee bolster, seat ... - only if all the components of a frontal restraint system are in perfect harmony it is possible to meet the different legal limit values as well as the requirements of consumer tests. However, these requirements, e.g. FMVSS 208, U.S. NCAP, Euro NCAP et al. are manifold and extensive, partly contradict each other, or the requirements superpose each other. Therefore it is a challenge for every development engineer to develop a restraint system by a clear, strategic procedure; time-saving and target-oriented with an optimal result.

In this 2-day seminar this strategic way of development will be shown. You will learn a procedure how to ideally solve the complex development task of a typical frontal restraintsystem design within the scope of the available tools test and simulation. Especially the importance and the influence of individual system components (e.g. belt-load limiters) for the accomplishment of development-sub tasks (e.g. minimum chest deflection) will be covered. In addition the influence of the airbag module design on the hazards of Out-of-Position (OoP) situations is going to be discussed, and a possible development-path for the compliance with the OoP requirements according to the FMVSS 208 legislation will be shown. The possibilities and limits of the development tools test and simulation will be discussed and communicated. Last but not least tips and tricks for a successful overall system design will be part of this seminar.

In this seminar you will become familiar with a procedure for the successful development of a frontal restraint system. Furthermore you will learn which development tool, simulation or test, is best suited for the respective sub task. Moreover you will be made aware of the influence of the individual components of a restraint system (belts, belt-load limiters, airbags, steering column, knee bolster, seat, ...) on the efficiency of the entire system.

Finally future topics such as the compatibility of vehicles as well as pre-crash preparation and prevention of accidents are integrated into the seminar.

Who should attend?

The seminar addresses simulation and test engineers, project engineers and project managers as well as the heads of development departments in the field of passive safety who work on the design of restraint-systems for vehicles.

Course Contents

- Identification of the relevant development load cases
- Procedures for the development of a restraint system
- Influence and importance of individual system components on the overall performance
- Development strategy for UN regulations and NAR restraint systems
- Development path for the conformance to the OoP requirements according to FMVSS 208





Kai Golowko (Bertrandt Ingenieurbüro GmbH) has been working in the area of vehicle safety since 1999. He started his career as a test engineer for passive safety at ACTS. Since 2003 he has been working as senior engineer for occupant safety and pedestrian protection. Since 2005 he has managed the department vehicle safety at Bertrandt in Gaimersheim. He has also been responsible for active and passive vehicle safety for the Bertrandt Group since 2017.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Ď	2829.01.2021	20/3603	Alzenau	2 Days	1.340,- EUR till 31.12.2020, thereafter 1.590,- EUR	
	0811.03.2021	20/3824	Online ¹	4 Days	790,- EUR till 08.02.2021, thereafter 940,- EUR	
	1415.06.2021	20/3825	Gaimersheim	2 Days	1.340,- EUR till 17.05.2021, thereafter 1.590,- EUR	
	1819.11.2021	20/3826	Tappenbeck	2 Days	1.340,- EUR till 21.10.2021, thereafter 1.590,- EUR	

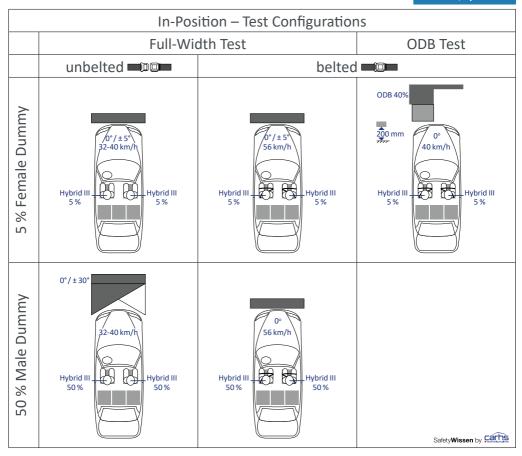


Passive Safety Wissen



FMVSS 208: Frontal Impact Requirements: In-Position

TP-208-14, April 2008



FMVSS 208: Frontal Impact Requirements: Out of Position

Front seat	Dummy	Test configuration			
Driver side	Hybrid III 5 % female	chin on airbag module in steering wheel chin on top of steering wheel			
	CRABI 12 m	in 23 defined CRS / positions			
Passenger side	Hybrid III 3 y/o	chest on instrument panel head on instrument panel			
	Hybrid III 6 y/o	chin on top of steering wheel in 23 defined CRS / positions chest on instrument panel			



Passive Safety Seminar





Development of Frontal Restraint Systems - Advanced

Course Description

Building on the seminar 'Development of Frontal Restraint Systems meeting Legal and Consumer Protection Requirements', this seminar deals with the influence of the adjustment screws in today's highly effective restraint systems. After a short introduction to the worldwide load case mix and the available components and their parameterization, the optimization of systems and their effect on system performance will be elaborated in group work using various practical examples. The analysis of test parameters is the focus of this course. The interactions of the different load cases will be clarified once again and evaluated especially with regard to the new dummy generation around THOR-M and the new US load case Oblique Moving Deformable Barrier (OMDB). This is a workshop aiming at intensive collaboration among the participants.

Course Objectives

The course provides participants with experience in the evaluation of different load cases in frontal passenger protection using practical examples.

Who should attend?

The seminar is aimed at graduates of the course "Development of Frontal Restraint Systems - Advanced" and at developers who have already gained experience in restraint system development.

Course Contents

- Control of the energy of the restraint system
- Control of the kinematics of the occupants
- Achieving the functional objectives



Kai Golowko (Bertrandt Ingenieurbüro GmbH) has been working in the area of vehicle safety since 1999. He started his career as a test engineer for passive safety at ACTS. Since 2003 he has been working as senior engineer for occupant safety and pedestrian protection. Since 2005 he has managed the department vehicle safety at Bertrandt in Gaimersheim. He has also been responsible for active and passive vehicle safety for the Bertrandt Group since 2017.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
۵	0811.02.2021	167/3827	Online	4 Days	790,- EUR till 11.01.2021, thereafter 940,- EUR	
	23.09.2021	167/3828	Alzenau	1 Day	790,- EUR till 26.08.2021, thereafter 940,- EUR	

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Passive Safety Seminar



Early Increase of Design Maturity of Restraint System Components in the Reduced Prototype Vehicle Development Process

Course Description

The number of hardware prototypes available for the development of restraint systems and restraint system components is declining steadily due to an increasing cost pressure in automotive development. In the project schedule the availability of hardware (restraint system components and / or vehicle environments) shifts to the late vehicle development phases. As a result, ensuring the required degree of maturity of restraint system components, in addition to the sole functional development of seat belts and airbag, necessitates new strategies and development paths.

In this seminar, current risks in the development of seat belts and airbags are addressed and ideas for the early increase of maturity are elucidated. This is done by explaining the link between milestones in the development schedule, the functional requirements of restraint system components, the development duration of restraint system components and the description of approaches for the creation of substitutes of vehicle environments in the early development process. In addition the project schedules of conventional vehicle development processes and prototype-reduced development processes of base line models and derivatives are shown. Interactions of the development of seat belts and airbags with surrounding components (e.g. trim parts) are also discussed.

Course Objectives

The course provides thoughts and ideas for a successful approach in the development of restraint systems within vehicle development processes in which only a small number of prototypes are available for verification and optimization of the systems.

Who should attend?

The seminar is aimed at engineers and project managers of restraint systems and restraint system components development, as well as heads of teams or departments in the field of passive safety, which want to gain, in addition to the pure functional development of restraint systems, an overview of the requirements of the prototype-reduced restraint system development with regard to achieving and ensuring the necessary degree of maturity of belts and airbags.

Course Contents

- Overview and differences of vehicle development schedules
 - Standard project schedule
 - Prototype-reduced development of lead series
 - Prototype-reduced development of derivatives
 - Safety belts
 - Examples of requirements for safety belts
 - Prerequisites and timing for functional development
 - Timing for homologation and certification
 - Ideas / possibilities for creating vehicle environments
 - Interactions with surrounding components

Airbags

- Examples of requirements for airbags
- Prerequisites and timing for functional development
- Ideas / possibilities for creating vehicle environments
- Interactions with surrounding components



Sandro Hübner (EDAG Engineering GmbH) studied mechanical engineering at the University of Applied Sciences Schmalkalden. After completing his studies he worked as an engineer in the FEM laboratory of Schmalkalden University of Applied Sciences. From 2003 he worked as a CAE engineer for occupant safety at EASi Engineering GmbH. In 2006, he moved to EDAG Engineering GmbH as a CAE engineer for vehicle safety and has been project manager for vehicle safety and CAE since 2013.

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	2124.06.2021	166/3753	Online	4 Days	790,- EUR till 24.05.2021, thereafter 940,- EUR	
	11.10.2021	166/3752	Alzenau	1 Day	790,- EUR till 13.09.2021, thereafter 940,- EUR	





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Frontal Impact Protection Criteria Compared

Regulation Criterion	Crash Type	ATD [UoM]						Safe	ty Wissen by	carhs.
HIC ₁₅	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	[-]	300	400	500	600	700	800	900	1000
FMVSS 208	FWRB/ODB	HIII 5/50	11111111						1111111111	
FMVSS 208	OOP	HIII 5							-	
FMVSS 208	OOP	HIII 6y/o								
FMVSS 208	OOP	HIII 3y/o								
FMVSS 208	OOP	CRABI 12 m								
Euro NCAP ¹	MPDB/FWRB	TH 50/HIII								
C-NCAP	MPDB/FWRB	TH 50/HIII				(1)				
JNCAP	ODB	HIII 5				<u> </u>				
IIHS	ODB/SOB	HIII 50								
HIC ₃₆		[-]	300	400	500	600	700	800	900	1000
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 5/50								
JNCAP	ODB/FWRB	HIII 50					N////////	N///////	W////////	\setminus
Head a _{3ms}		[g]	60	65	70	75	80	85	90	95
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 5/50								
Euro NCAP ¹	MPDB/FWRB	TH 50/HIII				////////				
C-NCAP	FWRB	TH 50/HIII				N////////				
Chest Com	oression	[mm]	10	20	30	40	50	60	70	80
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 50								
UN R137	FWRB	HIII 5								
FMVSS 208	FWRB/ODB	HIII 5								
FMVSS 208	FWRB	HIII 50								
FMVSS 208	OOP	HIII 5						_		
FMVSS 208	OOP	HIII 6y/o								
FMVSS 208	OOP	HIII 3y/o								
FMVSS 208	OOP	CRABI 12m								
Euro NCAP	MPDB	TH 50					WITTU			
Euro NCAP	FWRB	HIII 5	<u> </u>					N		
C-NCAP	MPDB	TH 50				X \\\\\\\\\\\\	///////////////////////////////////////	\		
C-NCAP		HIII 50			/////////					
C-NCAP JNCAP	MPDB/FWRB ODB/FWRB	HIII 5 HIII 50			X/////////////////////////////////////					
JNCAP	FWRB	HIII 50 HIII 5			X/////////////////////////////////////					
JNCAP	ODB	HIII 5 HIII 5			X					
					W/////////////////////////////////////	W\\\\\\\\				
Legend:		Regulations:	requireme	ents are m	et / NCAP:	maximum	score			

Regulations: requirements not met / NCAP: zero score

Linear interpolation of the score between the upper and lower limit

¹ assessed only if Head ares peak > 80 g

Please note that the values indicated in this graph may be rounded and that additional criteria may exist. Please take exact values and additional criteria from the tables for the respective regulation.





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Regulation Criterion	Crash Type	ATD [UoM]						\$	Safety Wissen	by carhs
Chest a _{3ms}		[g]	30	40	50	60	70	80	90	100
FMVSS 208	FWRB/ODB	HIII 5/50								
FMVSS 208	OOP	HIII 5								
FMVSS 208	OOP	HIII 6y/o								
FMVSS 208	OOP	HIII 3y/o								
FMVSS 208	OOP	CRABI 12 m								
IIHS	ODB/SOB	HIII 50								
JNCAP	ODB/FWRB	HIII 50		///////////////////////////////////////	N///////					
Chest VC _{ma}	X	[m/s]	0	0.2	0.4	0.6	0.8	1.0	1.2	1.4
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 5/50								
IIHS	ODB/SOB	HIII 50								
Euro NCAP	MPDB/FWRB	-						\		
C-NCAP	MPDB/FWRB	HIII / TH				W////////	N///////			
Femur Faxia	al	[kN]	0	2	4	6	8	10	12	14
UN R94	ODB	HIII 50								
UN R137	FWRB	HIII 5								
UN R137	FWRB	HIII 50								
FMVSS 208	ODB	HIII 50								
FMVSS 208	ODB/FWRB	HIII 5								
FMVSS 208	OOP	HIII 5								
Euro NCAP		TH 50/HIII 50								
Euro NCAP C-NCAP	FWRB MPDB/FWRB	HIII 5								
C-NCAP C-NCAP	MPDB	HIII 5					V\\\\\			
JNCAP	ODB/FWRB	HIII 50					///////////////////////////////////////	V		
JNCAP	ODB	HIII 5						N		
			4	6	0	10	12	1.4	16	10
Knee Displa		[mm]	4	6	8	10		14	16	18
UN R94	ODB	HIII 50								
Euro NCAP IIHS	MPDB ODB/SOB	TH 50/HIII 50 HIII 50	J							
C-NCAP	MPDB/FWRB		0			W////////	N///////			
Tibia Index		[-]	0	0.2	0.4	0.6	0.8	1.0	1.2	1.4
UN R94	ODB	HIII 50								
Euro NCAP	MPDB	TH50 /HIII 50	D				11111111			
IIHS	ODB/SOB	HIII 50								
C-NCAP	MPDB/FWRB	TH 50/HIII 50				<u> </u>	N///////	N/////////////////////////////////////	W////	
JNCAP	ODB/FWRB	HIII 50			V////////	N///////	N///////	N///////	N////	
Tibia Comp	ression	[kN]	0	2	4	6	8	10	12	14
UN R94	ODB	HIII 50								
Euro NCAP		TH 50/HIII 50			MIIII	<u>WITTUN</u>				
IIHS	ODB/SOB	HIII 50								
C-NCAP	MPDB/FWRB	TH 50/HIII 50	J		W//////W	N/////////////////////////////////////				

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UPDATE

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2021 2022

Safety Requirements for Rear Seats and Restraint Systems

Frontal impact tests with rear seat occupants

			2021 2022
Euro NCAP FWRB	Euro NCAP / ANCAP MPDB	KNCAP FWRB	ASEAN NCAP ODB
H III 5%	PDB 1400 kg 0°, 50 km/h 50 km/h	H III 5%	ODB 40% 40% 64 km/h 50% Q1.5
JNCAP ODB	C-NCAP FWRB	C-NCAP ODB	Latin NCAP ODB
ODB 40% 40% 64 km/h H III 5 %	HIII 50 km h HIII 5 %	ODB 40% \$0mm \$0,50% \$0mm \$0,50% \$0,50% \$0 km/h \$0,60% \$0,50% \$0,60% \$0,60% \$0,60% <t< td=""><td>ODB 40% \$20mm HIII 50% Q3 HIII 50% Q1.5</td></t<>	ODB 40% \$20mm HIII 50% Q3 HIII 50% Q1.5

FMVSS 201: Head impact on belt		UN R14: Belt
anchorages		UN R16: Belt system
FMVSS 207: Seat stability		UN R17: Seat anchorages
FMVSS 208: Belt system		UN R21: Head impact
FMVSS 209: Belt system		UN R25: Head rests
FMVSS 213: Child seats		UN R44: Child seats
FMVSS 225: ISOFIX anchorages		UN R129: Child seats
		UN R145: ISOFIX anchorages

Side impacts tests with rear seat occupants

2021 2022

FMVSS 214	U.S. NCAP	IIHS / C-IASI	C-NCAP
43 km/h MDB, 1368 kg SID IIS	55 km/h 1368 kg	SID IIS MDB IIHS SO km//n 90°	WS AE-MDB, 1400 k S0 km/h 90° SID IIS ES-2
Euro NCAP MDB	Latin NCAP MDB	ASEAN NCAP	KNCAP
₩S ME-MDB, 1400 K C 60 km/t 90° ₩ ₩ ₩ ₩	So km/h 950 kg 01.5 03	ES-2	WS AE-MDB, 1400 kg 60 km/h 90° Q10 Q6



Passive Safety Seminar



Rear Seat Occupant Protection in Frontal Impact

Course Description

While the design of restraint systems for the rear seats used to be a secondary issue, it has moved in the focus of research and development since the introduction of occupant safety assessments on adult and child dummies in rear seats in consumer protection tests. In addition to looking at Euro NCAP, however, requirements of other NCAPs as well as legal requirements must be considered for a sensible design of the restraint system. Last but not least, a system design must also consider real life aspects. Starting from knowledge on typical injury patterns in real-world accidents, this 1-day seminar discusses both NCAP and legal requirements for the frontal crash. In addition, the dummies to be used in the vehicle rear will be presented. in particular the Q6 and Q10 dummies will be discussed. For the most important load cases, the most relevant protection criteria and possibilities for influencing them through the restraint parameters are being examined. The seminar will be rounded off by approaches for designing restraint systems for the back seat and an outlook on new seating positions possible in the context of automated driving.

Course Objectives

The objective of the seminar is to provide an understanding of the requirements and specifics in rear seat occupant protection, to provide the knowledge of test configurations and dummies, and to provide a view on state-of-the-art solutions.

Who should attend?

The seminar addresses simulation and test engineers, project engineers and project managers as well as the heads of development departments in the field of passive safety who work in R&D of occupant restraint-systems.

Course Contents

- Typical injury patterns in real accident events and injury risk curves
- Legal requirements
- Requirements from consumer testing
- Dummies on the rear seat; Q6 and Q10 child dummies, Hybrid III 5 %
- Relevant protection criteria for the most important load cases
- Solutions for restraint system design and optimization
- Overview: Safety of occupants in new seating positions (automated driving)





Dr-Ing. Burkhard Eickhoff (Autoliv B.V. & Co. KG) studied mechanical engineering in Hannover (Germany) focusing on vehicle engineering and applied mechanics. Starting from 1999 he worked with Autoliv B.V. & Co. KG as a test engineer for sled and crash tests. Since 2003 he has been project manager in systems development (safety belt) of the same company. He was involved in the definition and assessment of new restraint systems and he conducted feasibility studies using system simulation as well as dynamical tests. Moreover he had a consultant role regarding restraint system design. He finished his doctoral thesis at the Helmut Schmidt University Hamburg in 2012 on the reduction of belt induced thorax deflection in frontal crashes. Since 2016 he has been head of the department Virtual & System Engineering, Homologation at Autoliv B.V. & Co. KG.

ŝ	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
8	04.11.2021	146/3746	Alzenau	1 Day	790,- EUR till 07.10.2021, thereafter 940,- EUR	



Passive Safety Seminar







Crash-Sensing and Intelligent Restraint Systems

Course Description

Sensors are the organs of perception of vehicle safety: Recognizing accident risks in split of seconds, they control accident mitigation systems and occupant protection systems accurately, reliably and effectively. Mechanical Electrical Micro Systems (MEMS) such as micro-oscillators or gyros on the scale of micrometers sense even the most subtle movements and shocks and will stabilize the car, prevent vehicle roll and activate the occupant protection systems such as seat belt pre-tensioners, airbags and other protection devices according to crash type and severity. Predictive surround sensors such as radar, LiDAR, cameras and ultrasonic detect accident risks at an early stage and do not only mitigate accidents by automatic emergency braking or evasive maneuvers, but also optimize the effectiveness of occupant protection systems. Since the introduction of seat belt pre-tensioners and driver airbags in the early 80ies the requirements to crash sensors and restraint control electronics have been increased continuously: Starting with single point sensing and focus on frontal crashes with full barrier overlap to trigger driver airbags and seat belt pre-tensioners, all real world accident types and crash severities must be discriminated today utilizing up to a dozen peripheral crash satellites in order to control appropriately up to two dozens of occupant protection devices. New crash tests such as the lateral pole impact or the frontal small overlap crash mandated by regulations and consumer ratings have permanently tightened the requirements to crash sensing and smart restraint control. Above and beyond utilizing the predictive sensors of accident avoidance and advanced driver assistance systems (ADAS), the protection of occupants can be increase significantly: protection devices can be pre-triggered while a crash is imminent, and new protection measures are possible. Last but not least the occupant protection can be adapted and tailored to the occupant size, weight and position (out-of-position) which will be particularly important in autonomous cars with variable seat positions and other new vehicle

interior variances. In the seminar, (predictive-) crash sensors, restraint (pre-) triggering crash algorithms and (pre-crash) occupant protection systems are discussed for the following accident scenarios: Frontal- and rear-end collisions, side impact, vehicle rollover, and accidents with pedestrians and cyclists. From scratch, the seminar explains simply and understandably the physical principles of sensors and measuring systems, their properties and application specific benefits and drawbacks, the restraint triggering algorithms in particular. A specific focus is on future safety systems and technologies, such as artificial intelligence / neural networks, and new occupant protection systems in autonomous cars.

Who should attend?

The seminar addresses all engineers, technicians and experts working in the development, application and research of vehicle safety, both at automobile manufacturers and tier 1/2 / 3 suppliers, system engineers, project engineers and project leaders in particular. Basically, all experts somehow dealing with vehicle safety and being interested in current and future sensor and actuator technologies in passive and active safety are very welcome.

Course Contents

- Sensors for frontal-, rear and side impacts, roll-over, collisions w/ pedestrians & cyclists, occupant recognition & monitoring
- Predictive (surround) sensors (radar, LiDAR, cameras, ultrasonic)
- Intelligent restraint control and triggering, artificial intelligence and neural networks
- Structure and function of sensors and electronic control units, system-architectures
- Today's and future occupant protection systems, integrated safety

nstructo

Dr. Lothar Groesch (Groesch Automotive Safety Consulting) has been working in vehicle safety for more than 40 years, both in passive (crash sensing and electronics, occupant protection) and in active safety (surround sensors, accident avoidance). After working for 18 years for a leading OEM in vehicle safety, his experience was significantly enhanced by working for another 16 years in automotive safety sensors and electronics at a leading automotive supplier. Working as a Product Director for Automotive Safety Systems in the US from 2000 through 2009, he is particularly familiar with the specific requirements of the US market, legislation and product liability. Since 2009, Dr. Groesch has been doing consulting business under the name Automotive Safety Consulting, with the focus on stereo-vision, Radar-application and functional safety. Last but not least, he is teaching at several universities and conducting numerous seminars about Automotive Safety Driver Assistance and Automated Driving and Safety Sensors.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	1618.03.2021	175/3834	Online	3 Days	1.340,- EUR till 16.02.2021, thereafter 1.590,- EUR	
	0103.09.2021	175/3835	Online	3 Days	1.340,- EUR till 04.08.2021, thereafter 1.590,- EUR	





MDB Side Impact Test Procedures according to UN R95, Euro NCAP and IIHS

			2023	
Requirement	UN R95	Euro NCAP	IIHS	
Impact angle		lateral 90°		
MDB velocity	50 km/h	60 km/h	50 km/h (60 km/h)	
Barrier (MDB)	EEVC	AE-MDB	IIHS (IIHS 2.0)	
Mass	950 kg	1400 kg	1500 kg (1900 kg)	
Ground clearance	300 mm	300 mm (bumper 350 mm)	379 mm (bumper 430 mm) 350 mm (bumper 400 mm)	
Upper edge height	800 mm	800 mm	1138 mm (950 mm)	
Width	1500 mm	1700 mm	1676 mm (1700 mm)	
Dummy front seat	ES-2 impact side	WS 50 % impact side, optional WS 50 % on far side (dual occupancy test)	SID IIs impact side	
Dummy rear seat		Q10 impact side Q6 far side	SID IIs impact side	
Protection Criteria	Head HPC < 1000 Chest VC < 1.0 m/s Rib deflection D < 42 mm Abdomen Σ APF < 2.5 kN Pelvis PSPF < 6.0 kN	 page 40 (Adults) page 112 (Children) 	➔ page 51	BafetyWissen by Carths

Pole Side Impact Tests according to Euro NCAP, UN R135, GTR 14, FMVSS 214 and CMVSS 214

Requirement	Euro NCAP	UN R135 / GTR 14	FMVSS 214 / CMVSS 214	U.S. NCAP
Vehicle Velocity (on Flying Floor)	32 km/h up to 32 km/h (26 km/h for vehicles up to 1.5 m width ¹)		up to 32 km/h	32 km/h
Impact angle		0	blique 75° on fixed pole	
Pole diameter			254 mm	
Dummy	Euro NCAP: opt	50 % on impact side tional WS 50 % on far side occupancy test)	ES-2 re or SID IIs (Build Level D) on impact side	SID IIs 5 % on impact side
Protection Criteria	➔ page 40	Head HIC ₃₆ < 1000 Shoulder F _{lateral} < 3.0 kN Chest deflection < 55 mm Abdomen deflection < 65 mm Lower Spine Acc. < 75 g PSPF < 3.36 kN	$ \begin{array}{llllllllllllllllllllllllllllllllllll$	Safety Wissen by Cathe
Test Configuration	32 km/h WS 50 %	15*	32 km/h	32 kmh

¹ GTR 14 only



Passive Safety Wissen

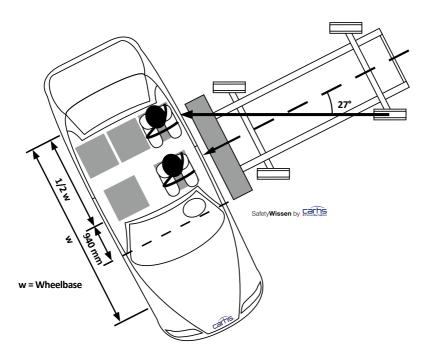
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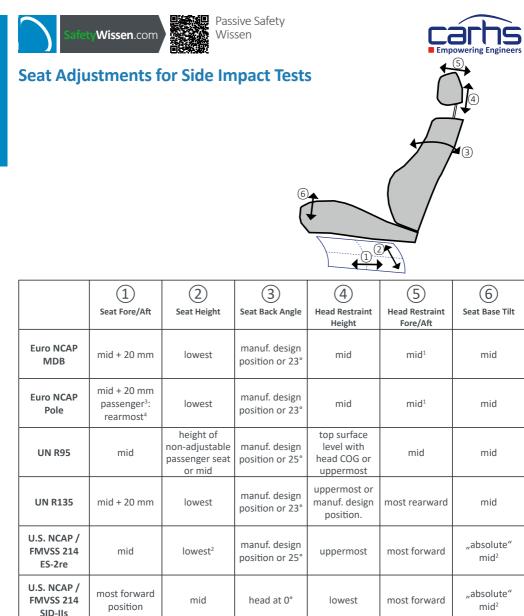


MDB Side Impact Tests according to FMVSS 214, CMVSS 214 and U.S. NCAP

Requirement	FMVSS 214 / CMVSS 214	U.S. NCAP	U.S. NCAP Upgrade ¹			
Impact angle		lateral 90°, 27° crab angle				
Impact velocity	53 ±1 km/h (33.5 mph) (~47 km/h in 90° direction)	61.9 ±0.8 km/h (~55	5 km/h in 90° direction)			
Barrier						
Mass	1368 kg					
Ground clearance		279 mm (bumper 330 mm)				
Upper edge height		838 mm				
Width		1676 mm				
Dummy front seat	ES-2 re impact side	ES-2 re impact side	WorldSID 50 % (SBL F) impact side			
Dummy rear seat	SID IIs (Build Level D) impact side	SID IIs (Build Level D) impact side	SID IIs (Build Level D) impact side			
Protection Criteria	SID IIs: HIC ₃₆ < 1000 Chest acceleration < 82 g Pelvis force < 5.525 kN ES-2 re: HIC ₃₆ < 1000 Chest deflection < 44 mm Abdominal force < 2.5 kN Pelvis force < 6 kN	⇒ page 46	Criteria not yet defined			

¹ planned





0.2						
U.S. NCAP / WorldSID 50	mid + 20 mm	lowest ²	manuf. design position or 25°	uppermost	most forward	"absolute" mid²
ISO WorldSID 50	mid + 20 mm	lowest	manuf. design position or 23°	uppermost or manuf. design position.		

SafetyWissen by

¹ If there is any interference with the rear of the dummy head, move the HR to the most rearward position.

 $^{\rm 2}\,$ Seat base tilt adjustment (6) has priority w. r. t. seat height adjustment (2).

³ For dual occupancy test to prove that interaction between driver and passenger in side impact is prevented

⁴ The head center of gravity must be no further rearward than the pole impact line







Homologation



Durability & RG Fleet Management

NVH



Engineering



Turn-key Projects



System & Component

Development

Euro NCAP & GreenNCAP **Official Laboratory**



Hybrid & Full Electric Vehicle Testing





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Side Impact - Requirements and Development Strategies

Course Description

In addition to the frontal impact, the protection in a side impact has a fixed place in the development of vehicles. Continuous aggravation of consumer tests and legal regulations, due to new pole tests (UN ECE R135 and U.S. NCAP), enhanced deformable barriers and the introduction of World-SID Dummies (5 / 50%ile) with test specific measuring methods are causing a need to further improve side impact protection. In order to achieve this enhancement, it is necessary to get a much more profound understanding of the highly complex phenomena and modes of action in a side impact which goes far beyond the simple application of additional airbags. The seminar provides a comprehensive overview of today's standard test procedures including country-specific variations, the legal regulations and the requirements of consumer protection as well as an outlook on changes in the near future. In addition, tools, measuring methods and criteria, and virtual methods such as crash and occupant simulation, as well as the analysis of the performance of the restraint systems will be discussed. Furthermore it will be explained how a targetoriented use of CAE-simulation and hardware tests can lead to optimal passenger values, while at the same time obeying to boundary conditions such as costs, weight and time-tomarket. A workshop with crash-data analysis finally deepens the understanding.

Who should attend?

The seminar addresses development engineers who are new in the field of side crash, or who have already gained some experience in the field of safety, as well as developers of assemblies that have to fulfil a sidecrash-relevant function. Furthermore it is also interesting for project managers and managers, who deal with side impact and who would like to gain a deeper understanding of this topic in order to use it for an improvement of procedures.

Course Contents

- Challenges of side impacts
- Explanation of the different measuring means, in particular the different dummies
- Overview of current test procedures and side impact relevant protection criteria
 - Legal tests (FMVSS 214, UN ECE R95, UN ECE R135, ...)
 - Other tests (Euro NCAP, U.S. NCAP, further NCAPs, IIHS, manufacturer specific tests)
- Development methods and tools:
 - Crash and occupant simulation, range of application and limitations.
 - Analysis of the performance of protection and restraint systems in side impact. Discussion of the boundary conditions, limits, conflicts and problems
 - Development strategy for an optimal restraint system for side impact
 - Target oriented use of CAE-simulation and hardware tests to develop optimal occupant load values
- Workshop with analysis of crash-data and discussion of the results



Stephanie Wolter (BMW AG) studied engineering physics at the University of Applied Sciences Munich. Since 1995 she has been working at BMW AG in different functions in the field of side protection, such as pre-development, development of side airbags and as a project engineer in various car lines. Moreover, she represents BMW Group in various national and international bodies that deal with side impact and other aspects of side protection, e.g. ISO Working Groups, etc.



Norman Meißner (BMW AG) studied electrical engineering at the University of Applied Sciences in Dresden with a focus on automation and system technology. He has been working in passive safety since 2011 in different functions, initially in the areas of simulation and pre-development, later as a system- and projectengineer. Since 2017, he has been working at BMW AG as a project engineer in the side-crash-development as part of various vehicle projects.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Õ	1215.04.2021	28/3766	Online	4 Days	1.340,- EUR till 15.03.2021, thereafter 1.590,- EUR	
	0708.07.2021	28/3767	Alzenau	2 Days	1.340,- EUR till 09.06.2021, thereafter 1.590,- EUR	
	2021.10.2021	28/3768	Gaimersheim	2 Days	1.340,- EUR till 22.09.2021, thereafter 1.590,- EUR	



Passive Safety Wissen

UPDATE

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Side Impact Protection Criteria Compared

Crash	ATD [-]	300	400	500	600	700	800	900	1000
MDB/Pole ¹	WS 50	111111	11111111				11111111	11111111	minin
MDB	WS 50				<u> </u>				
					$\chi(1)(1)/\chi$	\			
	[-]	300	400	500	600	700	800	900	1000
MDB	ES-2								
	[-]	300	400	500	600	700	800	900	1000
Pole MDB/Pole	WS 50 ES-2/SID 2s								
	[g]	60	65	70	75	80	85	90	95
		111111	11111111				1777 11111	1	1101111
		30 g			*****				
	[mm]	20	25	30	35	40	45	50	55
MDB	ES-2								
Pole	WS 50								
MDB/Pole	ES-2								
MDB/Pole	WS 50			WITT	MITTUN	<u>unnun</u>		\	
				X///////	X///////	X///////	X//////X		
	[kN]	0	1	2	3	4	5	6	7
	WS 50								
	WS 50								
	WS 50								
	[m/s]	0	0.2	0.4	0.6	0.8	1.0	1.2	1.4
MDB	ES-2								
MDB/Pole	WS 50								
MDB	SID 2s								
a _{3ms}	[g]	0	25	50	75	100	125	150	175
Pole	WS 50								
orce	[kN]	0	0.5	1	1.5	2	2.5	3	3.5
MDB	ES-2								
MDB/Pole	ES-2								
-	[mm]	40	45	50	55	60	65	70	75
MDB/Pole	WS 50								
MDB/Pole	WS 50			VIIIIII	V///////	V///////			
MDB	WS 50			<u> </u>	N////////	<u> </u>			
	[kN]	0	1	2	3	4	5	6	7
MDB	ES-2								
Pole	WS 50								
Pole MDB/Pole	WS 50 ES-2								
Pole MDB/Pole MDB/Pole	WS 50 ES-2 WS 50								
Pole MDB/Pole	WS 50 ES-2 WS 50 WS 50								
Pole MDB/Pole MDB/Pole MDB/Pole	WS 50 ES-2 WS 50	0		2	3	4	5	6	7
Pole MDB/Pole MDB/Pole MDB/Pole	WS 50 ES-2 WS 50 WS 50 WS 50	0	1	2	3	4	5	6	7
	MDB MDB/Pole MDB MDB e but capping onl MDB Pole MDB/Pole e but capping onl ression MDB/Pole	MDB WS 50 MDB/Pole WS 50 MDB SID 2s MDB SID 2s e but capping only for HIC > 700 ImbB ES-2 ImbB ES-2 ImbB ES-2 MDB ES-2 ImbB/Pole WS 50 MDB/Pole WS 50 MDB/Pole	MDB/Pole ¹ WS 50 MDB WS 50 MDB/Pole WS 50 MDB SID 2s MDB SID 2s MDB SID 2s e but capping only for HIC > 700 I-] 300 MDB ES-2 I-] 300 MDB ES-2 I-] 300 MDB/Pole WS 50 MDB/Pole WS	MDB/Pole ¹ WS 50 MDB WS 50 MDB/Pole WS 50 MDB SID 2s MDB SID 2s MDB SID 2s e but capping only for HIC > 700 I-1 300 MDB ES-2 I-1 300 MDB ES-2 Image: Interpretent of the system Image: Ima	MDB/Pole1 WS 50 MDB MDB/Pole WS 50 MDB MDB SID 2s MDB MDB SID 2s MDB MDB SID 2s MDB e but capping only for HIC > 700 MDB SID 2s I-1 300 400 500 MDB ES-2 MDB SID 2s I-1 300 400 500 MDB/Pole WS 50 MDB/Pole SID 2s Image: Interpret interpr	MDB/Pole ¹ WS 50 MDB WS 50 MDB SID 2s MDB SID 2s mbb SID 2s mbb SID 2s mbb SID 2s ebut capping only for HIC > 700 Image: Imag	MDB/Pole ¹ WS 50 MDB WS 50 MDB SID 2s I-1 300 400 500 600 MDB ES-2 Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s MDB/Pole WS 50 Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s MDB/Pole WS 50 Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s MDB/Pole WS 50 Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s MDB/Pole WS 50 Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s MDB/Pole WS 50 Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s Image: Sid 2s <	MDB/Pole ¹ WS 50 MDB WS 50 MDB SID 2s MDB Es-2 Image: Side Side Side Side Side Side Side Side	MDB/Pole WS 50 MDB WS 50 MDB SID 2s but capping only for HIC > 700 S00 400 500 600 700 800 900 MDB SID 2s but capping only for HIC > 700 Image: second

Legend:

11

Regulations: requirements are met / NCAP: maximum score Regulations: requirements not met / NCAP: zero score Linear interpolation of the score between the upper and lower limit





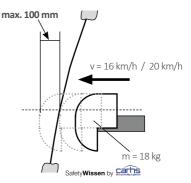
FMVSS 226, CMVSS 226 - Ejection Mitigation

Requirements:

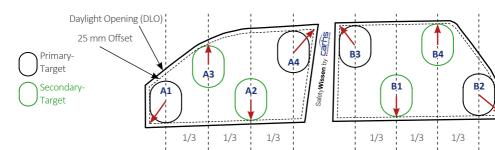
- At up to 4 impact test locations on each side window in the first 3 rows of seats the head excursion may not exceed 100 mm
- Tests at two impact velocities: 16 km/h and 20 km/h
- Head protection systems (e.g. curtain airbags) must be fired before the impact:
 - at 20 km/h with a time delay of 1.5 s prior to the impact
 - at 16 km/h with a time delay of 6 s prior to the impact
- Tests are done without glazing or with pre-damaged glazing
 pre-damage: perforation in a 75 mm grid pattern
- Valid for vehicles with GVWR \leq 4536 kg

Locating Targets:

Front Row Window



Rear Row Windows



Steps	Front Row Window	Rear Row Windows Safety Wissen by
1	Set Primary Target A1 in lower front corner	Set Primary Target B3 in upper front corner
2	Set Primary Target A4 in upper rear corner	Set Primary Target B2 in lower rear corner
3	Divide horizontal distance between A1 and A4 in thirds	Divide horizontal distance between B3 and B2 in thirds
4	Move A3 at the first third vertically upward	Move B1 at the first third vertically downward
5	Move A2 at the second third vertically downward	Move B4 at the second third vertically upward
6	Measure Distances D _x (horizontal) and	D _z (vertical) of the target center points
7	If D _z (A2 - A3) < 135 mm and D _z (A2 - A3) < 170 mm \rightleftharpoons Eliminate A3	If D _z (B1 - B4) < 135 mm and D _z (B1 - B4) < 170 mm \Rightarrow Eliminate B4
8	If D _x (A4 - A3) (or A2 if A3 was eliminated in step 7) < 135 mm and D _x (A4 - A3/2) < 170 mm \Rightarrow Eliminate A3/2	If D _x (B3 - B4) (or B1 if B4 was eliminated in step 7) < 135 mm and D _z (B3 - B4/1) < 170 mm \Rightarrow Eliminate B4/1
9	If D _x (A4 - A2) (or A3 if A2 was eliminated in step 8) < 135 mm and D _x (A4 - A2/3) < 170 mm \Rightarrow Eliminate A2/3	If D _x (B2 - B1) (or B4 if B1 was eliminated in step 8) < 135 mm and D _x (B2 - B1/4) < 170 mm \Rightarrow Eliminate B1/4
10	If D _z (A1 - A4) < 135 mm and D _z (A1 - A4) < 170 mm \Rightarrow Eliminate A4	If D _z (B3 - B2) < 135 mm and D _z (B3 - B2) < 170 mm \Rightarrow Eliminate B3
11	If only 2 targets remain: Measure absolute	e distance D the center points of the targets
12	If D > 360 mm, set additional 3rd target on	the center of the line connecting the targets
13		ctor rotated by 90 degrees. If this results in a higher number of rotated targets.
14		til it is possible to fit the impactor in the DLO-offset. Then place geometric center of the DLO as possible.



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Passive Safety Wissen



Regulations for Head Impact on Vehicle Interiors

UN R21



A pendulum equipped with a spherical impactor (165 mm) hits the interior parts in front of the driver and passenger (side, pedal and steering wheel excluded) with a velocity of 24.1 km/h.

Protection Criteria

a_{3ms} < 80 g; no failure of structure and sharp edges in impact zone

Pendulum test is not necessary, if it can be shown that there is no contact between head and the instrument panel in case of a frontal impact.

This can be done by crash tests, sled tests and/or numerical occupant simulation. (See app. 8 of UN R21)

FMVSS 201U



Test Procedure TP-201U-02, Jan 2016

UN R21, 01 Series, Supplement 3

Test Procedure

A Free Motion Headform (FMH) impactor hits the upper interior parts with a velocity of 24 km/h (A-, B-, C-pillar, roof etc.).

FMH Impactor Data

Mass of FMH impactor: 4.54 kg Head form according to SAE J 921 and J 977 including triaxial acceleration sensor.

Protection Criteria

HIC Calculation

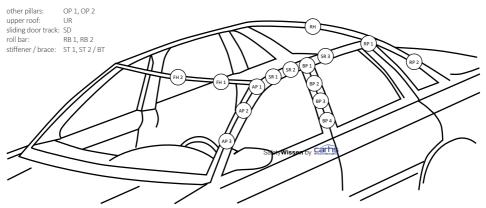
HIC = $\sup_{t_1, t_2} \left\{ \left[\frac{1}{(t_2 - t_1)} \int_{t_2}^{t_2} a dt \right]^{2,5} (t_2 - t_1) \right\} = t_2 - t_1 < 36 \text{ ms; } a \text{ [g]; } t \text{ [s]}$

HIC value for FMH

HIC(d) = 0.75446 HIC + 166.4

HIC(d) must not exceed 1000.

24 points defined for impact according Test Procedure TP-201U-02 (each side, left and right)











Head Impact on Vehicle Interiors: FMVSS 201 and UN R21

Course Description

To prevent injuries resulting from impacts of the occupants' heads on vehicle interior parts, these parts need to be designed in a way which allows sufficient deformation space to reduce the loads on the head. Internationally there are two important regulations regarding the design of interiors, such as cockpits, roof and door liners: The U.S. FMVSS 201 and the Regulation UN R21. Both regulations stipulate requirements concerning the maximum head acceleration or the HIC in impacts on interior parts.

The objective of this course is to provide an overview of the legal requirements and to show how these can be fulfilled. The focus of the seminar is on the development process and the development tools and methods. In particular the interaction of testing and simulation will be described and different design solutions will be discussed. Typical conflicts of objectives in the design - e.g. to fulfil NVH requirements, static stiffness, or misuse, while fulfilling the safety standards at the same time - are addressed in this seminar. Examples of practical solutions will be shown and discussed.

In addition, the development according to the head impact requirements in the overall-context of vehicle development is described in this seminar.

In a workshop exemplary head impact locations in a vehicle interior and impact areas on a dashboard are determined.

Who should attend?

This seminar is especially suited for engineers and technicians who work on the development of vehicle interior parts and who want to become familiar with the safety requirements that are relevant for these parts.

Course Contents

- Introduction
- Rules and regulations concerning head impact
- FMVSS 201
 - UN R21
- Development tools
 - Numerical simulation
 - Test
- Workshop: Determination of impact locations in a vehicle
 - Development process and methods
 - Solving of conflicts of objectives
 - Typical deformation paths, padding materials



Torsten Gärtner (Opel Automobile GmbH) has been working as a simulation expert since 1997. From numerous projects he has extensive experience in the field of occupant simulation and interior safety. He is Technical Lead Engineer Safety Analytics at Opel Automobile GmbH. Before that he worked as department manager for safety with TECOSIM GmbH and spent 10 years in various management positions with carhs gmbh.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	26.03.2021	46/3699	Alzenau	1 Day	790,- EUR till 26.02.2021, thereafter 940,- EUR	
	1718.06.2021	46/3795	Online	2 Days	790,- EUR till 20.05.2021, thereafter 940,- EUR	
	08.10.2021	46/3750	Alzenau	1 Day	790,- EUR till 10.09.2021, thereafter 940,- EUR	



Passive Safety Wissen UPDATE

Test Procedures and Protection Criteria for Pedestrian Protection

						_								_	-						-	-			_		_								
2 Between "Blue	adult headforr	¹ Points to be te	9.5 kg	Upper Legform ⁶	5				Lower Legform ⁶	4					10.5 kg	3			Ø 165 mm	3.5 kg				ø 165 mm	Adult Headform 4.5 kg				Test Method						
Otherwise the adult headlorm is used. Between "Blue Line" and 1000 mm	adult headform impactor, if the points are on the moveable/hinged bonnet top.	Points to be tested that lie between WAD 1500 and 1700 are tested with child-/small	Bending Moment (Nm)	Sum of forces (kN)	VL (km/h)	ACL/PCL Elongation (mm)	MCL Elongation (mm)	Tibia Bending (Nm)	Tibia Bending (Nm)	Femur Bending (Nm)	Ground clearance d (mm)	VL (km/h)	Legform	Bending Moment (Nm)	Sum of forces (kN)	VU (km/h)	αU (°)	HPC/HIC (-)	on Windscreen	WAD (mm)	VC (km/h)	αC (°)	HPC/HIC (-)	on Windscreen	WAD (mm)	VA (km/h)	αA (°)		Parameter						
	are on the m	AD 1500 and	285	л	40	10	19	282			75	40	Flex PLI	285 Nm	5 kN	20 - 33	90 w.r.t. IBRL ⁴ - WAD 930	650	yes	$1000 - 1700 (1500)^{1}$	40	50	650	yes	1700 (1500) ¹ - 2100	40	65	max. score	Euro NCAP / ANCAP U.S. NCAP ⁷						
	oveable/hin	nd 1700 are te moveable/hir	d 1700 are te noveable/hin	d 1700 are te	d 1700 are te	d 1700 are te	d 1700 are te	d 1700 are te noveable/bin	350	6	0	10	22	340			01	0	PLI	350 Nm	6 kN	33	4 - WAD 930	1700	S	0 (1500) ¹			1700	S	0) ¹ - 2100		01	zero score	CAP7
nged bonnet		sted with chi				0	14.8	202			75	40	Flex PLI					650	yes	1000 - 1700	40	50 (20 ²)	650	yes	1700 - 2100	40	65	max. score	JNCAP						
		ild-/small ⁶		-		13	19,8	306				1	ЪГ					1700		1700		0 ²)	1700		2100			zero score	4P						
is at the ch	applied. Fo		300 / 28510 5	ы	40	10	19	282			75	40	Flex PLI					650	yes	1000 - 1700	40	50	650	yes	1700 - 2100	40	65	max. score	KNCAP C-NCAP						
or venicies	r vehicles v	s with a lo	510 / 35010	7.5 / 610		10	22	340										1700		700			1700		100			zero score	4 9						
is at the choice of the manufacturer	vith a lower	wer bumpe					27		275	390	25	40	aPLI					650	yes	$1000 - 1700 (1500)^1$	40	50	650	yes	1700 (1500) ¹ - 2300	40	60 ¹¹ /65	max. score	C-NCAP 2021						
r r	- bumper h	er height <					32		320	440								1700		(1500) ¹			1700		1 - 2300		5	zero score							
neignt ≥ 425 i	leight ≥ 500 m	For vehicles with a lower bumper height < 425 mm the lower	510	7.5	40	13	22	340 (380)5			75	40	Flex PLI					1000 / 1700 ³	no	1000 ⁸ - 1700 ⁹	35	50	$1000 / 1700^3$	no	1700 - 2100 ⁹	35	65		UN R127 KMVSS 102-2						
is applied. For venicles with a lower bumper neight≥425 mm an< 500 mm the impactor is at the choice of the manufacturer	applied. For vehicles with a lower bumper height \geq 500 mm the upper legform test \bigcirc	ower legform test (4) is	510	7.5	40	13	22	340 (380) ⁵			75	40	Flex PLI					1000 / 1700 ³	no	1000 - 1700 ⁹	35	50	$1000 / 1700^{3}$	no	1700 - 2100 ⁹	35	65		GTR No. 9						
m the impactor	gform test 5	st 4 is	510	7.5	40	13	22	340 (380) ⁵			75	40	Flex PLI					1000 / 1700 ³	no	1000 - 1700	35	50	$1000 / 1700^{3}$	no	1700 - 2100	35	65		Japan Article 18 Attachment 99						

- ² Between "Blue Line" and 1000 mm
- ³ The HPC shall not exceed 1000 over one half of the child headform test area and, in test areas. The HPC for the remaining areas shall not exceed 1700 for both headaddition, shall not exceed 1 000 over 2/3 of the combined child and adult headform
- IBRL = Internal Bumper Reference Line torms.

⁵ In an area no wider than 264 mm.

- is at the choice of the manufacturer.
- Proposed U.S. NCAP rating
- ⁸ Minimum 82.5 mm rearward of Bonnet Leading Edge
- Maximum 82.5 mm forward of Bonnet Rear Reference Line
- ¹⁰ C-NCAP







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16th PraxisConference

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Top-class experts

In the lecture session of the conference, representatives from the automotive industry, authorities and institutions will speak about current developments and research projects. International experts will report on the progress of the committees working on legislation and consumer protection test procedures (NCAP). Other presentations will show practical experience in the execution of tests and present new solutions for pedestrian protection.

What is special about the PraxisConference : Hands-on pedestrian protection

As the name suggests, the PraxisConference is not a normal conference, but brings together theory and practice. On both conference days there is a detailed practical session. On the first day, the current test methods for pedestrian protection will be presented in the laboratory and on the BASt outdoor area, both for passive safety and for active safety. On the second day of the conference, automobile manufacturers will present the pedestrian protection measures of their current models directly on the exhibited vehicle and will provide deep insights into the respective solutions.

More than pedestrian protection

When the conference started in 2006, it was still all about pedestrian protection. In the meantime the topic has been broadened: All vulnerable road users (VRU) are addressed, including cyclists and motorcyclists.

Who should attend?

The PraxisConference is aimed at both experts and newcomers in the field of VRU protection. Experts receive an update on current legal and technical developments and use the conference to exchange experiences with colleagues. Beginners will get a very practiceoriented overview of the topic and can use the event to establish contacts with pedestrian protection experts.







Facts

07.-08.07.2021

Bergisch Gladbach, GERMANY & ONLINE

HOMPAGE www.carhs.de/pkf

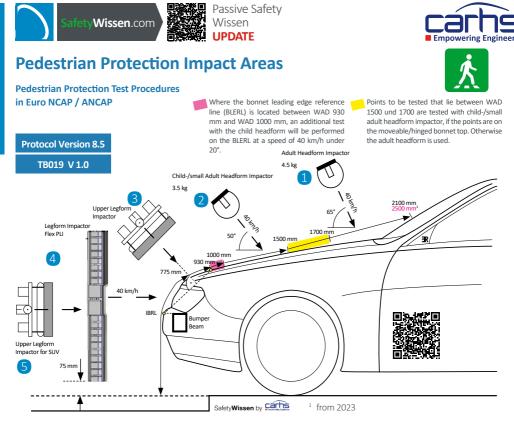
LANGUAGE

PRICE

German with translation into English

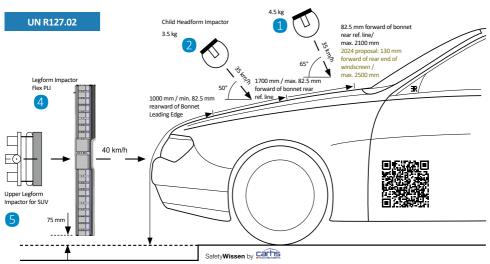
1.490,- EUR till 09.06.2021, thereafter 1.750,- EUR, ONLINE 990,- EUR





Pedestrian Protection Test Procedures according to UN R127.02

Adult Headform Impactor





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Euro NCAP / ANCAP Pedestrian Protection: Head and Leg Impact Grid Method

Head Impact

Between WAD 1000 and WAD 2100 impact points are located on a fixed 100 mm grid. The manufacturer provides a result prediction (points) for the Grid-Points. Euro NCAP verifies 10 randomly selected points, the manufacturer can nominate up to 10 additional randomly selected points. A tolerance of 10 % is applied to the verification tests, i.e. even if the actual HIC is 10 % above or below the margins of the predicted score, the predicted score is applied. At the verification points the actual test result is divided by the manufacturer's prediction. This so called correction factor is applied to all the grid points to obtain the final score:

Wissen.com

Actual tested score

Predicted score = Correction Factor

Predicted score

Per Grid-Point 0 - 1 points are available according to the following scheme:

	HIC ₁₅	< 650	1.00 Point
650 ≤	HIC ₁₅	< 1000	0.75 Points
1000 ≤	HIC ₁₅	< 1350	0.50 Points
1350≤	HIC ₁₅	< 1700	0.25 Points
1700 ≤	HIC ₁₅		0.00 Points

"Default" Results

Grid points on the A-pillars are defaulted to red = 0 points. Grid points on the windscreen that have distance of more than 165 mm from the solid strip around the periphery of the windscreen mounting frame and without any underlying structures within 100 mm measured in the direction of impact are defaulted to green = 1 point. Defaulted locations are not included in the random selection of verification tests. Where the vehicle manufacturer can provide evidence that shows an A-pillar is not red, those grid points will be considered in the same way as other points.

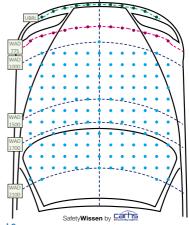
Unpredictable Grid Locations: Blue Zones

In the following areas

- Plastic scuttle
- Windscreen wiper arms and windscreen base
- Headlamp glazing
- Break-away structures

the manufacturer may define a "blue zone" consisting of up to 2 adjacent grid points, for which no prediction is made. A maximum of eight zones may be blue over the entire Headform impact area.

The laboratory will choose one blue point to assess each zone. The test results of blue points will be applied to all the grid point(s) in each zone.



Total Score:

The total score will be calculated as follows:

- Σ Predicted Score x Correction Factor
- + ∑Default Scores
- + \sum Scores from Blue Zones
- = Total
- ÷ Number of Grid Points
- = Percentage of max. achievable score
- x 24 (Maximum achievable score)
- = Total Score for Headform Test

Leg Impact

For leg impact a 100 mm grid on WAD 775 (Upper Legform) respectively on Upper Bumper Reference Line (Flex PLI) is used. Euro NCAP selects either the centerline point or an adjacent point as a starting point for testing. Starting from this position every second grid point will be tested. Symmetry is applied across the vehicle. Grid points that have not been tested will be awarded the worst result from one of the adjacent points. Manufacturers may sponsor additional test for those points that are not tested (in advance). Per Grid point up to 1 point is awarded. For the Upper Legform the score is based upon the worst performing parameter (Sum of Forces / Bending moment). For the Legform the 1 point per grid point is divided into two independent assessment areas of equal weight (0.5 Pts. / each): Tibia moments and ligament elongations.

Total Score:

The total score for the Upper/Lower Legform tests will be calculated as follows:

- \sum Scores of all Grid Points
- ÷ Number of Grid Points
- = Percentage of max. achievable score
- x 6 (Maximum achievable score)
- = Total Score for Legform Test

Assessment Protocol Version 10.0.3 Testing Protocol Version 8.5



Precise Industrial 3D Metrology

High-speed Image Acquisition

Digital Image Correlation Point Tracking Strain, 3D Displacement and 3D Deformation Velocity and Acceleration 6Dof and Trajectories Contour detection

3D Metrology for Crash and Safety Tests

Passenger kinematics Sled Test Side impact Head impact Airbag deployment

Head LCS. Phi(X) Head LCS. Psi(Z) Head LCS. Theta(Y)

Find out more at gom.com/goto/02xs











Pedestrian Protection - Development Strategies

Course Description

Euro NCAP annually adjusts details in its pedestrian rating protocols and even U.S. NCAP plans to introduce a pedestrian protection assessment.

Stricter injury criteria, modified testing areas and the testing of vehicles that were previously not tested because of their weight, require the thorough knowledge of the requirements and a strict implementation of the requirements in the development process.

In the introduction the seminar informs about the different impactors that are used for pedestrian safety testing. Thereafter the various requirements (regulations and consumer tests) are explained and compared.

The focus of the seminar is on the development strategy: Which decisions have to be taken in which development phase? What are the tasks and priorities of the person in charge of pedestrian protection? As a background, ideas and approaches towards the design of a vehicle front end in order to meet the pedestrian protection requirements are discussed. In addition to that, the seminar explains how the function of active bonnets can be proven by means of numerical simulation. This includes both, the pedestrian detection that need to be proven with various impactors or human models, as well as the proof that the bonnet is fully deployed at the time of impact.

Who should attend?

The seminar is intended for development, project or simulation engineers working in the field of vehicle safety, dealing with the design of motor vehicles with regard to pedestrian protection.

Course Contents

- Introduction with an overview of current requirements regarding pedestrian protection
 - Legal requirements (EU, UN Regulations, Japan, GTR)
 - Consumer tests (e.g. Euro NCAP, U.S. NCAP, JNCAP, KNCAP)
- Presentation and discussion of the design and application of the impactors
 - Leg impactors (Flex PLI, Upper Legform, aPLI)
 - Head impactors (Child head, Adult head)
- Methods in numerical simulation, testing and system development
- Requirements on the design of vehicle front ends for pedestrian protection
- Development strategy
 - Interaction between simulation and testing
 - Integration in the vehicle development process
- Solutions to fulfill the requirements
 - Passive solutions
 - Active solutions (active bonnets, airbags)



Maren Finck (carhs.training gmbh) is a Project Manager at carhs.training gmbh. From 2008 - 2015 she worked at EDAG as a project manager responsible for passive vehicle safety.

Previously, she worked several years at carhs GmbH and TECOSIM as an analysis engineer with a focus on pedestrian safety and biomechanics.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	15.03.2021	152/3703	Alzenau	1 Day	790,- EUR till 15.02.2021, thereafter 940,- EUR	
	0710.06.2021	152/3747	Online	4 Days	790,- EUR till 10.05.2021, thereafter 940,- EUR	
	29.11.2021	152/3748	Alzenau	1 Day	790,- EUR till 01.11.2021, thereafter 940,- EUR	





Workshop Pedestrian Protection and Low Speed Crash

Course Description

While pedestrian protection works best when sufficient deformation space is available, for example by means of component failure, damage to the vehicle must be kept to a minimum for the UN R 42, FMVSS 581 and RCAR tests. In this workshop, the aim is to extend the scope of the simulation engineers' work to include function development. This also includes the implementation of component changes and the solution of conflicting objectives. Thus, both disciplines (pedestrian protection and low speed crash) first present their requirements and design criteria, and then search for features that enable the resolution of the target conflicts. Subsequently, the tasks of the function developers are worked out in detail, from the definition of a design strategy to the preparation of tests, including hardware acquisition, up to the final release. The focus is on method transfer instead of training design criteria, which the participants usually master very well due to their daily work.

Course Objectives

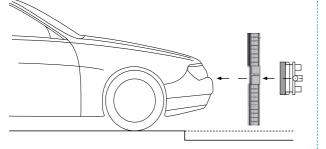
First, the involved groups (Pedestrian Protection and Low Speed Crash) present their respective development goals and constraints to each other to provide a basis for solving the target conflicts. Then the physics of the relevant load cases are worked out in order to technically solve target conflicts. In the final part, the participants are prepared to take on the role of a function developer.

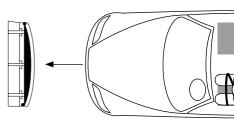
Who should attend?

The one-day workshop is aimed particularly at CAE engineers from the fields of pedestrian protection and low speed crash. Both regularly face conflicting targets when designing the vehicle front end.

Course Contents

- Mutual presentation of legal and consumer protection requirements
 - Test areas on the vehicle
 - Load cases
 - Criteria and limit values
 - Consequences of non-compliance
 - Design criteria
 - Target conflicts
 - Recognize
 - Avoid
 - Disassemble
 - Solve
- Function development
 - Dealing with time schedules
 - Determination of the design space and derivation of a development strategy
 - Pushing through of component changes
 - Test hardware: planning and logistics
 - Test execution: ensuring reproducible results
 - Homologation







Maren Finck (carhs.training gmbh) is a Project Manager at carhs.training gmbh. From 2008 - 2015 she worked at EDAG as a project manager responsible for passive vehicle safety.

Previously, she worked several years at carhs GmbH and TECOSIM as an analysis engineer with a focus on pedestrian safety and biomechanics.

tes	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
B	25.10.2021	192/3832	Alzenau	1 Day	790,- EUR till 27.09.2021, thereafter 940,- EUR	



Passive Safety Seminar



Passenger Cars in Low-Speed Crashes

Course Description

In addition to the design of car structures for the protection of its occupants at high impact velocities, requirements and test procedures for collisions at low speeds, which massively influence the design of the vehicle front, were brought to the fore in recent years.

For the initial insurance classification of passenger cars classification tests of RCAR / AZT (impact speed up to 15 km/h) are used to determine standardized repair costs. To meet the insurance classification tests, many vehicles are equipped with cross member systems that feature energy absorbing elements (crash boxes), that can be connected via a detachable connection to the longitudinal members in the vehicle front.

Additional partly conflicting requirements are added through the UN R127.02 and the NCAP tests for pedestrian protection. Compliance with the directive in the leg impact area is usually achieved by energy absorption in conjunction with a targeted support of the impacting leg in the immediate front area of the vehicle.

In connection with the design of vehicles for the different requirements, numerous conflicts occur, which often can only be solved at the expense of a non-optimum front end package or increased weight and manufacturing costs.

Additional requirements regarding the design of the vehicle front result from legislation for vehicle protection (FMVSS581,UN R42, ...) and internal testing procedures of the manufacturer for ensuring management of everyday damages for his vehicles.

Course Objectives

In this seminar, you first get an overview on the requirements and regulations which have an impact on the design of cars for the various low-speed crash constellations. This is followed by a presentation of current energy management in the front body structure and an introduction of technical solutions. Based on the state of the art approaches of integral safety are discussed.

Who should attend?

The seminar is aimed at specialists from passenger car and light commercial vehicle development, engineers and technicians from simulation and testing, project engineers and managers who want to get an overview of the requirements and technological solutions for the development of passive and integrated safety systems for passenger cars in low-speed crashes.

Course Contents

- Requirements and test procedures for low-speed crash
 - Introduction to the requirements for low-speed crash tests
 - Legal tests
 - Consumer protection tests
 - Other requirements
- Energy management and structural forces in the vehicle front
 - Load paths and structure loading
 - Connections to high-speed test
 - Influencing factors on crash sensing and structural design changes
 - Changes of structural design
 - Influence of crash sensing and restraint systems
- Design of passive systems
 - Existing solutions on the market
 - Conceptual solution approaches
 - Conflicts of objectives
 - Technological feasibility and limits
- Discussion of integral safety systems
 - Potential of integrated solutions
 - Technological feasibility and limits



Prof. Dr. Harald Bachem (Ostfalia University of Applied Sciences) has been in charge of teaching and research in vehicle safety at the Ostfalia University of Applied Sciences since 2011. Prior to joining the university he held various management positions in industry where he was in charge of development and testing of vehicle safety functions. His last management position was head of cab body development at MAN Truck & Bus AG. Prof. Bachem is chairman of the Wolfsburg Institute for Research, Development and Technology Transfer e. V.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
ő	1922.04.2021	159/3733	Online	4 Days	790,- EUR till 22.03.2021, thereafter 940,- EUR	
	02.11.2021	159/3732	Alzenau	1 Day	790,- EUR till 05.10.2021, thereafter 940,- EUR	

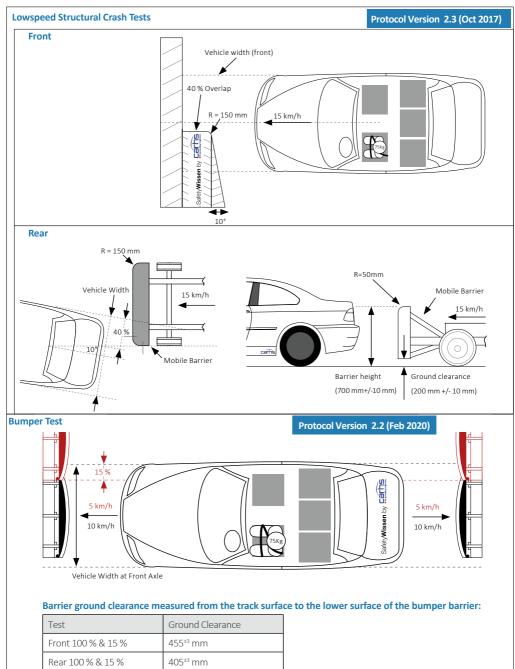


UPDATE

iety Wissen.com



RCAR Insurance Tests







Whiplash Requirements Front Seats

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	1
Gaps	
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Delta Theta	
HIC ₁₅	
Head Contact Time HCT	
Head Rebound Velocity	
Upper Neck Force F _{x+}	
Upper Neck Force F ₂₊	
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Seatback Deflection Angle	•
Dummy Artefact Modifier	•
Seat Track Dynamic Displacement	
Upper Neck Tension F ₂ + UN Momentum My	
Lower Neck Force F _{x+}	
Lower Neck Force F ₂₊	
Upper Neck Momentum My	
Lower Neck Momentum M _y	

¹ Capping only

This table is based on material generated by: LEAR Whiplash Applied Research Group

106







In co-operation with:



Heckaufprall-Sitze-Whiplash

The passive safety of motor vehicles has been a major focus of the automotive world over the past 4 decades. In this context, rear impact has also become the focus of lawmakers and consumer protection organizations.

In 2019 and 2020, the rating guidelines for whiplash were changed and the weighting in the adult rating was doubled to 10%. In advance of the Euro NCAP changes, the GTR on whiplash has also been tightened. Because of the enormous volume of damage, the insurance industry also has a keen interest in protecting occupants in rear-end collisions

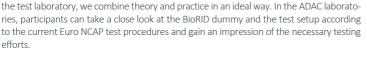
Autonomous driving: When the frontal impact turns into a rear impact.

Autonomous driving will enable new seating arrangements and occupant positions. To protect occupants in these situations as well, legislators and consumer protection organizations will set new requirements. These new requirements, as well as development strategies and solutions, will be a focus of this year's conference.

Through our concept of the PraxisConference, where part of the conference takes place in







Conference Topics

- Accident research & biomechanics
- Regulations and consumer protection requirements
- Occupant protection for alternative seating positions in autonomous vehicles .
- Praxis part at the ADAC Technology Centre
- Presentation BioRID, handling and positioning
- Sled test according to Euro NCAP
- Measurement of rear seat headrest according to Euro NCAP
- Test technology for rear-end collisions
- Numerical simulation н.
- н. Development strategies and solutions

Who should attend?

The PraxisConference is aimed at employees of the automotive industry who want to deal with the rear-end collision and gain a comprehensive overview of the topic. Experts receive an update on current legal and technical developments and use the conference to exchange experiences with colleagues. Beginners receive a practice-oriented introduction to the topic and can make contacts with experts.

DATE VENUF HOMPAGE LANGUAGE 10.-11.11.2021 Bad Wörishofen, GERMANY

www.carhs.de/pkh

PRICE

1.490,- EUR till 13.10.2021, thereafter 1.750,- EUR









Passive Safety Wissen UPDATE



Euro NCAP / ANCAP Front Seat Whiplash Assessment

Dynamic Assessment	Assessment	Protocol Version	n 9.1.2	Testing Protocol		
Whiplash Test	r	Medium Severity Puls	se		High Severity Pulse	
SafetyWissen by	Higher Limit	Lower Limit	Capping Limit	Higher Limit	Lower Limit	Capping Limit
NIC	11.00	24.00	27.00	13.00	23.00	25.50
Nkm			0.69			0.78
Rebound velocity (m/s)			5.2			6.0
Upper Neck F _{x,shear(+ve)} (N)	30	190	290	30	210	364
Upper Neck F _{x,shear(-ve)} (N)			360			360
Upper Neck F _{z,tension} (N)	360	750	900	470	770	1024
Upper Neck My,extension+flexion (Nm)			30			30
Lower Neck F _{x,shear(ABS)} (N)			360			360
Lower Neck My,extension+flexion (Nm)			30			30
T1 acceleration (g)			15.55			17.80
T-HRC (ms)			92			92
Seatback Deflection (°)						32

* All parameters, except rebound velocity, are calculated until THRC-end (= End of Head Restraint Contact Time).

If the Higher Performance Limit is reached, **1 point** is awarded **per criterion**. A sliding scale is used between Higher and Lower Performance Limit (1 0 points). If the capping limit is exceeded by one criterion, the entire test is rated with zero points.

Modifiers

Seatback Dynamic Deflection

A **-3 point** modifier will be applied where the seat has a dynamic deflection \ge 32° in the high severity pulse test.

Dummy Artefact Loading

A **-2 point** modifier will be applied as a means of penalizing any seat that, by design, places unfavorable loading on other body areas or exploits a dummy artefact.

Static Assessment

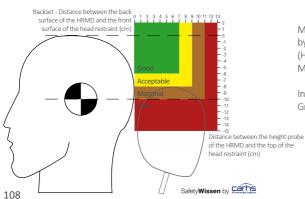
	Head Restrai in Test Position (mid r	nt Geometry ange locking position)	Head Restraint Geometry in Worst Case Position (= lowest & rearmost)		
	Higher Limit	Lower Limit	Limit		
Score	+1 Point	-1 Point	+1/n Points per front seat (n = number of front seats)		
Effective Height (mm)	825	755	> 790		
Backset (mm)	< 45	≥ 45	< 70		

The assessments are based on the worst performing parameter from either the height or backset.

Overall Rating

For the overall rating the total of max. 8 points (3 per pulse + 1 Geometry + 1 Worst Case Geometry) is scaled by the factor 0.375 to a maximum of 3 points and is part of the Adult Occupant Protection rating.

Static Geometry Assessment by IIWPG / IIHS



RCAR Version 3 (Mar 2008)

IIHS Version VI (Nov 2020)

Measurement of the head restraint position by a "Head Restraint Measuring Device" (HRMD) and rating as Good, Acceptable, Marginal or Poor.

International Insurance Whiplash Prevention Group (IIWPG)

Learn more about IIHS's static and dynamic assessment ⊃ page 50









Whiplash Testing and Evaluation in Rear Impacts

Course Description

In real-world accidents, distortions of the cervical spine or so-called whiplash injuries following a rear impact are among the most expensive injuries for the insurance industry. About 75 % of all injury costs of the insurers are caused by whiplash injuries in highly-motorized countries. About 80 % of all injuries in a rear impact are whiplash-injuries. This is why this type of injury - even though it is neither very serious nor lethal - has reached a high priority in the endeavors to develop test procedures and assessment criteria which help in designing constructive measures in the car in order to avoid this type of injury.

As an introduction, this seminar refers to the different accident data for whiplash injuries, which offer many realizations but no consistent pattern with regard to the biomechanical injury mechanisms. However, some organizations - mainly from the field of consumer information and insurance institutes - are working on the development of test procedures and assessment criteria. The most active ones are Thatcham (UK) and IIHS (USA) which are united in the group IIWPG (International Insurance Whiplash Prevention Group), SNRA and Folksam (Sweden) and the German ADAC.

In 2008 Euro NCAP has introduced a whiplash test procedure as part of its rating system. In 2014 an additional static assessment for the rear seats was added. In 2020 Euro NCAP introduced a new Whiplash assessment on front seats. Where concepts and methods from the future legal requirement the Global Technical Regulation No. 7 Phase II (Head Restraints) can be recognised. The Euro NCAP assessment will be explained in detail in the seminar. Furthermore, the EEVC working group 20 is active as a consulting authority concerning whiplash injuries for the legislation in Europe. The Global Technical Regulation No. 7 Phase I (Head Restraints, short GTR 7) is unsatisfactory from the European point of view. Therefore the United Nations work on a second phase of this regulation. The content of the GTR 7 Phase II gives the legal base for the future HR development requirements. The focus of this work is on improving the BioRID dummy and on the definition of so called Seat Performance Criteria.

All discussions about the assessment of whiplash injuries within the framework of consumer information have in common, that the protection effect in a rear-end impact needs to be examined in an isolated vehicle seat by means of a sled test using a generic acceleration pulse. It turns out to be problematic, however, that presently there is no traumato-mechanical explanation of the phenomenon "whiplash injury" and that all the currently discussed dummy criteria with the respective limit values follow a so-called "black-box approach". Experts try to correlate the measured dummy criteria with the findings from accident data and to thus derive limit values. In this context the available dummy-technology with the different measuring devices and criteria, as well as the proposed limit values are going to be presented.

In the last part of the seminar different seat design concepts (energy-absorbing, respectively geometry-improving), subdivided into active and passive systems will be introduced, and their advantages and disadvantages will be discussed.

Who should attend?

The seminar addresses development engineers who are new in the field of rear impacts or who have already got some experience in the field of safety, as well as developers of subassemblies which have to fulfill a crash-relevant function. It is furthermore especially interesting for project managers and managers who deal with the topic of rear-end impacts and who would like to obtain a better knowledge of this subject in order to use it for an improvement of procedures.

Course Contents

- Introduction into the characteristics of a rear-end impact
- Overview of the most important whiplash requirements
- Injury criteria
- Dummy-technology for rear impacts
- Presentation of the Euro NCAP and FMVSS 202-dynamic test procedures
- Outlook on possible harmonization-tendencies
- Explanation of the possible design measures in car seats



Thomas Frank (LEAR Corporation GmbH) joined the passive safety department of LEAR Corporation in 2002 after graduating from the Technical University of Berlin in physical engineering sciences. At LEAR Thomas Frank initially worked as a test engineer in crash testing, later he developed head rests. Today he is expert for head restraints and low speed rear impact safety. In his position he guides the seat development with respect to meet whiplash protection requirements in regulations and consumer tests.

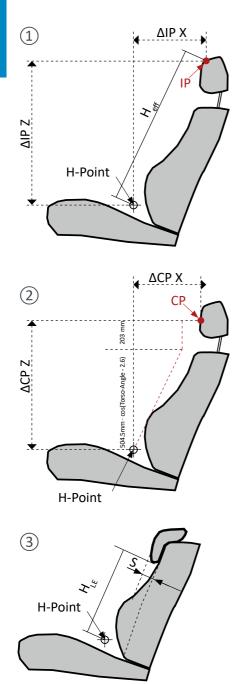
ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	23.02.2021	50/3695	Alzenau	1 Day	790,- EUR till 26.01.2021, thereafter 940,- EUR	
	2023.09.2021	50/3749	Online	4 Days	790,- EUR till 23.08.2021, thereafter 940,- EUR	



Passive Safety Wissen



Euro NCAP / ANCAP Rear Seat Whiplash Assessment



Assessment Protocol Version 9.1.2

Testing Protocol Version 1.1

(1) Effective Height H_{eff} requirements for the headrest: in highest position \geq 770 mm

and in worst case position \geq 720 mm

Calculation of H_{eff}:

 $H_{eff=} \Delta IP \ X \cdot sin \ (Torso-Angle) + \Delta IP \ Z \cdot cos \ (Torso-Angle) \\ IP: Intersection \ Point$

Determination of IP X and IP Z:

IP X = $88.5 \cdot sin (Torso-Angle- 2.6) + 5 + CP X$ IP Z = uppermost intersection of the headrest contour in the seat centerline with a vertical line through IP X

(2) Backset ΔCP X requirements for the headrest

in mid position and in worst case position:

 $\Delta CP X \le 7.128 \cdot Torso-Angle + 153$ CP: Contact Point

③ Requirements for the non-use position of the headrest:

- 1) Automatic Return Head Restraint, or
- 2) > 60° rotation of the headrest in non-use position, or
- 3) Δ Torso-Angle use / non-use > 10°, or
- 4) Height of lower edge of the headrest H_{LE}: 250 mm \leq H_{LE} \leq 460 mm with H_{LE} = $\Delta X \cdot sin$ (Torso-Angle) + $\Delta Z \cdot cos$ (Torso-Angle), or
- 5) Thickness of the lower edge of the headrest $S \ge 40 \text{ mm}$

Score if the Requirements (see above) are met:

The outboard seating positions of rear seating rows are assessed. Any centre seating position needs to comply with the requirements of UN R17.08.

Parameter	Points per seat
1 H _{eff}	1.5
② ΔCP X _{mid}	1*
② ΔCP Xworstcase	0.5*
③ Non-Use	1*
max. total	4
Scaling	1/8n (n = number of seats)

* only if Heff requirements are met



Passive Safety Seminar







Child Protection in Front and Side Impacts Current and Future Requirements

Course Description

For the transport and the protection of children in cars, child protection systems have been on the market since the 70ies. It was, however, only after the introduction of the European test regulation UN Regulation No. 44 in 1980, that their quality and effectiveness have reached a minimum standard that was acceptable at that time. Further developments of the legal regulations along with additional tests of different European consumer protection organizations - e.g. the German Stiftung Warentest, ICRT (International Consumer Research and Testing; governing body of the European product testers), Öko Test - and also the motor press (auto motor und sport, ADAC, Auto Bild, ÖAMTC) finally led to a significant decrease in the number of accident victims among children. Unfortunately the applied test setups and rating procedures in the sled tests vary greatly and partly lead to significantly diverging results, which can cause misunderstandings among consumers, manufacturers and developers.

Right from the start Euro NCAP has also tested child protection systems in full-size-front and side-impact tests and has introduced a separate test and assessment protocol for the evaluation of the protective effect of Child Restraint Systems (CRS). However, hereby only CRS recommended by the automotive OEMs are used in the tests.

The endeavours for research and harmonization of the New Programme for the Assessment of universal Child Seats (NPACS), founded in 2002, can be seen as the latest development on an European level. Members of NPACS are ICRT, ADAC and several European governments. In an initial phase, the test procedures of the ADAC and ICRT are to be harmonised.

Euro NCAP has revised it's child occupant assessment. Since 2013 Q dummies have been used in the dynamic assessment. In addition a CRS installation test was introduced. A significant change was the consideration of older children (Q6 and Q10) than in the previous protocol from 2015 onwards. This enables Euro NCAP to better assess the performance of the vehicle's restraint systems.

Course Objectives

In this seminar you will learn to understand the specific problems in child safety and you will become familiar with the approaches concerning child safety with which you can meet the different requirements.

Who should attend?

The seminar addresses engineers who deal with the development and design of child restraint systems and their integration into the passenger protection systems.

Course Contents

- Introduction: historical development of child safety, accident statistics, usage rates of child protection systems, injury biomechanics of children
- Child dummies: P-series, Q-series
- Legal requirements: UN R44, R129 and other legal requirements, sled tests, full-size front and side impact tests with special requirements concerning child protection
- Consumer protection tests, other tests, harmonization: Euro NCAP, NPACS; ISO proposal side impact, AMS, ADAC, others
- Child protection systems: types and classifications, standards, ISO-FIX, Top Tether, Ease of Use/Misuse



Britta Schnottale (BASt - German Federal Highway Research Institute) is working as a scientific assistant in the department for "Passive Safety and Biomechanis" of the German Federal Highway Research Institute (BASt).Here she is responsible for safety issues concerning children in vehicles. This includes participation in national research projects as well as in EU projects on child safety (CHILD, CASPER). She was a member of the informal working group of the GRSP "Child Safety" on the development of UN R129. Britta Schnottale is also a member of the Euro NCAP Child Safety Working Group.

ŝ	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
^ع /	12.11.2021	45/3781	Alzenau	1 Day	790,- EUR till 15.10.2021, thereafter 940,- EUR	

Euro NCAP / ANCAP Child Occupant Protection

Wissen.com

Dynamic Assessment

Testing:

Passive Safety

Test Protocol Version 7.3.1 Assessment Protocol Version 7.3.1

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	Qe the	: The Q6 of the vehicle n	lummy shall be seated in an appropriate CRS for a six year old child or a chile nanufacturer, or if there is no recommendation, a suitable CRS from the top	d with a stature of pick list.	125 cm. This will be either the CRS recommended by
	ma	anufacture	0 dummy shall be seated on a booster cushion only. This will be the booster r recommends a high back booster with detachable backrest it will be used hosen by Euro NCAP from a list of suitable options contained in the Technica	without backrest.	ended by the vehicle manufacturer. Where the vehicl If there is no recommendation for a booster cushion
	Pre	econdition	s: Where any of the following events occur zero points will be awarded to t	he dummy.	
	Fro	ontal impa	ct: During the forwards movement of the dummy only, the diagonal belt slip	os off the shoulde	r.
			ct: The pelvis of the dummy submarines beneath the lap section of the belt nd and is no longer restraining the pelvis.	or the lap section	does not prevent the dummy from moving upwards
	Fro	ontal and s	ide impacts: The dummy pelvis does not remain in the booster seat / cushic	on and is not corre	ectly restrained by the lap section of the seatbelt.
	Fro	ontal and s	ide impacts: CRS does not remain within the same seating position or is no	longer correctly re	estrained by the adult belt.
			ide impacts: There is any breakage or fracturing of load-bearing parts of the	-	
			ide impacts: There is any breakage or fracturing of any seat belt lock-offs, te sed to anchor the CRS to the vehicle fail.	thers, straps, ISOF	IX anchorages or any other attachments which are
	M	odifier: If,	during the forwards movement of the dummy, the diagonal belt moves into enalty of -4 points will be applied to the overall dummy score of the impact		
		Dummy		Points	Criteria
		Frontal I	npact (MPDB)		
				4	$HIC_{15}^{1} \le 500; a_{3ms} \le 60 g$
			Used	0 + Capping	$HIC_{15}^{1} \ge 700$ (capping: 800), $a_{3ms} \ge 80$ g
			Head	-2 (Modifier ²)	Head forward excursion > 450 mm
		Q6 /		-4 (Modifier)	Head forward excursion > 550 mm
	ş	Q10	Upper Neck	2	$F_z \le 1.7 \text{ kN}$
	nax. 24 points			0	$F_z \ge 2.62 \text{ kN}; \text{ My} \ge 36 (Q6) / 49 (Q10) \text{ Nm}$
s	24		Chest	2	$a_{3ms} \le 41 \text{ g}$ (Q10); Deflection $\le 30 \text{ mm}$ (Q6)
max. 49 points	max			0 + Capping ³	$a_{3ms} \ge 55 \text{ g} (Q10); \text{ Deflection} \ge 42 \text{ mm} (Q6)$
49 p		Side Imp	act (MDB)		uno 1.500 - 50
nax.			Head	2 0 + Capping	$HIC_{15}^{1} \le 500, a_{3ms} \le 60 \text{ g}$ $HIC_{15}^{1} \ge 700 \text{ (capping: 800), } a_{3ms} \ge 80 \text{ g}$
-		Q6 /		0 + Capping	$F_{res} < 2.4$ kN (Q6); $F_{res} < 2.2$ kN (Q10)
		Q10	Upper Neck	0	$F_{res} \ge 2.4 \text{ kN} (Q6); F_{res} \ge 2.2 \text{ kN} (Q10)$
				1	a _{3ms} <67 g
			Chest	0	a _{3ms} ≥67 g
	In	stallatio	on of CRS		
		Universa	CRS	points	4
	12 p ¹	ISOFIX C	S	points	2
	nax. 12	i-Size CRS		points	4
	F	manufac	turer recommended CRS	points	2
	Ve	ehicle B	ased Assessment		
	Pre	econdition	IS:		
	Pro	ovision of	hree-point seat belts on all passenger seats		
			vehicle handbook stating clearly, which seating positions are suitable or not		
			senger frontal airbag is fitted (both front and rear seats if applicable), the CF rbags are active the seat is NOT suitable for any rearward facing CRS.	S tables in the vel	nicle handbook must clearly indicate that when these
		Compati	pility of the 2nd row outboard seats with Gabarit according to 16 Annex 17 - Appendix 1	points	1
		Compati	bility of all other passenger seats with Gabarit according to 16 Annex 17 - Appendix 1	points	1
	points		ith i-Size & TopTether marking (for ISO/B2 i-Size fixture defined in UN ECE	points	2
	x. 13		ndent seats with i-Size and TopTether marking	points	1
	max.	2 or mor	e seating positions are suitable for fully independent use with the largest arward facing (Class C) ISOFIX CRS, Fixture (CRF) ISO/R3,	points	1
			r airbag warning marking and manual / automatic disabling	points	2/4
		integrate	d CRS	points	1 (1 CRS) / 3 (2 or more CRS)
			only applied if there is hard head contact, otherwise the score is based on a	_{3ms} only	
111	2	² Q10 on ³ capping	y applied for Q10 a _{3ms} only		
112	۷	cabbulg			



Passive	S	afe	ety
V	Ni	SS	en

UPDATE

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Protocol 2020 V1.1.2

Latin NCAP Child Occupant Protection

Requirements for points for Child Protection Rating: Child seats (CRS) for 1½ & 3 y/o children must be recommended by the vehicle manufacturer. CRS must be available for purchase from dealers in the 3 big Latin NCAP markets (AR, BR, MX) and in every other market where the vehicle is sold. CRS must be available at the 3 most important cities of each of the 3 big markets in at least 2 retailers per city. CRS manufacturer must be officially represented in each of the 3 big markets.

U		-		essment	kets in at least 2 retailers per city. CRS manufactu	Dummy	Q		1)3					
	<u> </u>				ssessments: no partial or full ejection of child du										
				by any of the vehicle interface		ining out of		st not be part		unie					
		Hea	d Co	ntact with the vehicle: any he	ad contact with the vehicle results in 0 points for	the head pe	formance								
				npact											
	1	Hea	d			points	4	0	4	0					
10		шo		no head contact with CRS head contact with CRS	no direct evidence + Head ^a res peak Head a _{res} 3ms	g	< 80 ≤ 72	≥ 88	< 96 ≤ 87	≥ 100					
oints		re fi	For	ward Facing CRS		points	4	0	4	0					
6 pc	•	scol		forward head excursion	relative to Cr point	mm	≤ 549	≥ 550	≤ 549	≥ 550					
max. 16 points		worst score from	Rea	rward Facing CRS		points	4	0	4	0					
ũ		Ň		head exposure	no compressive load on top of head, head fully contained within CRS		no exposure	exposure	no exposure	exposu					
						points	2	0	2	0					
		Nec	:k		upper Neck F _z	kN	≤ 1.7	≥ 2.62	≤ 1.7	≥ 2.6					
		Che	st		ares 3ms	g	≤ 41	≥ 55	≤ 50	≥ 66					
ß	Ľ	Side	e Imp	act											
Requirements for Points in Side Impact: head containment within shell of CRS, also there must be no fracturing of the CRS Head no head contact with CRS head contact with CRS head ares geak g < 80 < 72 ≥ 88 < 72															
6.8	1	Hea	d			points	4	0	4	0					
				no head contact with CRS head contact with CRS	no direct evidence + Head ares peak Head ares 3ms	g	< 80 ≤ 72	≥ 88	< 80 ≤ 72	≥ 88					
Ins			on of												
2				the reference list		points 10									
				nmended by the manufacture	r	points	points 2								
Ve	ehi	icle E	Based	d Assessment											
	_			of three-point seat belts					with a 3 point based assessn						
					Gabarit according to UN ECE R16.05	points			2						
			-		usly accommodate any reference list CRS	points			1						
nts	3		-	positions that can simultaneo	· · ·	points			1						
points				er seats equipped with ISOFIX		points 1 points +1									
. 13				ese 2 passenger seats meet i-S		points			-1						
max	s	size (of rea	positions comply with require arward facing ISOFIX seats	ments for largest	points	1								
				nger airbag		points	2 max. 4								
			-	r airbag warning and disabling		points									
			•	ed CRS		points			1 1						
S F			-	ed "Group I-III" CRS	Occupant Protection	points	- 202		rotocol Ve	rsion 2					
	_			Assessment: Frontal Impact	occupant i rotectior	Dummy	Q			13					
		Hea	d			points	4	0	4	0					
				no head contact with CRS	no direct evidence + Head ^a res peak	g	< 80		< 96						
				head contact with CRS	Head ares 3ms	5	≤ 72	≥88	≤87	≥ 100					
S		mo								0					
pints		re from	For	ward Facing CRS		points	4	0	4						
l6 points		t score from		ward Facing CRS forward head excursion	relative to Cr point	mm	4 ≤ 549	≥ 550	≤ 549						
max. 16 points		worst score from		ward Facing CRS forward head excursion Irward Facing CRS	relative to Cr point		4 ≤ 549 4 no	≥ 550 0	≤ 549 4 no	0					
max. 16 points		worst score from		ward Facing CRS forward head excursion	relative to Cr point	points	4 ≤ 549 4 no exposure	≥ 550 0 exposure	≤ 549 4 no exposure	0 exposu					
max. 16 points		Ň	Rea	ward Facing CRS forward head excursion Irward Facing CRS	relative to Cr point no compressive load on top of head, head fully restrained within CRS	points points	4 ≤ 549 4 exposure 2	≥ 550 0 exposure 0	≤ 549 4 no exposure 2	0 exposu 0					
max. 16 points	1	> Nec	Rea k	ward Facing CRS forward head excursion Irward Facing CRS	relative to Cr point no compressive load on top of head, head fully restrained within CRS upper Neck F _z	points points points kN	4 ≤ 549 4 exposure 2 ≤ 1.7	≥ 550 0 exposure 0 ≥ 2.62	≤ 549 4 exposure 2 ≤ 1.7	0 exposu 0 ≥ 2.62					
max. 16 points	1	> Nec Che	Rea k st	ward Facing CRS forward head excursion rward Facing CRS head exposure	relative to Cr point no compressive load on top of head, head fully restrained within CRS	points points	4 ≤ 549 4 exposure 2	≥ 550 0 exposure 0	≤ 549 4 no exposure 2	0 exposu 0					
pt. r		≥ Nec Che Dyn	Rea k st amic	ward Facing CRS forward head excursion Irward Facing CRS	relative to Cr point no compressive load on top of head, head fully restrained within CRS upper Neck F _z	mm points points kN g	4 ≤ 549 4 no exposure 2 ≤ 1.7 ≤ 41	≥ 550 0 exposure 0 ≥ 2.62 ≥ 55	≤ 549 4 no exposure 2 ≤ 1.7 ≤ 50	0 exposu 0 ≥ 2.62 ≥ 66					
8 pt. r		> Nec Che	Rea k st amic	ward Facing CRS forward head excursion nward Facing CRS head exposure Assessment: Side Impact	relative to Cr point no compressive load on top of head, head fully restrained within CRS upper Neck F _z ares 3ms	points points points kN	4 ≤ 549 4 exposure 2 ≤ 1.7 ≤ 41	≥ 550 0 exposure 0 ≥ 2.62	≤ 549 4 no exposure 2 ≤ 1.7 ≤ 50	0 exposu 0 ≥ 2.62					
max. 8 pt.		≥ Nec Che Dyn	Rea k st amic	ward Facing CRS forward head excursion rward Facing CRS head exposure	relative to Cr point no compressive load on top of head, head fully restrained within CRS upper Neck F _z	mm points points kN g	4 ≤ 549 4 no exposure 2 ≤ 1.7 ≤ 41	≥ 550 0 exposure 0 ≥ 2.62 ≥ 55	≤ 549 4 no exposure 2 ≤ 1.7 ≤ 50	0 exposu 0 ≥ 2.62 ≥ 66					
8 pt. r		≷ Necl Che: Dyn Hea	Rea k st amic	ward Facing CRS forward head excursion rward Facing CRS head exposure Assessment: Side Impact no head contact with CRS	relative to Cr point no compressive load on top of head, head fully restrained within CRS upper Neck F _z ares 3ms no direct evidence + Head ares peak	points points kN g points	4 ≤ 549 4 exposure 2 ≤ 1.7 ≤ 41 4 4 < 80	≥ 550 0 exposure 0 ≥ 2.62 ≥ 55	≤ 549 4 exposure 2 ≤ 1.7 ≤ 50	exposu 0 ≥ 2.62 ≥ 66					

べ Child Presence Detection



Protocol 2019

Dummy	Region	Points	Criteria		
Frontal	Impact again	st ODB v	with 40 % Overlap @ 64 km/h		
		4	HIC ₁₅ < 500; a _{3ms} < 60 g		
	Head ¹	0	$HIC_{15} \ge 700$; $a_{3ms} \ge 80$ g		
		-4	Modifier: Head forward excursion ≥ 550 mm		
Q6	Neck ²	2	My,extension < 36 Nm; Fz,tension < 1.7 kN		
	NECK	0	$M_{y,extension} \ge 36 \text{ Nm}; F_{z,tension} \ge 2.62 \text{ kN}$	S	
	Chest	2	Deflection < 30 mm	max. 16 points	
	Chest	0	Deflection > 42 mm	5 pc	
		4	HIC ₁₅ < 500; a _{3ms} < 60 g;	. 16	
	Head ¹	0	$HIC_{15} \ge 700$; $a_{3ms} \ge 80$ g;	nay	
		-2/-4	Modifier: Head forward excursion ≥ 450 mm / 550 mm	-	
Q10	Neck ²	2	My,extension < 49 Nm; Fz,tension < 1.7 kN		
	NECK	0	$M_{y,extension} \ge 49 \text{ Nm}; F_{z,tension} \ge 2.62 \text{ kN}$		
	Chest	2	a _{3ms} < 41 g		ing
	Chest	0	a _{3ms} ≥ 55 g		rat
Barrier	Side Impact (AE-MDE) @ 60 km/h		points in the overall rating
	Head ¹	4	HIC ₁₅ < 500; a _{3ms} < 60 g		000
	Heau	0	$HIC_{15} \ge 700$; $a_{3ms} \ge 80$ g		the
Q6	Neck	2	F _{z,tension} < 2.4 kN		.⊆
QU	NECK	0	$F_{z,tension} \ge 2.4 \text{ kN}$	S	ints
	Chest	2	a _{3ms} < 67 g	max. 16 points	
	Chest	0	a _{3ms} ≥ 67 g	5 pc	80
	Head ¹	4	HIC ₁₅ < 500; a _{3ms} < 60 g;	ć. 1	n to
	neau	0	$HIC_{15} \ge 700$; $a_{3ms} \ge 80$ g;	na)	No No
Q10	Neck	2	Fz,tension < 2.2 kN	-	o pa
QIU	NECK	0	$F_{z,tension} \ge 2.2 \text{ kN}$		cale
	Chest	2	a _{3ms} < 67 g		S SI
	Chest	0	a _{3ms} ≥ 67 g		oint
Modifier	hi ana 14 fb ann an an	-4	If, during the forwards movement of the dummy, the diagonal belt moves the gap between the clavicle and upper arm with folding of the belt webb a penalty of -4 points will be applied to the overall dummy score of the im in which it occurs.	ing,	max. 32 points scaled down to 8

Preconditions: Where any of the following events occur, zero points will be awarded to the dummy.

Frontal impact: During the forwards movement of the dummy only, the diagonal belt slips off the shoulder.

Frontal impact: The pelvis of the dummy submarines beneath the lap section of the belt or the lap section does not prevent the dummy from moving upwards during rebound and is no longer restraining the pelvis.

Frontal and side impacts: The dummy pelvis does not remain in the booster seat / cushion and is not correctly restrained by the lap section of the seatbelt.

Frontal and side impacts: CRS does not remain within the same seating position or is no longer correctly restrained by the adult belt.

Frontal and side impacts: There is any breakage or fracturing of load-bearing parts of the belt system including buckles, webbing and anchorage points.

Frontal and side impacts: There is any breakage or fracturing of any seat belt lock-offs, tethers, straps, ISOFIX anchorages or any other attachments which are specifically used to anchor the CRS to the vehicle fail.

 $^{\scriptscriptstyle 1}~$ In the absence of hard contacts the score is based on a_{3ms} only.

 $^{\scriptscriptstyle 2}~$ In the absence of hard contacts the score is based on neck tension force only.

4	$\leq 50 \text{ cm}^{\circ}$	≤ 45 km/n	≤ 350 kg ³	≤ 4 KVV		
4			≤ 400 kg ^{3,4}	≤ 15 kW		
		Vehicles use	ed for the carria	ge of passenger	S	
≥4					≤9	
≥4					> 9	≤ 5 t
≥4					> 9	> 5 t
		Vehicles u	used for the car	riage of goods		
≥ 4						≤ 3.5 t
≥ 4						3.5 t < m ≤ 12 t
≥ 4						> 12 t
		Traile	rs (including ser	ni-trailers)		
						≤ 0.75 t
						0.75 t < m ≤ 3.5 t
						3.5 t < m ≤ 10 t
						> 10 t
		Agricu	ultural or forest	ry vehicles		

Passive Safety Wissen

Unladen

Mass

250 kg 3

UNECE Vehicle Classification

Wheels

2

3

2

3¹

3²

Consolidated Resolution on the Construction of Vehicles (R.E.3), Revision 6 Engine

Capacity

 $\leq 50 \text{ cm}^3$

 $\leq 50 \text{ cm}^3$

> 50 cm³

> 50 cm³

> 50 cm³

 $< E0 \text{ cm}^3$

Maximum

Design Speed

≤ 50 km/h

≤ 50 km/h

> 50 km/h

> 50 km/h

> 50 km/h

< 15 km/h

G Off-road vehicles ¹ asymmetrically arranged in relation to the longitudinal median plane

² symmetrically arranged in relation to the longitudinal median plane

³ not including the mass of the batteries in case of electric vehicles

 $^{4} \leq 550$ kg for vehicles intended for carrying goods

Applicability of selected UN Regulations to Vehicle Categories:

UN R	L1	L2	L3	L4	L5	L6	L7	M1	M2	M3	N1	N2	N3	01	02	03	04
11								•			•						
12								•			•						
14								•	•	•	•	•	•				
16		•		•	•	•	•	•	•	•	•	•	•	•	•	•	•
17								•	•	•	•	•	•				
21								•									
25		•		•	•	•	•	•	•	•	•	•	•				
32								•									
33								•									
42								•									
94								•									
95								•			•						
100								•	•	•	•	•	•				
127								•			•						
135								•	\bullet^1		•	\bullet^1					
137								•									
145								•							Safety	Vissen by	carhs
¹ ontio	nal un te	4500	kσ														



Category

L1

L2

L3

L4

L5

L6 L7 Μ M1 M2 M3 Ν N1 N2 N3 0 01 02 03 04 Т



Maximum Mass



Wissen.com

Seats

Power





SAFETYTESTING



Crash and Safety Testing are key elements in the product development cycle of any new vehicle development. The partners of **SafetyTesting+active** are leading companies in crash and safety testing technology serving the global automotive markets.

You can expect a full day of expert presentations focussing on the hot topics in crash and safety testing, presented by the technology leaders in the industry. The **SafetyTesting**+*active* conference that has been established in 2011 is part of the SafetyWeek in Würzburg, Germany.

Conference Topics

The **SafetyTesting**+active conference will feature presentations on the following topics:

- Full Scale Crash Testing Technologies
- Advanced Sled Simulation with Live Battery Testing Applications
- Measuring Technologies and Data Acquisition
- Lighting and Video Technology
- VRU Test Tools
- New Testing Technology for ADAS and ADS

Who should attend?

The **SafetyTesting**+*active* conference is suited for engineers and decision makers from testing departments for active and passive safety. Both experts and newcomers get an overview over the latest innovations in test equipment and software tool and find ample opportunity to share their own experiences with industry colleagues.









31.08.2021

Hompage

DATE

VENUE

Würzburg, GERMANY & ONLINE www.carhs.de/safetytesting











Introduction to Data Acquisition in Safety Testing

Course Description

Sensor technology and data acquisition are central elements of safety testing. A 100 % reliability of the used technology in combination with the highest accuracy of the employed sensors are the basis for the success and usefulness of the tests in vehicle development.

The course first presents a short overview on the historical development of data acquisition technology in the safety field and continues by going into details of current technologies of sensors, data acquisition as well as dummy and vehicle instrumentation.

Based on the procedures of a safety test, the different tasks of calibration and certification of sensors, filtering and evaluation of signals, as well as the calculation and evaluation of measurement errors will be explained.

The course provides the basic knowledge in crash data acquisition and gives a comprehensive overview on the procedures employed in data acquisition in the crash testing environment.

Course Objectives

The course participants will learn about the technology and terminology of sensor and data acquisition technology used in safety testing. They will be qualified to define tests, to supervise tests and to interpret and evaluate test results.

Who should attend?

This introductory course aims at new test engineers and project engineers as well as engineers from simulation departments at automotive OEMs, suppliers and engineering service providers.

Course Contents

- Sensors
 - Basic sensor principles
 - Sensors in safety testing
 - Selection of sensor systems
 - Systems for data acquisition (DAS)
 - State of the art in DAS technology
 - InDummy and Onboard DAS
 - Filtering
- Instrumentation
 - Overview dummy instrumentation
 - Overview vehicle instrumentation
 - Overview instrumented barriers
- Evaluation & Measuring Errors
 - Error calculation (set-up of sensors, sensors, DAS, evaluation ...)
 - Sources of errors in crash testing
 - Interpretation of signals
 - Calibration and Certification
 - Dummy certification
 - Sensor calibration
 - SAE J211
 - Procedures
 - Test preparation
 - Test execution
 - Test evaluation



Thomas Wild (Continental Safety Engineering International GmbH) studied Electrical and Tele-Communications Engineering at the Technical University Darmstadt. Since 1996 he has been employed at Continental Safety Engineering International as a measurement engineer. 1998 - 2001, he assumed additional responsibilities as an application engineer in the algorithm development. Since 2003 he is team leader measurement and video technology. Since 1997 he works in the working group Data Processing in Vehicle Safety (MDVFS).

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Ö	2629.01.2021	123/3786	Online ¹	4 Days	790,- EUR till 29.12.2020, thereafter 940,- EUR	
	0506.10.2021	123/3785	Alzenau	2 Days	1.340,- EUR till 07.09.2021, thereafter 1.590,- EUR	
	¹ Online Semi	nar with red	duced content			117





Highspeed Camera Recording Settings

Variable	Derivation	Symbols	Units
Framerate	$f = \frac{v}{s} \cdot n_{frame}$	f Framerate v Velocity s Displacement nframe Number of frames	fps m/s m frames
	Sample - Car: v = 40 m/s	$f = \frac{40 \text{ m/s}}{1.6 \text{ m}} \cdot 1$ frame = 25 fps	
	<i>s</i> = 1.6 m	$f = \frac{40 \text{ m/s}}{1.6 \text{ m}} \cdot 5 \text{ frame} = 125 \text{ fps}$	
Exposure as derivative of the displacement	$E = \frac{B_S}{v}$	EExposureBsAcceptable Motion Blur as DisplacementνVelocity	s m m/s
	Sample - Bicycle: v = 10 m/s	$E = \frac{0.4 \text{ m}}{10 \text{ m/s}} = 0.04 \text{ s} = 1/25 \text{ s}$	
	$B_S = 0.4 \text{ m or } 0.04 \text{ m}$	$E = \frac{0.04 \text{ m}}{10 \text{ m/s}} = 0.004 \text{ s} = 1/250 \text{ s}$	
Exposure as derivative of the resolution	$E = \frac{B_r \cdot D_x}{(v \cdot X)}$	B_r Acceptable Motion Blur as Resolution D_x Imagewidth D_y Imageheight	pixel m m
	$E = \frac{B_r \cdot D_y}{(v \cdot Y)}$	X Horizontal Image ResolutionY Vertical Image Resolution	pixel pixel
	$B_r = \frac{B_S}{P}$	B_{s} Acceptable Motion Blur as Displacement	m
	$P = \frac{D_X}{X} P = \frac{D_Y}{Y}$	P Pixelcalibration	m/pixel
方。	•	Frame 8 320 ms	
<u>オ オ オ オ オ オ オ オ オ オ オ オ オ オ オ オ オ オ オ </u>		Frame 7 280 ms	40 mm motion blur
* 50		Frame 6 7 8	@4 ms shutter
方。		Frame 5 200 ms displacement displacement	400 mm nent motion blur
*		Frame 4 (925 fps 160 ms) framerate framerate	@40 ms
东岙		Frame 3 120 ms	
方。忝		Frame 2 80 ms	40 m/s
方。		Frame 1 40 ms	5 frames
方			@125 fps 1 frame @25 fps

SafetyWissen in Cooperation with Photron Deutschland GmbH

Photron HIGH-SPEED CAMERAS

Ideally suited for both on-board and off-board vehicle safety testing, Photron FASTCAM high-sped cameras deliver excellent resolution, high frame rate, outstanding image quality and the best light sensitivity in its class.





4 Mega Pixel @ 1,400fps (12-bit) Sealed body Remote lens control





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Dummy | Crash Test ssen UPDATE



Current Dummy Landscape

GTR 7 (Head Restr.)		AL ANCAP	S ADR (Frontal, Side)	A ASEAN NCAP	sia KNCAP •	C-NCAP	China Regulations	JNCAP	Japan Regulations	Ar Latin NCAP	•	U.S. NCAP	FMVSS xxx (OMDB)	FMVSS 202a	FMVSS 213	FMVSS 214	FMVSS 208	E Euro NCAP	•	UN R135	UN R129	UN R44	UN R95	UN R94	Dummies HIII HIII HIII HIII	Frontal Impact
	L	•			•	•						0	0					•							THOR 50 %	
			•	•		•	•		•	•													•		ES-2	Side Impact
							•					•				•									ES-2re	Ipact
						•					•	•				•									SID-IIs	
•	L	•	•		•	•	•	•	•			0				0		•		•					World SID	
														•											HIII 50 %	Rear Impact
	•	•			•	•		•			•							•							BioRID II	npact
	Γ														•		•								CRABI	Child
															•										CAMI	
SafetyWiss															•		•								HIII	
SafetyWissen by									•						•							•			P Series	
់ហី [/]		•		•	•	•				•					0			•			•				Q Series	



See your crash test images

in a whole new light

The Atlas Constant Light[™] system is now even more versatile.

Introducing the CL2000, the world's brightest 1800W continuous-mode floodlight. Based on the same revolutionary LED technology as the CL4000, the compact CL2000 is ideal for illuminating smaller target zones, component and airbag test stands, pit applications and more. Get the full picture at **atlas-mts.com**.





CL4000 — 3600W Ideal for large target zones



CL2000 — 1800W Ideal for small target zones







its for U.S. Limits for Euro

THOR 50 % Male Injury Criteria, Risk Functions and proposed Limits

				NC.	AP^1	NC	AP
Region	Criterion	Calculation ¹	Risk Function ³	Full score	Zero score	Full score	Zero score
	HIC ₁₅ (-)	$\left (t_2 - t_1) \left[\frac{1}{(t_2 - t_1)} \int_{t_1}^{t_2} a(t) dt \right]^{25} \right _{max}$	$p(\text{AIS } 2+) = \Phi\left[\frac{\ln HIC_{15} - 6.96362}{0.84687}\right]$ $p(\text{AIS } 3+) = \Phi\left[\frac{\ln(HIC_{15}) - 7.45231}{0.73998}\right]$	500	700	500	700
Head	Brain Injury Criterion BrIC (-)	$\begin{split} \sqrt{\left(\frac{\max(\omega_{x})}{\omega_{xc}}\right)^{2} + \left(\frac{\max(\omega_{y})}{\omega_{yc}}\right)^{2} + \left(\frac{\max(\omega_{z})}{\omega_{xc}}\right)^{2}} \\ & \text{with } \omega_{[x,y,z]} = \text{Angular velocity } (\text{rad/s}) \\ & \omega_{xC} = 66.25 \text{ rad/s} \\ & \omega_{yC} = 56.45 \text{ rad/s} \\ & \omega_{zC} = 42.87 \text{ rad/s} \end{split}$	$p(\text{AIS 3+}) = 1 - e^{-\left(\frac{BTIC - 0.523}{0.531}\right)^{1.8}}$ $p(\text{AIS 4+}) = 1 - e^{-\left(\frac{BTIC - 0.523}{0.647}\right)^{1.8}}$	0.71	1.05	-	-
	a3ms [g]			-	-	72	80
	N _{ij} (-)	$\label{eq:Fz} \begin{split} \frac{F_z}{F_{zc}} + \frac{M_y}{M_{yc}} \\ \text{with } F_{\text{ZC}} = 4200 \text{ N/}-6400 \text{ N} (\text{tension/compression}) \\ \text{M}_{yC} = 88.1 \text{ Nm} / -117 \text{ Nm} (\text{flexion/extension}) \end{split}$	$p(\text{AIS } 2+) = \frac{1}{1 + e^{(5.819 - 5.681Nij)}}$ $p(\text{AIS } 3+) = \frac{1}{1 + e^{(6.047 - 5.44Nij)}}$	0.39	0.85	-	-
Neck	F _{Shear} [kN]			-	-	1.9	3.1
	FTension [kN]			-	-	2.7	3.3
	M _{Extension} [Nm]			-	-	42	57
Chest	Multi-point Thoracic Injury Criterion R _{max} (mm)	$\begin{array}{c} max(UL_{max}, UR_{max}, LL_{max}, LR_{max}) \\ \qquad $	$p(AIS 3+) = 1 - e^{-\left(\frac{R_{max}}{58.183}\right)^{2.977}}$	37.9	52.3	35	60
Abdo- men	Compression δ _{max} (mm)	max(δL,δR): Peak X-axis deflection of the [left / right] abdomen	$p(\text{AIS 3+}) = 1 - e^{-\left(\frac{\delta_{max}}{106.222}\right)^{43127}}$	-	88.6	-	88
Pelvis	res. Actetabulum Load F _R (kN)	$\sqrt{F_x^2 + F_y^2 + F_z^2}$	$p(Hip fracture) = \Phi \left[\frac{\ln 1.429 F_{AR} - 1.5751}{0.2339} \right]$	2.583	3.486	3.28	4.1
Femur	Axial Load Fz (kN)	-	$p(\text{AIS } 2+) = \Phi\left[\frac{\ln(1.299F_{LC}) - 2.62}{0.3014}\right]$	5.331	8.588	3.8	9.07
	F _{z,upper} (kN)	-	$p(\text{AIS } 2+) = \frac{1}{1 + e^{(5.7415 - 0.8189F_{upper tibis})}}$	4.235	5.577	- ²	- 2
Tibia	F _{z,lower} (kN)		$p(\text{AIS 2+}) = \frac{1}{1 + e^{(3.7544 - 0.4683F_{lower tibla})}}$	3.573	5.861	- 2	_ 2
	Mres (Nm)	Request for Comments published in Janua	$p(\text{AIS } 2+) = 1 - e^{-e^{\left(\frac{\ln RT I - 0.3376}{0.3213}\right)}}$	178	240	- 2	- ²

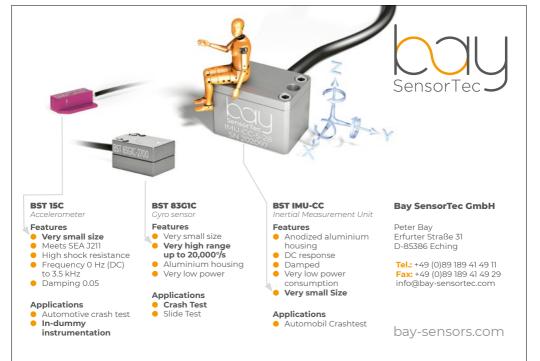
¹ as proposed in NHTSA's Request for Comments published in January 2017

 $^{\rm 2}$ $\,$ Euro NCAP uses the lower leg of the Hybrid III dummy

Euro NCAP Assessment Protocol 9.1.2

³ Source: Craig et al.: Injury Criteria for the THOR 50th Male ATD., NHTSA, September 2020







Dummy | Crash Test Wissen



Dummies: Weights, Dimensions and Calibration

Adult Dummies for Frontal / Rear Impact



	Weight (kg)	Seating Height (cm)	Instruction for Calibration
THOR 50 % Male	76.7	90.7	THOR 50th Percentile Male (THOR- 50M) Qualification Procedures Manu- al, September 2018 (NHTSA)
THOR 5 % Female	46.9	81.3	
Hybrid II 50 % Male	74.4	90.7	CFR 49 Part 572, Subpart B
Hybrid III 5 % Female	49.1	78.7	SAE J2862, J2878 CFR 49 Part 572, Subpart O
Hybrid III 50 % Male	77.7	88.4	SAE J2779, J2876 CFR 49 Part 572, Subpart E 1999/98/EC
Hybrid III 95 % Male	101.3	91.9	SAE J2860
BioRID II	77.7	88.4	User Manual

Adult Dummies for Side Impact



	Weight (kg)	Seating Height (cm)	Instruction for Calibration		
Eurosid 1	72.0	90.4	Eurosid 1 Certification Procedure 1996/27/EC, UN R95		
ES-2	72.0	90.9	FTSS- User Manual / UN R95		
ES-2 re	72.4	90.9	CFR 49 Part 572, Subpart U		
US-SID	76.7	89.9	CFR 49 Part 572, Subpart F		
US-SID/Sid-H3	77.2	89.9	CFR 49 Part 572, Subpart M		
SID IIs	44.12	78.0	CFR 49 Part 572, Subpart V		
WorldSID 5 % Female	48.27		User Manual		
WorldSID 50 % Male	73.91	86.9	User Manual		

Child Dummies



>			
	Weight (kg)	Seating Height (cm)	Instruction for Calibration
P0. P¾. P6. P10	3.4 - 32.0	34.5 - 72.5	User Manual
P3	15.0	56.0	User Manual
P1½	11.0	49.5	P1½ User Manual
Q1	9.6	47.9	Q1 User Manual
Q1½	11.1	49.9	Q1.5 User Manual
Q3	14.5	54.4	Q3 User Manual
Q3s	14.5	56.6	CFR 49 Part 572, Subpart W
Q6	23.0	63.6	Q6 User Manual
Q10	35.5	73.4	Q10 User Manual (Rev. A Draft)
CRABI 12 m	10.0	46.4	CFR 49 Part 572, Subpart R
Hybrid II - 3 y/o	15.1	57.2	CFR 49 Part 572, Subpart C
Hybrid II - 6 y/o	21.5	64.5	CFR 49 Part 572, Subpart I
Hybrid III - 3 y/o	16.19	54.6	CFR 49 Part 572, Subpart P
Hybrid III - 6 y/o	23.4	63.5	CFR 49 Part 572, Subpart N
Hybrid III - 6 y/o - weighted	27.92	64.06 - 66.6	CFR 49 Part 572, Subpart S
Hybrid III - 10 y/o	35.2	71.6	CFR 49 Part 572, Subpart T

in Cooperation with BGS Böhme & Gehring GmbH





Dummy-Trainings

Seminars by our Partner BGS Böhme & Gehring GmbH

DUMMY	Hybrid III 5 %, 50 %, 95 %
DATE	0405.10.2021
ID	707/3480
PRICE	1.590,- EUR each
DUMMY	THOR
DATE	2224.11.2021
ID	721/3848
PRICE	2.450,- EUR each
DUMMY	BioRID II
DATE	2628.10.2021
ID	708/3843
PRICE	1.590,- EUR each
DUMMY	WorldSID 50 %
DATE	1516.11.2021
ID _	718/3847
PRICE	1.750,- EUR each
DUMMY	ES-2 / ES-2re
DATE	0203.11.2021
ID _	709/3845
PRICE	1.590,- EUR each
DUMMY	SID IIs
DATE	1011.11.2021
ID _	710/3847
PRICE	1.590,- EUR each
DUMMY	P- / Q-Child Dummy
DATE	08.10.2021
ID _	711/3842
PRICE	875,- EUR each
DUMMY	Q6/Q10
DATE	08.11.2021
ID _	720/3844
PRICE	875,- EUR each
DUMMY	Hybrid III 3 and 6 y/o
DATE	07.10.2021
ID _	712/3841
PRICE	875,- EUR each
VENUE	Bergisch Gladbach
LANGUAGE	

Course Description

The seminars give you the opportunity to gain efficiency and security in the use and handling of dummies.

After a short theoretical introduction you are going to be trained in the handling of the respective dummy-type in a dummy lab in practical exercises in work groups.

Course Contents

- Introduction of the respective dummy-type History, development, assemblies, standard instruments, optional measuring points, recent modifications, regulations for application/test, calibration
- Complete disassembly of the dummies in work groups Explanation of the functions of the assemblies and the individual parts, special features, deviations from other dummy-types, practical hints for the handling of individual assemblies, sensors and cabling, special tools, other devices, cleaning
- Complete assembly of the dummies in work groups work steps, possible assembly errors, mounting of the sensors, cabling, adjustments of joints, storing / transport
- Dummy calibration Demonstration and explanation of the calibration tests

Course Objectives

- Efficiency and security in use and handling of dummies
- Exact knowledge about assembly, mechanics and sensor positions
- Understanding of the measuring possibilities and limits

Who should attend?

Project and test engineers, technicians, mechanics







DUMMY	SID IIs
DATE	1011.11.2021
ID	710/3847
PRICE	1.590,- EUR each
DUMMY	P-/Q-Child Dummy
DATE	08.10.2021
ID	711/3842
PRICE	875,- EUR each
DUMMY	Q6 / Q10
DATE	08.11.2021
ID	720/3844
PRICE	875,- EUR each
DUMMY	Hybrid III 3 and 6 y/o
DATE	07.10.2021
ID	712/3841
PRICE	875,- EUR each
VENUE	Bergisch Gladbach
LANGUAGE	



Dummy Specialists, BGS Böhme & Gehring GmbH

BGS operates the dummy calibration laboratory of the German Federal Highway Research Institute (BASt). BGS calibrates crash test dummies for the automotive industry. The seminars are held by experienced engineers from BGS' team.





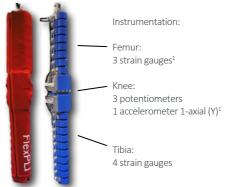
Impactors for Pedestrian Protection

advanced Pedestrian Legform Impactor: aPLI



Length	Total Mass.	Upper Body Mass
1096 mm	24.7 kg	11.3 kg

Flexible Pedestrian Legform Impactor: Flex PLI

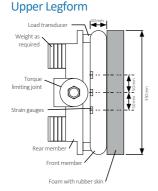


Injury Criteria

Criterion		
Tibia Bending Moment		
MCL Elongation		
ACL / PCL Elongation		

Length	Diameter	Mass
975 mm	132 - 140 mm	13.4 kg

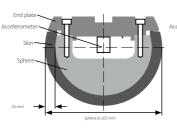
¹ not assessed

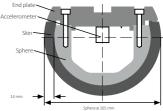


Length	Width	Mass	
350 mm	~ 155 mm	11 - 18 kg	Adult I

Adult Headform Impactor

Child Headform Impactor



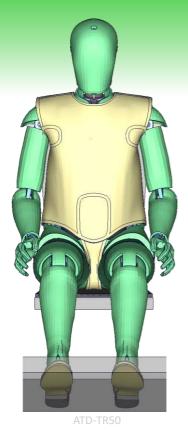


SafetyWissen by

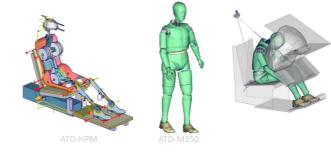
	Diameter	Mass		Diameter	Mass
Adult Headform	165 mm	4.5 kg	Child Headform	165 mm	3.5 kg

more on pedestrian protection \bigcirc page 96

in Cooperation with BGS Böhme & Gehring GmbH



ATD P MODELS FE - Dymmy Solutions



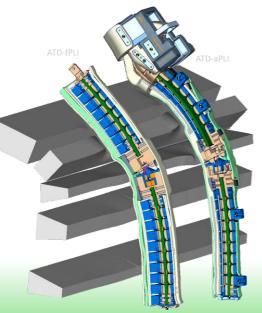
ATD - Hybrid III and THOR Dummy Models and Leg Impactor Models

- Well recognized technology supplier
- Wide range of OEMs and supplier costumers worldwide
- Specialized in development, distribution and support of high quality finite element models
- Codes: LS-Dyna, PamCrash, Abaqus, Radioss
- 2021 new releases:

ATD-TR50 (THOR-50M) ATD-fPLI (FlexPLI) ATD-aPLI SBL-B (aPLI, new hardware version)

Always developing new models - get in touch!







Dummy | Crash Test Seminar



Seminars by our Partner BGS Böhme & Gehring GmbH

Pedestrian Protection - Test Procedures

Course Description

A basic prerequisite for successful implementation of pedestrian protection is a detailed knowledge of test requirements. This seminar provides the complete knowledge regarding the test methods as defined by the EU regulation on pedestrian protection and Euro NCAP's pedestrian protection assessment in theory and praxis.

Compact presentations explain the basics and technical details of the regulation and the test protocols. Practical exercises the BASt's test laboratory include test preparation, vehicle marking, selection of test points, handling of the impactors and the actual testing with head and legform impactors.

Course Contents

Basics and current status of the regulations (presentations)

- Euro NCAP Rating (presentation)
- Test preparation according to Euro NCAP testing protocol and EU regulation (practical exercises)
- Test demonstrations: Head, Upper Legform and Legform impact (demonstrations and practical exercises)
- Discussion

Who should attend?

- Project, test and simulation engineers, .
- Technicians, mechanics -

ates	DATE	2123.09.2021
Dat	COURSE ID	713/3856
	VENUE	Bergisch Gladbach
	PRICE	2.250,- EUR each
	LANGUAGE	

Pedestrian Protection Workshop: aPLI NEW

Course Objectives

- Detailed Knowledge of the new Impactor
- Experience with Handling and Usage of the Impactor
- Understanding of the Impactor's Functionality

Course Contents

- History, Biomechanics, Evaluation, Legislation
- Assembly, Transducers, Onboard Data Acquisition, . Technical Details
- Disassembly along with Comments on Function of Components
- Assembly along with practical Tips and Pointers to . Specialities and possible Mistakes

- Adjustments of the Compound Springs, Clamping Bolts, Stopper Cables, etc.
- Demonstration of both Certification Procedures
- Data Analysis and Interpretation of Test Results

Who should attend?

- Project, test and simulation engineers,
- Technicians, mechanics

fes	DATE	1609.2021
Dates	COURSE ID	765/3859
	VENUE	Bergisch Gladbach
	PRICE	975,- EUR each
	LANGUAGE	

Pedestrian Protection Workshop: Vehicle Mark-Up

Course Objectives

- Experience with the new Vehicle Markup
- Certainty in its Application н.
- Deep Understanding of the Procedure

Course Contents

- Basics, Background and Development of the Procedure
- Test Area Determination, Borders, Exemption Zones, Special Cases
- Necessary Laboratory Equipment, Helpful Tools
- Exemplification by a complete Mark-up of a Vehicle
- Color Scheme, Manufacturers Predictions, allowed Tolerances

- Default Green / Default Red Definitions
- Result Analysis, Point Assessment
- Adaption of the Principle to Upper- and Lowerleg Areas

Who should attend?

- Project, test and simulation engineers,
- Technicians, mechanics

fes	DATE	1309.2021
Dates	COURSE ID	716/3858
	VENUE	Bergisch Gladbach
	PRICE	975,- EUR each
	LANGUAGE	



Active Safety | AD Seminar







Introduction to Active Safety of Vehicles

Course Description

Increasing demands on the protection of vehicle occupants have led to a continuous reduction in the number of injured and killed persons. While more than 20,000 persons have been killed on German roads in the early 1970s, this number is now just over 3,000. Passive safety, i.e. measures which are designed to minimize the consequences of an accident, has made a significant contribution to this achievement.

While the potential of passive safety is considered to be largely exhausted and huge efforts are required to achieve further progress in occupant protection, active safety has become increasingly important in recent years. Active Safety means measures which prevent an accident or at least reduce the collision speed and thus the energy input.

While technologies such as ABS or ESC have been established years ago and have proven their effectiveness, new techniques such as the emergency brake or the lane keeping assist and numerous other driver assistance systems are just entering the market. It can be assumed that these systems will be widely used in the next few years and will lead to a further decrease in the number of traffic victims.

Automated driving can be seen as the next step of active safety. Although there is still a lot of development needed in this area, it can be assumed that vehicles which will driven at least partially automatically in certain traffic scenarios will enter the market over the next ten years.

In the seminar first a brief introduction to active safety, in contrast to passive safety is given. This is followed by a presentation of current active safety systems and an overview of the requirements of legislation and consumer protection organizations. In addition, current and upcoming developments in the area of driver assistance systems and automated driving are presented.

Who should attend?

The seminar is aimed at new and experienced engineers working in the field of active vehicle safety in research and development departments of automotive OEMs or suppliers, as well as for all other interested parties, which want to receive an overview of current and future developments in the areas of active vehicle safety, driver assistance and automated driving.

Course Contents

- Fundamentals of active safety
 - Basic principles of action
 - Legal requirements
 - Euro NCAP requirements
- Current active safety systems
 - ABS
 - ESC
 - Brake assist
 - Pre-crash systems
- Driver assistance systems
 - Basic requirements and design strategies
 - Current and future driver assistance systems
 - Automated driving
 - State of the art
 - Opportunities and risks
 - Human machine interface
 - Market introduction strategies



Dr. Gerd Müller (Technical University Berlin) has been working at the department automotive technology of the Technical University of Berlin since 2007. From 2007 to 2015 he was a research assistant. Since 2015 he has been a senior engineer of the same department. His research focuses on vehicle safety and friction coefficient estimation. Dr. Müller gives the lecture "Fundamentals of Automotive Engineering" and conducts parts of the integrated course "Driver Assistance Systems and Active Safety".

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	2629.04.2021	51/3815	Online	4 Days	790,- EUR till 29.03.2021, thereafter 940,- EUR	
	11.11.2021	51/3765	Alzenau	1 Day	790,- EUR till 14.10.2021, thereafter 940,- EUR	





Active Safety | AD
 Wissen
 UPDATE



NCAP Tests for Active Safety and Driver Assistance

Occupant Status Monif Driver Status Monitoring Seat Belt Reminder (SBF	toring (OSM)		Total	_	
Driver Status Monitorin				3	00
	J (DSM)		Total		00
	R) on rear seats (n = number of rear s	eating positions)			er seat
SBR on rear seats with c	occupant detection (n = number of re	. ,			er seat
	· ·	ar seating positions,			
Speed Assist Systems (S	SAS)	_	Total Basic SLIE	3. 0.50	00
			Advanced SLIF	0.50	
Speed Limit Informa-					1.50
tion Function (SEIF)					
		Speed Lim	-	0.23	
Creard Control		•	· · ·	1 25	
•					1.50
Tunction					
		more ⊃ page 15	5 Total		00
					0.50
	1 01 ,	Single lane mark	ing		
· · · · · · · · · · · · · · · · · · ·		-	-		0.50
	Solid line	-	-	0.25	
			U	0.25	
	Road Edga				
Francisco	Noad Edge				
					3.00
Keeping (LLK)	solid line				
		-			
	0	,			
	-	,	Tetel	6	00
AEB Car-to-Car	more ⊃ page 152		Iotal	6.	00
AEB VRU: max. 18 P	oints (as part of the VRU Protecti	on assessment)	nore 🗢 page 143		
AEB City (as part of t	he Adult Occupant Protection ass	essment): 3 Points			
AEB VRU (as part of	the Pedestrian Protection assessm	nent): 12 Points			
Seat Belt Reminder:	10 Points				
 Speed Assistance Sy 	stems: 3 Points			in just 2	days with
	Points				
ESC: 15 Points					
 Lane Support Syster 				tings	
Blind Spot Detection	n: 3 Points more 🗢 page 55	learn more	on V page 157		
afety Assist Technolo	gy (SAT) Assessment 2021 - 202	5			
Weighting: 20 % of the	overall rating)				
 Effective Braking 	& Avoidance (EBA): ABS / ESC: 6 P	oints			
 Seat Belt Remind 	er Driver / Passenger (with seat oc	cupancy detector)	/ rear seats: 6 Points		
AEB: 6 Points					
 Advanced SAT: 2 	Points				
	systems are assessed in the Moto	orcyclist Safety box	(
more 🗢 page 59					
	tion Function (SLIF) Speed Control Function Lane Support Systems (Human Machine Interface (HMI) Lane Keep Assist (IKA) Emergency Lane Keeping (ELK) AEB Car-to-Car AEB VRU: max. 18 P AEB City (as part of t AEB VRU (as part of t AEB Inter-Urban: 9 F ESC: 15 Points Lane Support Syster Blind Spot Detectior afety Assist Technolo Weighting: 20 % of the Effective Braking Seat Belt Remind AEB: 6 Points Advanced SAT: 2 more assistance	tion Function (SLIF) Speed Control Function Intelligent Lane Support Systems (LSS) Human Machine Interface (HMI) Lane Departure Warning (LDW) Interface (HMI) Blind Spot Monitoring (BSM) Lane Keep Assist Dashed Line (LKA) Solid line Road Edge Road Edge Emergency Lane solid line Noncoming vehicle Overtaking vehicle Overtaking vehicle Overtaking vehicle AEB Car-to-Car more \bigcirc page 152 AEB Carty (as part of the Adult Occupant Protection assessment Seat Belt Reminder: 10 Points Speed Assistance Systems: 3 Points AEB Inter-Urban: 9 Points ESC: 15 Points Lane Support Systems: 3 Points East Set Technology (SAT) Assessment 2021 - 202 Weighting: 20 % of the overall rating) Effective Braking & Avoidance (EBA): ABS / ESC: 6 P Seat Belt Reminder Driver / Passenger (with seat occols AEB: 6 Points Actarts: 6 Points Advanced SAT: 2 Points Tore assessed in the Motor	Tion Function (SLIF) Speed Lim Speed Control Function Function Intelligent Speed Assist (ISA) a Lane Support Systems (LSS) more 2 page 15' Human Machine Interface (HMI) Lane Departure Warning (LDW) Blind Spot Monitoring (BSM) Jashed Line Lane Keep Assist Dashed Line Solid line Single lane mark Centreline no line Road Edge dashed dashed dashed Solid line Single lane mark Oncoming vehicle Fully marked lan Overtaking vehicle Fully marked lan NCAP - Ne Speed Assistance Systems: 3 Points AEB Car-to-Car more 2 page 152 AEB Chty (as part of the Adult Occupant Protection assessment): 12 Points Seat Belt Reminder: 10 Points Get familia Speed Assistance Systems: 3 Points More 2 page 55 <t< th=""><th>tion Function (SLIF) System Accuracy Warning Function Speed Limitation Function (SLF) Speed Control For cars without SLF Function For cars without SLF Function For cars without SLF Intelligent Speed Assist (ISA) and/or intelligent ACC Lane Support Systems (LSS) more \bigcirc page 155 Total Human Machine Interface (INNI) Lane Departure Warning (LDW) Blind Spot Monitoring (BSM) Lane Keep Assist Dashed Line Solid line Single lane marking Centreline Road Edge no line no line dashed no line dashed solid line Solid line Single lane marking Oncoming vehicle Fully marked lanes Orcarking vehicle Fully marked lanes Orcarking vehicle Fully marked lanes Orcertaking vehicle Fully marked lanes Orcer to the Adult Occupant Protection assessment): I 2 Points AEB Car-to-Car more \bigcirc page 152 AEB VRU (as part of the Pedestrian Protection assessment): I 2 Points Seat Belt Reminder: 10 Points</th><th>tion Function (SLIF) System Accuracy 0.25 Speed Control Function Speed Limitation Function (SLF) 0.25 Speed Control Function For cars without SLIF 1.25 For cars without SLIF 0.75 Intelligent Speed Assist (ISA) and/or intelligent ACC 1.50 Lane Support Systems (LSS) more 2 page 155 Total 4. Human Machine Interface (HMI) Lane Departure Warning (LDW) 0.25 Lane Keep Assist Dashed Line Single Iane marking 0.25 Solid line Single Iane marking 0.25 Solid line Single Iane marking 0.25 Road Edge no line no line 0.25 Solid line Single Iane marking 0.25 solid line Single Iane marking 0.25 Solid line Solid line 0.25 solid line Solid line 0.25 solid line Solid line Solid line 0.25 oncoming vehicle Fully marked Ianes 1.00 Overtaking vehicle Fully marked Ianes 1.00 Overtaking vehicle Fully marked Ianes 1.50</th></t<>	tion Function (SLIF) System Accuracy Warning Function Speed Limitation Function (SLF) Speed Control For cars without SLF Function For cars without SLF Function For cars without SLF Intelligent Speed Assist (ISA) and/or intelligent ACC Lane Support Systems (LSS) more \bigcirc page 155 Total Human Machine Interface (INNI) Lane Departure Warning (LDW) Blind Spot Monitoring (BSM) Lane Keep Assist Dashed Line Solid line Single lane marking Centreline Road Edge no line no line dashed no line dashed solid line Solid line Single lane marking Oncoming vehicle Fully marked lanes Orcarking vehicle Fully marked lanes Orcarking vehicle Fully marked lanes Orcertaking vehicle Fully marked lanes Orcer to the Adult Occupant Protection assessment): I 2 Points AEB Car-to-Car more \bigcirc page 152 AEB VRU (as part of the Pedestrian Protection assessment): I 2 Points Seat Belt Reminder: 10 Points	tion Function (SLIF) System Accuracy 0.25 Speed Control Function Speed Limitation Function (SLF) 0.25 Speed Control Function For cars without SLIF 1.25 For cars without SLIF 0.75 Intelligent Speed Assist (ISA) and/or intelligent ACC 1.50 Lane Support Systems (LSS) more 2 page 155 Total 4. Human Machine Interface (HMI) Lane Departure Warning (LDW) 0.25 Lane Keep Assist Dashed Line Single Iane marking 0.25 Solid line Single Iane marking 0.25 Solid line Single Iane marking 0.25 Road Edge no line no line 0.25 Solid line Single Iane marking 0.25 solid line Single Iane marking 0.25 Solid line Solid line 0.25 solid line Solid line 0.25 solid line Solid line Solid line 0.25 oncoming vehicle Fully marked Ianes 1.00 Overtaking vehicle Fully marked Ianes 1.00 Overtaking vehicle Fully marked Ianes 1.50

ACTIVE SAFETY Solutions for all ADAS and AV Test Scenarios

Ultra-Flat Overrunable Robot Platform

- > Up to 100kph real-world testing
- > Enhanced synchronization for superior accuracy
- > 100% waterproof for easy maintenance
- > Introducing UFOnano for pedestrian testing

Driving Robot

- > Complimentary to UFO to simulate complex test scenarios
- > Shares the same operator software & HMI
- > Full synchronization between systems to VUT
- > Ultra compact design; OEM steering remains intact









Driving Robot

Swappable Batteries



Anti-Lock Braking System

Alternative Trajectory

humaneticsatd.com





Active Safety | AD Wissen



NCAP Tests for Active Safety and Driver Assistance

	planned: Crash Avoidance Rating consisting of		
	I OI WATU CONISION WATTING. IO FOILIG	Planned Cra	sh Avoidance Rating
	 Crash Imminent Braking: 12 Points more ⊃ page 159 Dynamic Brake Support: 8 Points 	Stars	required points
	 Dynamic Brake Support: 8 Points Low Beam Headlighting: 20 Points 	Stars	(out of 100)
	 Semi-automatic Headlight Beam Switching: 10 Points 		
	 Amber rear Turn Signal: 5 Points 	****	80
	 Lane Departure Warning: 12 Points 	****	60
	Blind Spot Detection: 5 Points	***	40
AP	Assessment of the risk for rollover (Static Stability Factor SSF): 18 Points	**	20
NC	Additionally as part of the pedestrian safety assessment: AEB Pedestrian		
U.S. NCAP	■ Rear Auto Braking more ⊃ page 160	*	0
_			
	■ AEB Car-to-Car more ⊃ page 158 (part of the Top Safety Pick rating mor	e 🗢 page 51 🌖	
	 approach to standing vehicle at 20 km/h and 40 km/h assessment of the speed reduction 		
	 1 additional point for FCW (Forward Collision Warning) meeting the U.S. NCAP cri 	teria	
	■ AEB Pedestrian more ⊃ page 158 (part of the Top Safety Pick rating mo	re ⊃ nage 51 _)	
	 3 scenarios: adult nearside, child nearside obstructed, adult longitunial 		
	 assessment of the speed reduction 		
	 1 additional point for FCW (Forward Collision Warning) 		
	■ Advanced Lighting (part of the Top Safety Pick rating more ⊃ page 51)		
IIHS	 Assessment of the illumination and glare of high and low beam headlights in vario systems that automatically switch between high and low beam. 	ous test scenarios.	Additional credit is given for
_		ts for adv. safet	y systems 2019
	SBR: 4 Points		32
		strian (day) strian (night w/	illumination) 25
		strian (night w/c	
	LSS Bost View	Monitor	16
P	 ASV+ Award for cars achieving ≥ 12 Points ASV++ Award for cars achieving ≥ 46 Points Headlight: 		5
INCAP	■ ASV+++ Award for cars achieving ≥ 86 Points Pedal Mise	application	2
			max. total 141
	 Rollover assessment based on SSF like in U.S. NCAP: 5 Points Braking Performance Tests: Measurement of the stopping distance from 1 	00 km/h on dry	and wet road. Check if
	vehicle stays within the 3.5 m wide track while braking: 5 Points		
	Basic Active Devices:		
	FCW, LDW, SLD, SBR front, SBR rear: 0.5 Points each		
	 AEB Inter-Urban: 1 Points AEB City: 1.5 Points 		
AP	 Additional Active Devices (optional): Max. total points for Additional Active 	e Devices = 2 Po	ints
KNCAP	 ASCC, BSD, RCTA, LKA, ISA: 0.5 Points each 		
×	 AEB Pedestrian, Advanced Airbag: 1 Point each 		
	Active Safety Assessment based on Management Regulation 2021 (valid from	1/2022) more	page 161 (Weighting:
	25 % of the overall rating): more ⊃ page 63		
	ESC: 8 Points		
	AEB Car to Car Rear: 11 Points, AEB Car to Pedestrian: 10 Points, AEB Car	to Two-wheeler	: 11 Points
	 LKA: 3 Points HMI: 6 Points 		
٩.	 Optional Systems: Lane Departure Warning: 2 Points, Speed Assistance Sy 	stem 2 Points	Blind Spot Detection (Car
C-NCAP	to Car, Car to Two-wheeler): 5 Points		
С-	 Headlights: 10 Points 		

DEKRA Technology Center

DEKRA



Areas of responsibility:

- > Accreditation as a Testing Laboratory according to ISO 17025 (DAkkS)
- > 540 ha proving ground for automated and connected mobility
- > FIA Test Laboratory for motorsport safety
- > Designation as a Technical Service for type approval in: Germany, Netherlands, Ireland, Sweden, Luxembourg
- > Recognition as Testing Lab in Japan, Taiwan, Australia and Brasil
- > Information management system according to TISAX

DEKRA Technology Center Senftenberger Straße 30 01998 Klettwitz Telephone: 035754.7344-500 datc@dekra.com www.dekra-lausitzring.de www.datc.de





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 UPDATE



NCAP Assistance System Rating Matrix

	Euro NCAP / ANCAP	U.S. NCAP	SHII	Latin NCAP	ASEAN NCAP	C-NCAP	C-IASI	JNCAP	KNCAP
SBR Seat Belt Reminder									
OSM / DSM Occupant/Driver Status Monitoring									
COPD Child Occupant Presence Detection	•								
ABS Anti-Lock Braking System									
ESC Electronic Stability Control									
MCB Multi Collision Brake									
SAS Speed Assistance System									
LSS Lane Support Systems									
BSM Blind Spot Monitoring									
AEB CCR Car to Car Rear						٠			
AEB Tap Turn across path								•	
AEB Pedestrian									
AEB Reverse Pedestrian									
AEB Cyclist									
AEB PTW Powered Two Wheeler	•								
FCW Forward Collision Warning									
DBS Dynamic Brake Support									
AES Autonomous Emergency Steering									
Emergency Call									
Rear View Monitor									
Rear Cross Traffic Alert									
Headlights									
Pedal Misapplication									
• 2021 • 2022 • 2022									

• 2021 • 2022 • 2023











Advances in Sensors for Automated Driving

Course Description

The seminar addresses the crucial importance of surround sensors for safe and reliable automated driving.

After an introduction into the target scenarios and key technologies of automated and autonomous driving, challenges, technology gaps and system limits are discussed.

In recent years, the performance and capabilities of RaDAR, cameras, LiDAR and Ultrasonic sensors have been significantly improved and enhanced. Ultimately, the robustness and classification reliability needed for Level 4 full automated driving shall be achieved by sensor fusion and redundancies, utilizing artificial intelligence.

Step-by-step, state of the art and new advanced sensor technologies will be discussed:

- RaDAR: 3D-Phased Array Scanning, Digital Beam Control, Micro-Doppler-Effect,
- LASER Cross-Array Scanning,
- 3D-Solid State LiDAR, Vertical Cavity Surface Emitting LASER (VCSEL),
- Single-Photon-Avalanche Diodes (SPAD),
- Cameras: Digital Image Processing utilizing neuronal networks (deep learning),
- Sensor-fusion and redundancies,
- RaDAR, LiDAR and camera based road signature,
- Self-localization and matching (SLAM),
- High definition maps and communication systems,
- Artificial intelligence (deep learning, reinforcement learning),
- Driver vigilance monitoring.

Who should attend?

The seminar addresses all engineers, technicians and experts working in the development, application and research of automated driving systems and vehicle safety. Over and above, the seminar may be interesting and useful to all experts in traffic safety and planning, marketing and industrial engineering. Basically, all experts somehow dealing with automated driving and vehicle safety being interested in current and future sensor technologies are very welcome.

Course Contents

- Scenarios and technologies of automated driving
- Legislation status and legal requirements
- System limits, gaps and challenges
- State of the art and advances of utilized sensors
- Operating safety
- Use of intelligent algorithms and artificial intelligence



nstructo

Dr. Lothar Groesch (Groesch Automotive Safety Consulting) has been working in vehicle safety for more than 40 years, both in passive (crash sensing and electronics, occupant protection) and in active safety (surround sensors, accident avoidance). After working for 18 years for a leading OEM in vehicle safety, his experience was significantly enhanced by working for another 16 years in automotive safety sensors and electronics at a leading automotive supplier. Working as a Product Director for Automotive Safety Systems in the US from 2000 through 2009, he is particularly familiar with the specific requirements of the US market, legislation and product liability. Since 2009, Dr. Groesch has been doing consulting business under the name Automotive Safety Consulting, with the focus on stereo-vision, Radar-application and functional safety. Last but not least, he is teaching at several universities and conducting numerous seminars about Automotive Safety Safety, Driver Assistance and Automated Driving and Safety Sensors.

Ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	1215.04.2021	178/3836	Online	3 Days	1.340,- EUR till 16.03.2021, thereafter 1.590,- EUR	
	0709.09.2021	178/3837	Online	3 Days	1.340,- EUR till 10.08.2021, thereafter 1.590,- EUR	





SAFETYASSIST



The requirements by New Car Assessment Programs regarding safety-supporting driver assistance systems for passenger cars are constantly increasing: Oncoming traffic scenarios, tests in darkness and higher expected speed reductions are some of the prerequisites for a 5-star rating in the Euro NCAP or an IIHS Top Safety Pick.

The introduction of emergency brake assistants for passenger cars is being driven forward by legislation: From 2022 they will be mandatory for passenger cars. The details for proof of cyclist recognition are still being discussed, all other test conditions have already been decided. The lane departure warning functions have also been incorporated into UN R 79.03.

At the **Praxis Conference Safety Assist**, the boundary conditions relevant for development will be presented: Requirements, technical principles and development and release methods on the theory day in the conference hotel, followed by hands-on experience on the test track on the Demo Day. Various test scenarios will be performed and examples of how the test technology can be used will be shown live in the test setup.





This is what awaits you:

- The presentation of current and future requirements on emergency braking, evasion and highly automated driving functions, as well as development strategies that lead to a robust system.
- Face to face talk with the people who set the framework for the development of safety assist functions: Legislative representatives, consumer protection organizations, OEM representatives and suppliers of simulation and testing technologies.
- Practical experience with various test setups, targets, driving robots and control software on the Demo Day.

DATE VENUE HOMPAGE LANGUAGE September.2021 to be announced, GERMANY www.carhs.de/safetyassist German with translation into English Who should attend?

The Praxis Conference Safety Assist addresses everyone, who works in the field of safety-related driver assistance systems. The Praxis Conference is the right place to broaden and deepen your network: You will meet key players in development, system integration, regulation and verification of Safety Assist Systems.





Active Safety | AD Seminar





Briefing on the Worldwide Status of Automated Vehicle Policies

Course Description

Regardless of the hype surrounding "self-driving cars", it is clear that automated driving systems (ADS) will fundamentally change the automotive industry. Moreover, despite widespread expectations that ADS hold the key to achieving substantial reductions in road crashes, injuries, and deaths, these systems also raise concerns among safety authorities. The validation of ADS requires long-duration testing and development to ensure correct behavior under massively variable road conditions. Conventional regulatory methods developed over the past half-century lack methods and tools to assess such performance, forcing safety authorities to look for new ways to ensure that ADS will be safe for public use.

Course Objectives

This seminar reviews current efforts to adapt regulatory systems to meet this challenge, including the vigorous debates over strategies and methods and the roles of regulators and manufacturers in ensuring the safety of automated vehicles.

Who should attend?

The briefing is aimed at employees from the development departments of vehicle manufacturers and suppliers working in the field of automated driving and vehicles equipped with automated driving systems. Given the risks of misuse, it is particularly important for all employees in product strategy and marketing departments.

Course Contents

- Safety authority expectations for automated vehicle safety
- Role and influence of manufacturers on regulatory thinking
- Pressures on current regulatory methods and tools
- Pressure on type approval for near-term framework
- Guidance versus regulation: How and when?
- Hybridization: Merging of self-certification and type approval
- Levels of automation from a regulatory perspective
- Current efforts to establish automated vehicle regulations
- Outlook: Can regulations ensure automated vehicle safety?





John Creamer (GlobalAutoRegs.com) is the founder of GlobalAutoRegs.com and a partner in The Potomac Alliance, a Washington-based international regulatory affairs consultancy. In his client advisory role, Mr. Creamer is regularly involved with meetings of the UN World Forum for the Harmonization of Vehicle Regulations (WP.29). Previously, he has held positions with the US International Trade Commission and the Motor & Equipment Manufacturers Association (representing the US automotive supplier industry), as the representative of the US auto parts industry in Japan, and with TRW Inc. (a leading global automotive safety systems supplier).

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	0711.06.2021	184/3743	Online	5 Days	790,- EUR till 10.05.2021, thereafter 940,- EUR	
	14.10.2021	184/3742	Alzenau	1 Day	790,- EUR till 16.09.2021, thereafter 940,- EUR	

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Levels of Driving Automation according to BASt, SAE and NHTSA Definitions

						Execution of Steering and Acceleration/ Deceleration
						Monitoring of Driving Environment
						Fallback Performance of Dynamic Driving Task
All driving modes	Some driving modes	Some driving modes	Some driving modes	Some driving modes	1	System Capability
	Fully automated	Highly automated	Partially automated	Assisted	Driver only	BASt Level
5 Full automation	4 High automation	3 Conditional automation	2 Partial automation	1 Driver assistance	0 No automation	SAE Level
automation / Full self driving automation	3/4 Limited self driving	3 Limited self driving automation	2 Combined function automation	1 Functionspecific automation	0 No automation	NHTSA Level



😽 Auto[nom]Mobil

The Experts' Dialogue

Automated Driving and Safety

The hype about what is often called autonomous driving is increasingly giving way to reality. In recent years, even the greatest visionaries have realized that many questions still have to be answered, many barriers overcome and many challenges mastered in order to implement vehicle automation.

However, especially in times of the current crisis, it has become all the more clear that mobility must be regarded as one of the most fundamental basic needs, and mobility for all means that we must work on vehicle automation with full commitment.

In the Auto[nom]Mobil session of the carhs.training SafetyWeek, fundamental and crosscompetitive necessities for achieving goals will be addressed and possible solutions will be presented. This expert dialogue provides the platform for an intensive exchange and is intended to accelerate the essential stronger networking of the participants.

Safe Urban Mobility

Mobility creates Quality of Life

It is a prerequisite for business and commerce, but also for personal encounters. Urban mobility, however, is increasingly coming across to their limits.

There is a threat of traffic collapse. Increasing urbanization is accelerating this trend. Individual mobility is being supplemented or even replaced by new traffic concepts based on autonomous shuttles.

Are these Shuttles safe?

How do they protect their passengers and how do they protect external road users? Auto[nom]Mobil brings the protagonists of the new mobility together with the experts for vehicle safety and shows ways in which autonomous urban mobility becomes safe for all concerned.







VENUE HOMPAGE LANGUAGE PRICE

DATE



01.-02.09.2021

Würzburg, GERMANY & ONLINE

1.490,- EUR till 22.01.2021, thereafter 1.750,- EUR, ONLINE 990,- EUR





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Event









Active Safety | AD
 Seminar



Introduction to Artificial Intelligence and Machine Learning for Advanced Driver Assistance Systems and Automated Driving Functions

Course Description

The functions of automated driving - no matter what degree of automation - usually require the application of modern artificial intelligence techniques in order to be able to realize the desired functionalities at all. The aim of this seminar is to present the basic methods of Artificial Intelligence and Machine Learning. The methods should be demonstrated with concrete examples from the fields of assisted and automated driving. Care is also taken about validation, verification and safeguarding of the related models and AI-based software components.

Course Objectives

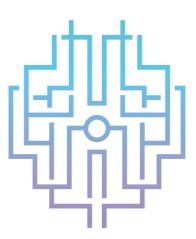
This seminar provides an overview and a brief introduction to the relevant methods of Artificial Intelligence and Machine Learning, so that both developers and managers can clearly decide which methods and procedures are relevant for their applications and which possible pitfalls they should consider in the application.

Who should attend?

Developers and (project) managers who have not yet had deep experience with the methodology and want to get a quick overview and introduction to the use of artificial intelligence.

Course Contents

- Introduction of data-based development versus analytical and rule-based approaches
- Overview of the different procedures and areas of application
- Artificial Neural Networks, Deep Learning, various variants and architectures
- Decision and regression trees
- Support Vector Machines
- Validation and safeguarding of models, sampling procedures, robustness assessment
- Data preparation and problem parameterization
- Meta modeling and model committees





Dr. Andreas Kuhn (Andata Entwicklungstechnologie GmbH) studied Technical Mathematics and Mechanical Engineering at the Technical University of Vienna. After his dissertation on the simulation of special satellite formations for the European Space Agency, he began his professional career in crash simulation at BMW. After further years as a consultant for stochastic simulation at EASI Engineering GmbH (today carhs), he founded ANDATA in 2004, where he is responsible for development and research as managing partner. Since 2009 he has also been co-owner of Automotive Safety Technologies GmbH in Gaimersheim. His professional interests are founded in effective and efficient development, validation and assessment methods for complex, safety-critical systems. In particular, he has been working for more than 20 years on the development and combined application of methods from the fields of artificial intelligence, machine learning, advanced simulation methods, scenario-based approaches and according process models in the virtual development of vehicles and autonomous robots. His current activities are the development and implementation of cooperative, networked, automated driving strategies for effective traffic automation.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	02.0202.03.2021	186/3726	Online	5 Days	1.340,- EUR till 05.01.2021, thereafter 1.590,- EUR	
	28.0601.07.2021	186/3761	Online ¹	4 Days	790,- EUR till 31.05.2021, thereafter 940,- EUR	
	2627.10.2021	186/3762	Alzenau	2 Days	1.340,- EUR till 28.09.2021, thereafter 1.590,- EUR	

¹ Online Seminar with reduced content



Active Safety | AD Seminar



Scenario-, Simulation- and Data-based Development, Validation and Safeguarding of Automated Driving Functions

Course Description

The complexity of modern driver assistance systems and automated driving functions sometimes requires completely new methods and approaches for their development, validation and testing. In particular, the wide coverage and analysis of functions with numerical simulation over the entire operating range (the so-called Operational Design Domain) is an indispensable tool for the effective and efficient development of appropriate vehicle functions. The course is about presenting the basics of scenario-based and data-based development and putting them in a holistic context.

Course Objectives

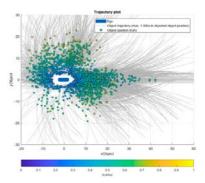
The course provides an overview and a brief introduction to the relevant scenario management methods for simulation and data-centric development and validation of automated driving functions. Some key basic principles in the development of complex systems are to be taught.

Who should attend?

The seminar addresses employees of automotive manufacturers, suppliers, engineering service providers, government agencies and research institutions, who are engaged in the development and validation of automated driving functions. In particular, method and process developers, simulation and test engineers are also addressed, who are responsible to implement corresponding processes and methods in their companies to ensure safe development and assessment of automated driving functions.

Course Contents

- Overview of the basic functions of automated driving
- Basics of Scenario and Data-based development
- Basics in Machine Learning, Data Mining and Artificial Intelligence
- Stochastic Simulation, Monte-Carlo-Simulation, Designof-Experiments
- Optimization and automated calibration
- Robustness and complexity management
- Anomaly and fault detection
- . Development processes for complex systems and software, top-down versus bottom-up
- Functional requirements management .
- Validation and verification
- . Definitions Operational Design Domain
- Effectiveness assessment of system functions and components
- Quality management for simulation data





Dr. Andreas Kuhn (Andata Entwicklungstechnologie GmbH) studied Technical Mathematics and Mechanical Engineering at the Technical University of Vienna. After his dissertation on the simulation of special satellite formations for the European Space Agency, he began his professional career in crash simulation at BMW. After further years as a consultant for stochastic simulation at EASI Engineering GmbH (today carhs), he founded ANDATA in 2004, where he is responsible for development and research as managing partner. Since 2009 he has also been co-owner of Automotive Safety Technologies GmbH in Gaimersheim. His professional interests are founded in effective and efficient development, validation and assessment methods for complex, safety-critical systems. In particular, he has been working for more than 20 years on the development and combined application of methods from the fields of artificial intelligence, machine learning, advanced simulation methods, scenario-based approaches and according process models in the virtual development of vehicles and autonomous robots. His current activities are the development and implementation of cooperative, networked, automated driving strategies for effective traffic automation.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	0306.05.2021	187/3764	Online ¹	4 Days	790,- EUR till 05.04.2021, thereafter 940,- EUR	
	1617.11.2021	187/3763	Alzenau	2 Days	1.340,- EUR till 19.10.2021, thereafter 1.590,- EUR	
					¹ Online Seminar with reduced content	141

141





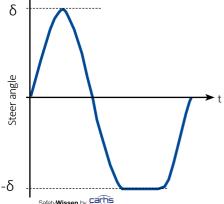
Test of ESC Systems in UN R140, GTR 8 and FMVSS 126

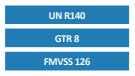
Step 1: Slowly-Increasing-Steer Manoeuvre to determine Parameter A

At a constant velocity of 80 ±2 km/h the steering angle is ramped at 13.5 deg/s until a lateral acceleration of 0.5 g is reached. Out of 2 series (1x left turn / 1x right turn) with 3 repetitions of the manoeuvre the steering angle A (in degrees) at which the lateral acceleration is 0.3 g is determined using linear regression.

Step 2: Sine with Dwell Manoeuvre to assess Oversteer Intervention and Responsiveness

At a velocity of von 80 \pm 2 km/h the vehicle is subjected to two series of test runs using a steering pattern of a sine wave at 0.7 Hz frequency with a 500 ms delay beginning at the second peak amplitude:



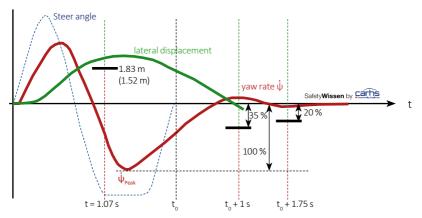


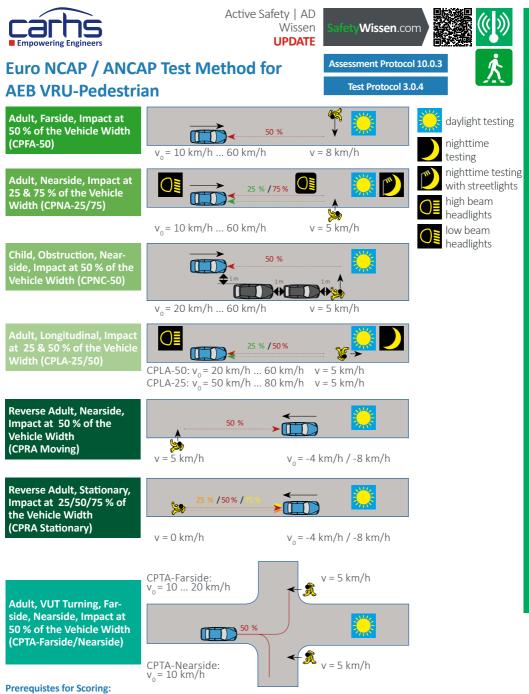
SafetyWissen by

One series uses counterclockwise steering for the first half cycle, and the other series uses clockwise steering for the first half cycle. In each series of test runs, the steering amplitude is increased from run to run, by 0.5 A, starting at 1.5 A. The steering amplitude of the final run in each series is the greater of 6.5 A or 270 degrees, provided the calculated magnitude of 6.5 A is less than or equal to 300 degrees. If any 0.5 A increment, up to 6.5 A, is greater than 300 degrees, the steering amplitude of the final run is 300 degrees.

Performance Requirements:

- Yaw Rate
 - 1 s after completion of the steering input (t₂) < 35 % of the first peak value of yaw rate recorded after the steering wheel angle changes sign
 - 1.75 s after completion of the steering input (t_x) < 20 % of the first peak value of yaw rate recorded after the steering wheel angle changes sign.
 - Lateral displacement of the vehicle center of gravity with respect to its initial straight path when computed 1.07 seconds after the Beginning of Steer (BOS)
 - for vehicles with GVM (GVWR) ≤ 3500 kg > 1.83 m
 - for vehicles with GVM (GVWR) > 3500 kg > 1.52 m





- The AEB system must be default ON at the start of every journey.
- The AEB system must operate from speeds \geq 10 km/h in the CPNA-75 day + night, must be able to detect pedestrians walking as slow as 3 km/h and reduce speed in the CPNA-75 scenario at 20 km/h.
- The system may not automatically switch off at a speed < 80 km/h.
- The score of the pedestrian impact tests (legforms & head) must be \geq 18 points.





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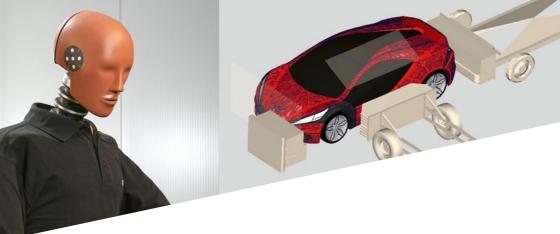
Test Protocol 3.0.4



Euro NCAP / ANCAP Test Method for AEB VRU-Pedestrian

			Scoring method:	AEB I			max. t	08	75	70	65	60	55	50	45	40	35	30	25	20	15	10	00	4			vo (km/h)	Scoring Table:
pass / fail: points are awarded if Vimpact ≤ vo - 20 km/h pass / fail: points are awarded if Forward Collision Warning (FCW) is issued @ TTC ≥ 1.7 s, or if the manufacturer demonstrates that	score = points x (vo - vimpact) / vo	pass / fail: points are awarded for full avoidance	nethod:	AEB Pedestrian total points	scenario points (3)	normalized scores (2)	max. total scenario score (1)																		function assessed	light conditions	Scenario	Table:
varded if warded if	npact) / v	varded fc			0.5		20					1	2	2	ω	ω	ω	2	1	ц	Ц	1			AEB	day	CPFA-50	
Vimpact: Forwarc	0	or full avo			0.25		20					1	2	2	ω	ω	ω	2	1	1	1	1			AEB	day	CPNA-25	
≤ vo - 20 d Collision		oidance			1		20					2	ω	ω	ω	2	2	1	1	1	1	1			AEB	night	A-25	
km/h n Warnir					0.25		20					Ц	2	2	ω	ω	ω	2	1	ц	ц	1			AEB	day	CPNA-75	
ng (FCW)					Р		20					2	ω	ω	ω	2	2	1	1	ц	ц	1			AEB	night		poi
is issued				Σ(2)·(3)	р	actua	20					р	2	2	ω	ω	ω	2	1	Ц	ц	1			AEB	day	CPNC-50	nts availa
@ TTC≥				max. 9 points	1 day/	actual score / (30 day /					2	ω	ω	ω	2	2	1	1	1					AEB	8 day	CPLA-50	points available per test speed
1.7 s, or i				oints	1 day/1 night	(1)	30 day / 30 night	1	1	Ц	1	2	ω	ω											FCW	day & night	CPLA-25	est speed
f the man							~													÷	ь	1			AEB	day	CPTA Farside	
ufacturer					1		4															1			AEB	day	CPTA Nearside	
demonsti					1		2																1	Ц	AEB	day	CPRA Stationary	
rates that					1		2																1	1	AEB	day	CPRA Moving	

their ESS (Emergency Steering Support) system provides appropriate support to avoid the collision



VEHICLE SAFETY – SIMULATION AND TESTING

Specialists for the development of vehicle safety – From concept to SOP

- Development of active and passive vehicle safety respecting legal, consumer rating and customer requirements
- Validation of conventional and alternative powertrain variants (HV, H2)
- Functional development and management of safety attributes
- CAE
- Component development of restraint systems
- Testing and coordination of component, system and the complete vehicle
- Execution of certification testing and homologation support

Our support throughout the process chain is reflected in EDAGs complete vehicle development projects.



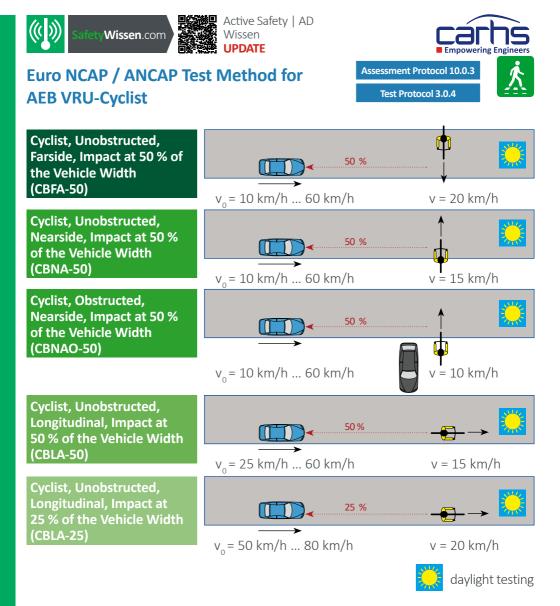
Contact

EDAG Engineering GmbH Kreuzberger Ring 40 65205 Wiesbaden Germany

safety@edag.com



edag.com



Prerequisites for Scoring:

- The AEB system must be default ON at the start of every journey.
- The system may not automatically switch off at a speed < 80 km/h.
- The score of the pedestrian impact tests (legforms & head) must be ≥ 18 points.



ON SITE & ONLINE

16th PraxisConference **Pedestrian Protection**



July 07 – 08, 2021

Bergisch Gladbach, Germany www.carhs.de/pkf

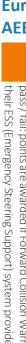








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pass / fail: points are awarded if Forward Collision Warning (FCW) is issued @ TTC \geq 1.7 s, or if the manufacturer demonstrates that

their ESS (Emergency Steering Support) system provides appropriate support to avoid the collision

Euro NC AEB VR score = points x (vo - vimpact) / vu pass / fail: points are awarded if vimpact ≤ vo - 20 km/h

С	AF	>/	Α	N	CA	P 1	ſes	st	M	et	ho	d	fo	r				Asse	essn	nent	Pro	toco	ol 10.0.3	3
R	J-(Cyc	clis	st															Tes	t Pro	otoc	ol 3.	0.4	
	Scoring method:				max.	80	75	70	65	60	б	50	45	40	ω	30	25	20	15	10			vo (km/h)	Scoring Table:
score = points x (vn - vimnact) / vn	method:	AEB Cyclist total points	scenario points (3)	normalized scores (2)	max. total scenario score (1)																function assessed	light conditions	Scenario	Table:
nnart) / vn			ω		11					1	Ľ	Ľ	1	1	1	1	1	1	1	1	AEB	day	CBFA-50	
			1.5		11					1	1	1	1	1	1	1	1	1	1	1	AEB	day	CBNA-50	
		$\Sigma(2)\cdot(3)$ max. 9 points	1.5	actual score $/(1)$	11					Ъ	Ц	Ц	1	1	1	1	1	1	1	1	AEB	day	CBNAO-50	points available
		S.		-	2					1	ω	ω	ω	2	2	1	1				AEB	day	CBLA-50	points available per test speed
			ω		27	1	1	1	1	1	ω	ω									FCW	day	CBLA-25	

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UPDATE





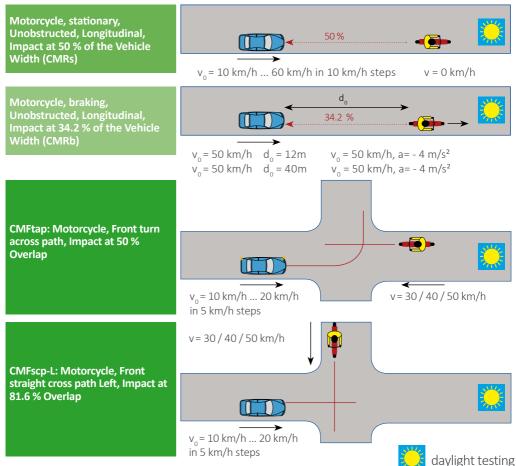
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Test Method for AEB PTW

The **MUSE** (Motorbike Users Safety Enhancement) project has developed test and assessment procedures for AEB PTW (Powered Two Wheelers) that are a basis for **Euro NCAP's AEB PTW** assessment starting in 2023. Please note that the actual Euro NCAP protocols are not available at this time and may differ from the information presented here.



Scoring Table for CMFTap and CMFscp-L:

		points available per test speed					
v ₀ (km/h)	VGMT	30 km/h	40 km/h	50 km/h			
10		1	1	1			
15							
20		1	1	1			
	max. total score (1)	∑ = 9					
	normalized scores (2)	actual score / (1)					
	scenario points (3)	3					
AEB CMFta	ap/ CMFscp-L total points		Σ(2)·(3)				

Scoring method:

pass / fail: points are awarded for full avoidance

Source: MUSE – UTAC CERAM





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Scoring Table for CMR:

	remaining impact apond				points available				
v ₀ (km/h)	remaining impact speed				CMRs	1Rb			
	v _{impact} (km/h)				AEB	AEB	FCW		
10	0 >0			>0	1				
20	0 >0				1				
30	<5 <15 <20 ≥20				1				
40	<5 <15 <20 ≥20				1				
50	< 5	< 15	< 20	≥20	1	1x2	1x2		
60	< 5	< 20	< 20	≥20	1				
		max. to	otal sco	ore (1)	∑=6	∑ = 2	∑ = 2		
	no	rmalize	ed scor	es (2)	a	ctual score / (1	L)		
		scena	rio poiı	nts (3)	0.5 0.3 0.2				
	A	B CMF	R total	points		Σ(2)·(3)			

Scoring method:

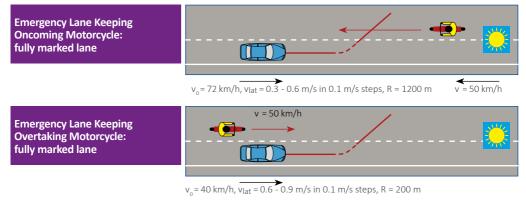
1.0 0.75 0.5 0 points are awarded depending on v_{impact} levels

Total AEB Car-to-PTW Score:

The maximum total score for AEB Car-to-PTW is 7.0 points (1.0 pt. CMR + 3.0 pt. CMFTap + 3.0 pt. CMFscp-L).

Test Method for Lane Support Systems PTW

The **MUSE** (Motorbike Users Safety Enhancement) project has developed test and assessment procedures for LSS PTW (Powered Two Wheeler) that are a basis for **Euro NCAP's LSS PTW** assessment starting in 2023. Please note that the actual Euro NCAP protocols are not available at this time and may differ from the information presented here.



Scoring Table for LSS PTW:

Scenario	Criteria	Points
Oncoming vehicle	full avoidance at all v _{lat}	1.0
Overtaking vehicle	two different warnings (visual, haptic or acoustic) \ge 1.2 s TTC or full avoidance at all v _{lat}	1.0
	max_total LSS PTW score	2.0

Note: The score distribution proposed by the MUSE project (7 points AEB PTW + 2 points LSS PTW) differs from the proposal by the Euro NCAP Rating Group (6 points + 3 points) in the Euro NCAP Rating Review 2018 V1.1.

Source: MUSE – UTAC CERAM



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Euro NCAP / ANCAP Test Method for AEB Car-to-Car

Prerequisites for Scoring in AEB Car-to-Car:

- AEB system needs to be default ON at the start of every journey and de-activation should not be possible with a single push on a button
- AEB and/or FCW must be operational up to speeds of at least 130 km/h, excluding stationary targets
- audible component of FCW needs to be loud and clear
- for CCRs only: Whiplash score for front seat must be at least "good", full avoidance must be achieved for speeds ≤ 20 km/h in all overlap situations

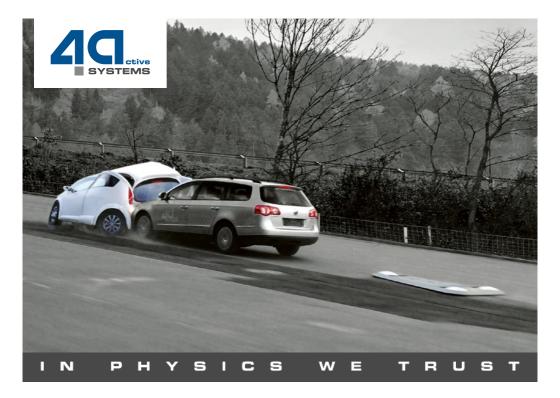
Car-to-Car Rear

CCRs*: Approach to stationary Target with ± 50 % / ± 75 % / 100 % Overlap AEB + FCW	$v_0 = 10$ km/h 80 km/h in 5 km/h step	v=0 km/h
CCRm*: Approach to slower Target with ± 50 % / ± 75 % / 100 % Overlap		
AEB + FCW	v _o = 30 km/h 80 km/h in 5 km/h step	os v = 20 km/h
CCRb*: Approach to braking Target		
100 % Overlap	$v_0 = 50 \text{ km/h}$ $d_0 = 12 \text{ m}$	$v_0 = 50 \text{ km/h}, a = -2 \text{ m/s}^2$
	$v_0 = 50 \text{ km/h}$ $d_0 = 40 \text{ m}$	v _o = 50 km/h, a = -2 m/s ²
* CCR: Car-To-Car Rear; s: stationary; m: moving; b: braking	$v_0 = 50 \text{ km/h}$ $d_0 = 12 \text{ m}$	$v_0 = 50 \text{ km/h}, a = -6 \text{ m/s}^2$
Coordina Tables	$v_0 = 50 \text{ km/h}$ $d_0 = 40 \text{ m}$	v _o = 50 km/h, a = -6 m/s ²

Scoring Table:

v ₀ (km/h)	remaining impact speed vimpact (km/h)				Poi avail			remaining relative impact speed V relative impact (km/h)					Points available			
		vim	Dact (KI	11/11)		CC	:Rs	CC	Rb	v relative impact (KITI/TI)			CCRm			
						AEB		AEB	FCW						AEB	FCW
10	0				>0											
15	0				>0											
20	0				>0											
25	< 5		< 15		≥15											
30	< 5	< 15	< 25		≥25					< 5				≥5	1	
35	< 5	< 15	< 25		≥25					< 5				≥5	1	
40	< 5	< 15	< 25	< 35	≥35					< 5		< 15		≥15	1	
45	< 5	< 15	< 25	< 35	≥35					< 5		< 15		≥15	1	
50	< 5	< 15	< 30	< 40	≥40			1x4	1x4	< 5	< 15	< 25		≥25	1	1
55	< 5	< 15	< 30	< 45	≥45					< 5	< 15	< 25		≥ 25	1	1
60	< 5	< 20	< 35	< 50	≥ 50					< 5	< 15	< 25	< 35	≥ 35	1	1
65	< 5	< 20	< 40	< 55	≥ 55					< 5	< 15	< 25	< 35	≥ 35	2	2
70	< 5	< 20	< 40	< 60	≥ 60					< 5	< 15	< 30	< 40	≥40	2	2
75	< 5	< 25	< 45	< 65	≥65					< 5	< 15	< 30	< 45	≥45	2	2
80	< 5	< 25	< 50	< 70	≥70		1			< 5	< 20	< 35	< 50	≥50	2	2
Grid point score	1.0	0.75	0.5	0.25	0	∑=14	∑=18	<u>Σ</u> =4	Σ=4	1.0	0.75	0.5	0.25	0	∑=15	Σ =11





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 UPDATE

Euro NCAP / ANCAP Test Method for AEB Car-to-Car



The score per test speed vo for AEB and FCW is calculated as Σ grid point scores¹ x points available / 6

The score per scenario and system (AEB/FCW) is calculated as **Score per test speed vo / Spoints available**

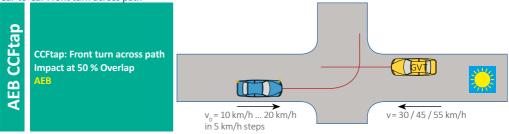
The score per system (AEB/FCW) is the average score per scenario of that system. The score per system is multiplied with 2.0 points for AEB and 1.5 points for FCW.

Where FCW does not result in full avoidance in the - 50 % overlap² grid points, the manufacturer can alternatively demonstrate that their **EES (Emergency Steering Support)** system functions to avoid the collision.

Manufacturers are expected to provide a prediction of the grid point scores. This predicted score per system is multiplied with the correction factor resulting from 10 verification tests for that system conducted by Euro NCAP³:

Correction factor = actual tested score / predicted score

Car-to-Car Front turn across path



Scoring Tal	ble:	points available per test speed					
v ₀ (km/h)	VGVT	30 km/h	45 km/h	55 km/h			
10							
15							
20							
	max. total score (1)	9					
n	ormalized scores (2)	actual score / (1)					
	scenario points (3)	2					
AE	B CCFtap total points	$\Sigma(2)$ ·(3) max. 2 points					

Scoring method:

pass / fail: points are awarded for full avoidance

Human Machine Interface

HMI points are added if there is a **supplementary warning** (other than audiovisual) for FCW (1 point) and if there is a **reversible belt pre-pretensioning** in the pre-crash phase (1 point). The HMI score is scaled down to a max. of **0.5 points**.

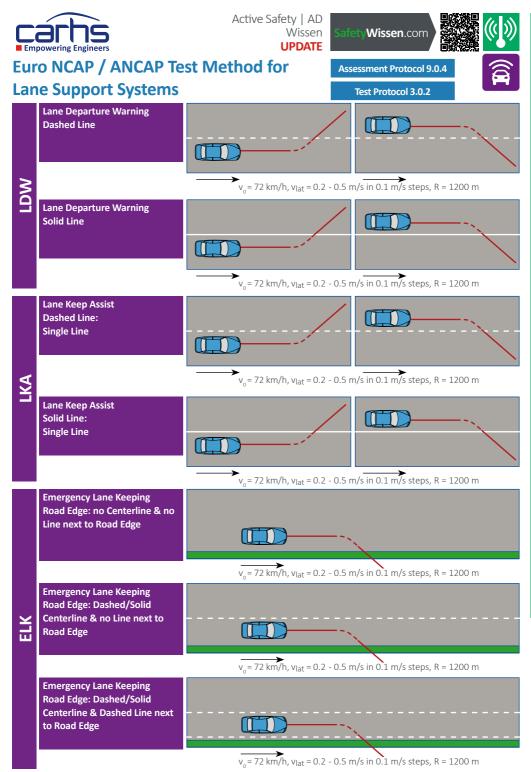
Total AEB Car-to-Car Score

The maximum total score for AEB Car-to-Car is 6 points (2 pt. CCR AEB + 1.5 pt. CCR FCW + 2.0 pt. CCFtap + 0.5 pt. HMI)

 $^{\scriptscriptstyle 1}\,$ where the score of the 100 % overlap grid point is double counted

- ² + 50 % overlap for RHD vehicles
- ³ plus up to 10 additional tests sponsored by the manufacturer







¹ Distance To Lane Edge

² max. HMI score limited to 0.50 points





Auf Deutscl



NCAP - New Car Assessment Programs Tests, Assessment Methods, Ratings

Course Description

In 1979 the first New Car Assessment Program (NCAP) was established by NHTSA in the United States. The goal was to motivate competing car manufacturers to enhance the safety level of their cars beyond the minimum safety standards defined by regulations. The same approach has been followed globally by other organizations (e.g. by Euro NCAP, IIHS, ANCAP, JNCAP, KNCAP, C-NCAP, ...). Euro NCAP which has been established in 1997 has taken a leading role and has significantly influenced other countries and regions. The NCAP programs in many cases are highly dynamic, especially in comparison with rulemaking activities. In order to reach the goal to continuously improve the safety level of cars, the requirements need to be permanently adapted to the state of technology. Developers in the automotive industry need to know about upcoming changes at an early stage in order to be able to design or equip their vehicles accordingly.

In this seminar attendees get an overview of the organizations in charge of the NCAP programs and become familiar with the various test and assessment methods.

The seminar is conducted several times a year with changing focuses:

- Focus passive safety: Here the focus is on test and assessment methods for passive safety. Frontal and side impact, whiplash, child protection and pedestrian protection are discussed in detail. Tests for active safety are only mentioned in as far as they are relevant for the overall rating.
- Focus active safety: Here the focus is on active safety systems such as AEB or lane assistance. The tests and assessments for these systems are explained in detail. Tests for passive safety are only mentioned in as far as they are relevant for the overall rating.

In both focusses the current overall rating methods are described and explained. In addition to that an outlook is given on the roadmaps and future developments of the NCAP programs.

Who should attend?

The seminar addresses design, simulation, testing and project engineers as well as managers who want to get a current overview on the global range of NCAP programs with an outlook on upcoming topics and trends from an insider. Depending on the focus of their work attendees should chose the appropriate focus of the seminar.

Course Contents

- New Car Assessment Programs overview
- U.S. NCAP
- IIHS
- Euro NCAP
- ANCAP
- JNCAP
- KNCAP
- C-NCAP
- C-IASI
- Latin NCAP
- ASEAN NCAP
- Bharat NCAP
- Global NCAP



Direktor and Professor Andre Seeck (German Federal Highway Research Institute)

is head of the division "Vehicle Technology" with the German Federal Highway Research Institute (BASt). In this position he is responsible for the preparation of European Safety Regulations. Furthermore he represents the German Federal Ministry of Transport and Digital Infrastructure in the Board of Directors of Euro NCAP and he is the chairman of the strategy group on automated driving and of the rating system. These positions enable him to gain deep insight into current and future developments in vehicle safety. In 2017 NHTSA awarded him the U. S. Government Special Award of Appreciation.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
ä	1922.04.2021	164/3818	Online ¹	4 Days	790,- EUR till 22.03.2021, thereafter 940,- EUR	
	2324.06.2021	164/3819	Alzenau	2 Days	1.340,- EUR till 26.05.2021, thereafter 1.590,- EUR	
	2728.10.2021	164/3820	Alzenau	2 Days	1.340,- EUR till 29.09.2021, thereafter 1.590,- EUR	

¹ Online Seminar with reduced content

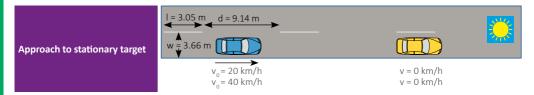


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IIHS AEB / Front Crash Prevention Test

AEB Test Protocol, V. I, Oct 2013



Assessment:

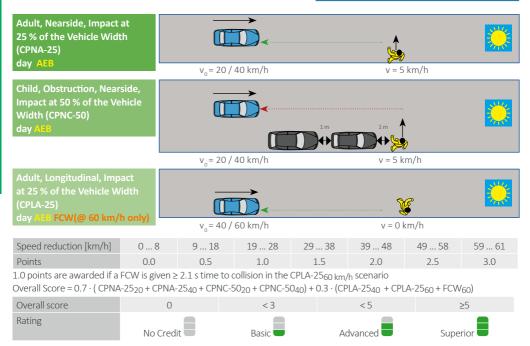
		20 km/h Test		40 km/h Test					
Speed reduction	< 8 km/h	8 - 14 km/h	≥ 15 km/h	< 8 km/h	8 - 14 km/h	15 - 34 km/h	≥ 35 km/h		
Points	0	1	2	0	1	2	3	1	

Rating Scheme:

Points			
	1	2 - 4	>5
Rating	BASIC	ADVANCED	SUPERIOR

IIHS Test Scenarios for AEB Pedestrian

Pedestrian AEB Test Protocol, V. II, Feb 2019





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U.S. NCAP Crash Imminent Braking

	CRASH IMMINENT BRAKE SYSTEM PERFORMA	NCE EVALUTION, Oct 2015
LVS (Lead Vehicle Stopped)		
Approach to stationary target	v _o = 25 mph (40.2 km/h)	v = 0 mph
LVM (Lead Vehicle Moving)		
Approach to slower target	v _o = 25 mph (40.2 km/h) v _o = 45 mph (72.4 km/h)	v = 10 mph (16.1 km/h) v = 20 mph (32.2 km/h)
LVD (Lead Vehicle Decelerating)		
Approach to braking target	v _o = 35 mph (56.3 km/h) d _o = 45.3 ft (13.8 m) ± 8 ft (2.4 m)	▼ v _o = 35 mph (56.3 km/h) a = -0.3 g
False Positive Test		
Approach to steel trench plate	v _o = 25 mph (40.2 km/h) 8 ft x 12 ft x 1 i v _o = 45 mph (72.4 km/h)	n (2.4 m x 3.7 m x 25 mm)

Requirements

Scenario	LVS	LVM 25 mph	LVM 45 mph	LVD	False Positive
Requirement	∆v≥9.8 mph (15.8 km/h)	no impact	Δv≥9.8 mph (15.8 km/h)	∆v ≥ 10.5 mph (16.9 km/h)	deceleration ≤ 0.5 g

U.S. NCAP Forward Collision Warning

	FORWARD COLLISION WARNING SYSTEM	CONFIRMATION TEST, Feb 2013
LVS (Lead Vehicle Stopped) Approach to stationary target	v _o = 45 mph (72.4 km/h)	v = 0 mph
LVM (Lead Vehicle Moving) Approach to slower target	v _o = 45 mph (72.4 km/h)	v = 20 mph (32.2 km/h)
LVD (Lead Vehicle Decelerating) Approach to braking target	$v_0 = 45 \text{ mph} (72.4 \text{ km/h}) d_0 = 89.4 \text{ ft} (30 \text{ m}) \pm 8.2 \text{ ft} (2.5 \text{ m})$	0

Requirements

Scenario	LVS	LVM	LVD
Requirem	ent Alert no later than	Alert no later than	Alert no later than
	2.1 s TTC	2.0 s TTC	2.4 s TTC





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U.S. NCAP Rear Automatic Braking

Rear Automatic Braking Feature Confirmation Test Procedure (Working Draft), Dec 2015



Dummy

4a Euro NCAP Pedestrian - Child Dummy static

Test Procedure^{*}

- Place the direction selector in reverse while maintaining full pressure on the brake pedal.
- Release the vehicle's brake pedal and allow the vehicle to coast backward while maintaining the vehicle's centerline within +/-1 inch of the longitudinal line marked on the ground.
- Allow the vehicle to coast until the rear automatic braking feature intervenes by automatically engaging the service brakes bring the vehicle to a stop or until the vehicle strikes the test object. Once either of these two outcomes occurs, the vehicle's brake pedal should be depressed to end the test trial. Every effort must be made to safely conduct this test. If testing indoors, proper ventilation must be provided. No personnel shall be located to the rear of a test vehicle at any time during the test trial.

Requirements*

- A positive test outcome would involve the vehicle coming to a stop before it reaches the location of the test object and with no physical contact with the test object for each of the three test object locations assessed.
- * Please note: The rear automatic brake test is part of the planned U.S. NCAP upgrade. The test procedure and requirements are based on "Rear Automatic Braking Feature Confirmation Test Procedure (Working Draft), December 2015". Docket NHTSA-2015-0119.

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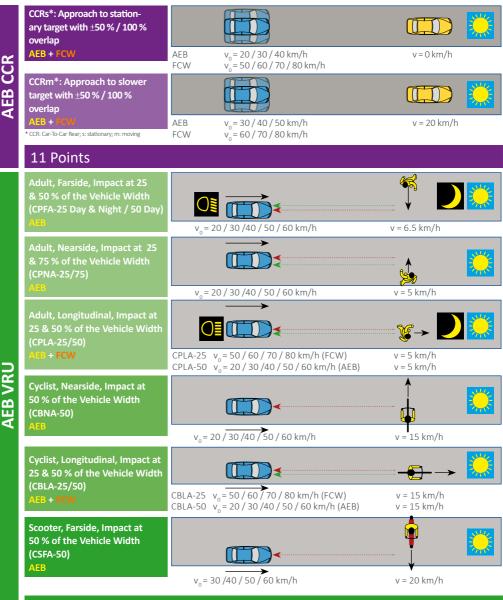
C-NCAP Active Safety Rating

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UPDATE

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Management Regulation 2021 (valid from 1/2022)



21 Points (10 Pedestrian + 11 Two-wheelers)

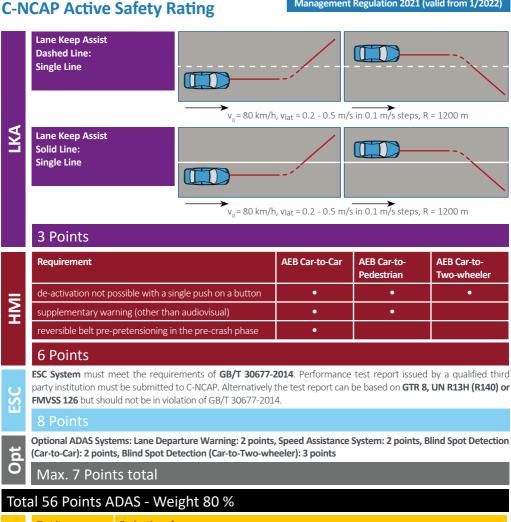




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Management Regulation 2021 (valid from 1/2022)



	Test item	Evaluation of
lts	Low Beam	straight line illumination, corner illumination, pedestrian visibility on the left, pedestrian visibility at intersection, width of curve lighting
<u>60</u>	High Beam	illumination range, pedestrian visibility at intersection
ead	Bonus	adaptive low beam function, adaptive high beam function, automatic low beam turn on function, automatic headlight leveling system
I	Demerits	glare
	10 Points	

Total 10 Points Headlights - Weight 20 %

Overall rating see page C-NCAP p. 63



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i-VISTA Intelligent Vehicle Integrated Systems Test Area

AEB Car-to-Car				Test Protocol A0-2020 Rating Protocol A0-20			
System	Scenario	v ₀ (km/h)	v _{Target} (km/h)	Criteria	Points	Σ	Σ
	CCRs	72	0	Warning issued @ ≥ 2.1 s TTC	1		
FCW	CCRb	72	72 @ -3m/s²	Warning issued $@ \ge 2.4 \text{ s TTC}$	1	3	
	CCRm	72	30	Warning issued $@ \ge 2.0 \text{ s TTC}$	1		
	CCRs	30	0		3	16	
AEB		50	0	Speed reduction	5		
AED	CCRm	50	20				
		70	20		5		22
Advanced Assistance		50	20	Additional warning: head-up display, seat belt vibration, tac warning			
		70	20				
		ous Emergency Steering Assist		Collision Avoidance	1		

AEB VRU				Test	Test Protocol A0-2020 F			Rating Protocol A0-2020		
System	Scenario	v ₀ (km/h)	v _{Target} (km/h)	Light Condition	Criteria	Points	Σ	Σ		
		20				2				
	CPNA-25	40				4				
		60				2				
		20		Day		2				
	CPNSOC-50	40		Duy		4				
		60				2				
AEB	CPNDOC-50	20			Speed reduction	2				
Pedestrian		30				3				
	CPNA-25	20				2	8			
		40				4				
		60				2		56		
	CPLA-25	25		Day		2		00		
		45				4				
	CPFOA-50	20		Night		2				
		30		- Night		3				
		20				2				
	CBNA-50	40				4	8			
		60				2				
AEB Cyclist	CBLA-50	35	15	Day		2				
	CBLA-SU	55				4				
	CBLA-50 (FCW)	55			FCW: Warning issued @ ≥ 1.7 s TTC	2	2			



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i-VISTA Intelligent Vehicle Integrated Systems Test Area

Lane Support	Systems			Test Protocol A0-2020	Rating Pro	tocol A0	-2020		
System	Scenario	v ₀ (km/h)	v _{lat} (m/s)	Criteria	Points	Σ	Σ		
LDP Lane		70	0.2	8	8				
Departure Prevention		72	0.5	– DTLE > - 0.3 m					
LDW	parture	Ctraight lang	Straight Jana	72	0.2		4		14
Lane		/2	0.5	Warning issued before					
Departure		72	0.2	DTLE < - 0.3 m	2				
Warning	Curve		0.5						

Side Support Systems

Test Protocol A0-2020

Rating Protocol A0-2020

System	Scenario		v ₀ (km/h)	v _{Target} (km/h)	Criteria	Points	Σ	Σ
				70		2		
		Left side		90		1		
	Overtaking		60	120		1		
BSD Blind Spot	car		00	70		2		
Detection		Right side		90		1		
Detection				120		1		
	Overtaking	Left side	20	30	Alarm issued within speci- fied interval	1	2	15
	two-wheeler	Right side				1		
		Left front		15		1		
		door						
DOW		Left rear				0.5		
Door	Overtaking	door	0					
Opening Warning		Left front						
warning		door		30				
		Left rear door				0.5		
	RCW Rear Collision Warning					0.5		
Advanced	RCTA Rear Cro				feature availability	0.5		
Assistance	DOW Rear ind					1		

Bonus Points

If all models across the model range are equipped with the rated systems as standard, bonus points are awarded. Bonus points do not increase the maximum score per system.

System equipped as standard	Bonus
AEB Car-to-Car	1
AEB VRU	3
LDP or LDW	1
BSD or DOW	1

Overall Rating

The overall rating is based on the normalized total score.

Rating	Good		Marginal	Poor					
Normalized score = total points / max. total points	≥ 75 %	≥ 65 %	≥ 50 %	< 50 %					
ne overali rating is based on the normalized total score:									

Rating Protocol A0-2020





automotive

October 19 – 20, 2021 **Congress Park Hanau** Germany

Computer simulation has become an indispensable tool in automotive development. Tremendous progress in software and computer technology makes it possible today to assess product and process performance before physical prototypes have been built. Despite of significant progress in simulation technology and impressive results in industrial application there remains a number of challenges which prevent a "100 % digital prototyping". We at carhs.training call these Grand Challenges.

Automotive CAE Grand Challenge offers a Platform for Dialogue

The automotive CAE Grand Challenge stimulates the exchange between users, scientists and software developers in order to solve these challenges. Annually the current, critical challenges in automotive CAE are being identified through a survey among the simulation experts of the international automotive industry. In the conference one session is dedicated to each of the most critical challenges, the so-called Grand Challenges. In each session CAE experts from industry, research and software development will explain the importance of the individual Challenge for the virtual development process and talk about their efforts to solve the challenge.

Automotive CAE Grand Challenges 2021

In October 2020 we have determined the important current challenges of automotive CAE - the so-called "Grand Challenges" - through a survey among the CAE experts of the international automotive industry. These "Grand Challenges" will form the topics of the sessions of our automotive CAE Grand Challenge 2021 conference:

- BODY STIFFNESS & STRENGTH: Modeling of Connections
- CAE PROCESS & QUALITY: Comparing Test and Simulation
- CRASH: Material Models for Battery Packs of Electric Vehicles
- **DURABILITY: Vibration Fatigue of HV-Batteries**
- FULL VEHICLE: Load Cases for Release of Automated Driving Functions
- NOISE VIBRATION HARSHNESS: Variability Analysis
- **OCCUPANT SAFETY: Scatter including OOP Simulation**

Who should attend?

The conference intends bringing together industrial users, researchers and software developers to discuss these current, critical challenges of automotive CAE and to initiate collaboration between these groups to help overcoming the Grand Challenges of automotive CAE. The presentation program of the conference provides both experts and beginners valuable information for their daily work. The possibility to meet and exchange with all stakeholders of automotive CAE is a great opportunity. In the accompanying exhibition participants can receive additional information from leading companies of CAE.

DATE VENLIE HOMPAGE

166

19.-20.10.2021 Hanau, GERMANY & ONLINE

www.carhs.de/grandchallenge

LANGUAGE

PRICE

980,- EUR till 21.09.2021, thereafter 1.180,- EUR, ONLINE 590,- EUR









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Introduction to Impact Biomechanics and Human Body Models

Course Description

To prevent human injury in traffic it is necessary to understand the biomechanics of impact. This can be done through experimental studies with human subjects, volunteers, or post-mortem human subjects (PMHS), after ethical approval. The individual variation is large in experiments with human subjects, due to the wide spread of anthropometry and material properties that depend on factors such as gender, age, and health status. Mechanical anthropometric crash test dummies were developed to provide repetitive tools for development and assessment of safety systems for specific loading scenarios, representing mid-size males, large males, small females and children of different ages. With the development of advanced safety systems, the need for repetitive tools with increased biofidelity and anatomical details, initiated development of numerical human body models. With increasing computer capacity, human body models have become popular tools for traffic safety research, crash simulations, safety evaluations and to study the effects of population diversity on traffic safety. This course covers the basic topics of impact biomechanics, such as human anatomy, population variance, mechanical properties of human tissues, and injury criteria. Finally, it focuses on computational models of the human body and their use to develop and evaluate safety systems.

Course Objectives

The objective of this course is to introduce impact biomechanics, injury biomechanics, and to provide an overview of computational models of the human body. You will learn about the most important topics and get a chance to understand how it relates to your work and traffic safety in general.

Who should attend?

This seminar addresses everyone who wants to obtain an upto-date overview or who needs a deepened understanding of the field of impact biomechanics, such as university graduates, career changers, management, project assistants, internal service providers, qualified technicians from the crash-test lab or anyone basing product development or decision-making on simulation results with human body models.

Course Contents

- Introduction to impact biomechanics
 - Human anatomy & physiology
 - Medical terminology
 - Injury scaling scores
 - Epidemiology
 - Human substitutes
- Material properties
 - Soft tissues
 - Hard tissues
- Injury mechanisms, tolerances & criteria
 - Head and neck
 - Thorax
 - Upper and lower extremities
- Population variability
 - Biomechanics of children
 - The aging population
 - Gender differences
- Human body models
 - Introduction to numerical methods
 - Methodology for model development
 - Validation of models
 - State of the art models
 - Strengths and limitations



Prof. Dr. Karin Brolin (Lightness by Design AB) has worked in the field of impact biomechanics throughout her career. Karin Brolin earned her Ph.D. in 2002 at the Royal Institute of Technology, and since then she has worked in both academia and industry on the topic of human body injury mechanisms and tolerances. The past ten years she led a research group focusing on human body simulations for traffic safety and injury prevention, as Professor in Computational Impact Biomechanics at Chalmers University of Technology. Since 2019 Dr. Brolin has worked as an independent consultant and researcher.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Õ	1215.04.2021	193/3793	Online	4 Days	1.340,- EUR till 16.03.2021, thereafter 1.590,- EUR	
	2326.11.2021	193/3794	Online ¹	4 Days	790,- EUR till 26.10.2021, thereafter 940,- EUR	

¹ Online Seminar with reduced content

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DATE VENUE HOMPAGE LANGUAGE

to be announced Würzburg, GERMANY & ONLINE www.leichtbau-gipfel.de German with translation into English



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Robust Design - Vehicle Development under Uncertainty

Course Description

The seminar addresses the current state of the art complemented by recent achievements in research and development to quantify and control uncertainties (lack-of-knowledge and variations) in vehicular development. Aspects of sensitivity and robustness analysis are discussed as well as topics in reliability, resilience, redundancy and model uncertainty. In addition, numerical methods for optimization with consideration of uncertainties and methods for Model Order Reduction (MOR) to reduce computational effort are discussed. Applications (e.g. NVH, crash) illustrate the usage of the methods and the fact that methods should be adapted to the degree of maturity of the design in the development process.

Course Objectives

The seminar is focused on methods and their theoretical background to enable the participants to realize applications directly in the industrial context. Hence, uncertainties can be characterized, quantified, and – together with sensitivity analysis – concept and structural evaluations are made possible, which consider robustness, reliability, resilience, and redundancy. Corresponding optimizations can then be realized in an efficient manner.

Who should attend?

The seminar is proposed for engineers with first experiences in numerical concept and series development of vehicles, who are interested in including robustness, reliability and other aspects of uncertainty management in their industrial designs.

Course Contents

- Mathematical methods for uncertainty quantification
- Linear and non-linear sensitivity analysis (global / local)
- Design of Experiments (DoE), Response Surface Methods (RSM)
- Methods for Model Order Reduction (MOR)
- Robustness versus reliability
- Robustness in early design stages (Set-based Design und Solution Space Approach)
- Methods for resilience, redundancy, model uncertainty
- Optimization under uncertainties
- Applications taken from acoustics and crashworthiness



172

Prof. Dr.-Ing. Fabian Duddeck (Technical University of Munich) is the head of the research group on optimization and robustness at the Technical University of Munich (TUM, Chair of Computational Mechanics, www.bgu.tum.de/cm). His research is focusing on numerical methods for optimization of structures with respect of crashworthiness, NVH (noise, vibration, and harshness), durability, and other disciplines. In this framework, new methods for stochastic modeling and robustness assessments for different types of uncertainties (aleatoric and epistemic) are included. Besides standard approaches using probabilistic theory, possibilistic and special methods for early phase design are developed and applied for problems in automotive, aerospace, and civil engineering.

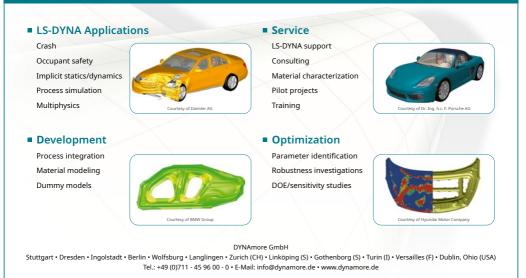
ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	2425.02.2021	144/3713	Alzenau	2 Days	1.340,- EUR till 27.01.2021, thereafter 1.590,- EUR	
	2021.09.2021	144/3744	Online ¹	2 Days	790,- EUR till 23.08.2021, thereafter 940,- EUR	

¹ Online Seminar with reduced content

Simulation and More



Finite Element Solutions



Interior Development – Fundamentals, Materials, Design, Manufacturing

Course Description

The seminar illustrates the subject, in many parts with workshop character:

Part 1: Basics of Plastics - physics, chemistry and application technology, in industry and in the automobile. Processes for Rapid Prototyping and Rapid Tooling, as well as the processes of mass manufacturing, such as injection molding and blow molding, are discussed. Day 1 ends with a workshop in which, based on practical examples, functionality and choice of materials are treated.

Part 2: Plastics in Automotive Interiors deals with the use of plastics in automotive interiors and their properties. Interior components are subject to many requirements, ranging from the design appearance, look and touch and ergonomics to production and assembly. The second part explains what is being done at various stages of the interior development process. Using the example of the cockpit and the cockpit module, the materials and processes used are discussed. Due to the complexity of the topic a lot of real components are shown and their properties are discussed.

Course Objectives

The aim of the seminar is to provide the necessary skills for the design of vehicle interior components and modules. This includes in particular the choice of materials, the design and manufacturing processes.

Who should attend?

The seminar is aimed at engineers, technicians and managers who are planning and controlling interior development projects. The focus of the seminar is on the cockpit module.



Dates

Timo Baumgärtner (csi entwicklungstechnik GmbH)

SEMINAR ON DEMAND

DURATION LANGUAGE

You can book this seminar as an in-house seminar with a minimum of 5 participants directly at your site. Alternatively, if you are interested in the course, you can make a reservation. As soon as a sufficient number of participants has been reached, we will arrange a specific course date with the interested parties.

2 Davs









Structural Optimization in Automotive Design Theory and Application

Course Description

In recent years numerical simulation has gained importance in all engineering disciplines. In the automotive industry the development process evolved from an experiment based to a virtual development process. Through this move towards simulation, mathematical optimization also gained importance and new opportunities for its application have been opened within the development process. Only a few years ago it would have been unthinkable to find the optimal cross section and the number and location of ribs for a cast part through mathematical optimization, which is now common practice.

As there exists no single optimization method that is suited for all problems it is important to gain an overview over various optimization methods and their characteristics. In the seminar the most popular and reliable optimization methods will be presented. The focus will be on the explanation of the basic concepts and ideas rather than on the detailed mathematical derivations and formulations.

Emphasis will be on practical applications. Possibilities for using optimization methods will be demonstrated through many industrial examples.

The following questions will be answered in the seminar:

- Which optimization methods are suited for which problems and which are not?
- How big is the optimization effort?
- How can the optimization effort be minimized?
- Which possibilities exist for the formulation of different optimization problems?
- What can lead to failure of an optimization?

Course Objectives

At the end of the seminar participants will have gained an overview over different optimization disciplines and procedures, the areas of application and their individual limitations.

Who should attend?

The seminar is suited for engineers and technicians from research and development departments, users that intend to enlarge or fresh up their background knowledge and new-comers that want to get an overview of the subject.

Course Contents

- Local and global optimization methods and coupled strategies
- Approximation methods
- Lagrange function, dual method
- Optimality criteria methods
- Bionic optimization procedures (CAO, SKO, evolutionary algorithms, optimization with particle swarms)
- Coupling with FEM
- Formulation of optimization problems
- Sensitivity analysis
- Determination of important variables and variable reduction
- Sizing
- Shape optimization, use of morphing techniques, topology optimization
- Robustness optimization
- Multi disciplinary and multi objective optimization
- Numerous application examples



Prof. Dr. Lothar Harzheim (Opel Automobile GmbH) worked in the Group of Professor Mattheck on the development of the optimization programs CAO and SKO, before joining the simulation department of Opel. At Opel he is responsible for optimization, bio engineering and robustness. In this position he not only introduced and applied optimization methods but has also developed software for topology optimization. Prof. Dr. Harzheim regularly holds seminars for applied structural optimization and teaches at the Technical University of Darmstadt. He is the author of the book "Strukturoptimierung: Grundlagen und Anwendungen".

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	2425.02.2021	112/3704	Alzenau	2 Days	1.340,- EUR till 27.01.2021, thereafter 1.590,- EUR	
	2225.11.2021	112/3798	Online ¹	4 Days	790,- EUR till 25.10.2021, thereafter 940,- EUR	

¹ Online Seminar with reduced content



CAEWissen.com

CAEWissen.com is <u>the</u> news portal for engineers and CAE experts in the automotive industry. On CAEWissen.com users find daily news from industry and research as well as many other topics from automotive CAE.





Improving Efficiency and Reducing Risk in CAE Driven Product Development

Course Description

To avoid mistakes and economic loss, CAE-applications require reasonable and reliable workflows. This seminar provides background information on risks of using CAE and gives recommendations of implementing best practice. Maintaining high quality of CAE applications and enhancing efficiency within the context of organizational structures and analysis tasks are the main focus of this seminar. Use of knowledge management builds a bridge between performing an analysis project and improving efficiency. Knowledge management is a basis for efficiency, quality of prognosis and reliability of CAE application. A holistic view onto knowledge management and knowledge based engineering will be given.

Who should attend?

The seminar is aimed at product developers, CAE engineers but also managers and decision makers who are responsible



Prof. Dr.-Ing. Klemens Rother (Munich University of Applied Sciences)

for risk, performance and efficiency of projects supported by numerical analyses.

Inhalte

- Motivation to use structured processes in CAE
- Which risks managers and analysis experts are facing?
- Use of CAE to minimize risks
- Structured process management in CAE as a means to focus improvements
- Duties of analysis experts and managers from liability and warranty issues
- Efficient and quality driven process management
- Specific procedural requirements for CAE environment and CAE processes
- Verification and validation
- Monitoring and documentation
- Quality driven practices and collaboration with suppliers

SEMI

Dates

SEMINAR ON DEMAND

DURATION LANGUAGE

You can book this seminar as an in-house seminar with a minimum of 5 participants directly at your site. Alternatively, if you are interested in the course, you can make a reservation. As soon as a sufficient number of participants has been reached, we will arrange a specific course date with the interested parties.

1 Day







Design of Composite Structures

Course Description

Since the mass is one of the main factors influencing the fuel consumption of vehicles, increasing demands to reduce energy usage and CO2 emissions, force the automotive industry to consider the use of alternative designs and new materials. Composite materials have proven their potential to reduce the weight of structures in many applications (e.g. aerospace and motorsports). As composites have a special set-up and behave completely different than traditional materials, engineers must learn how to employ these materials to take advantage of their special characteristics in the design of vehicle structures. In the seminar real world examples are used to create a basic understanding of designing composite structures. Then the theoretical and practical foundations of composite design are explained.

Course Objectives

After participating in the seminar participants are able to design and develop composite structures. They understand the specific requirements of composite structures and the related design concepts. In the seminar special attention is directed to the concurrent consideration of loading, design and manufacturing related requirements. Accordingly, the different designs - integral, differential, fully laminated and sandwich - are addressed. The seminar also provides knowledge about preliminary design and FE analysis based on classical laminate theory.

Who should attend?

This seminar is especially designed for engineers and technicians who work in the development departments of automotive manufacturers, suppliers and engineering service providers and deal with the design and development of composite components.

Course Contents

- Introduction
- Elastic behavior of composite materials
- Failure of composite materials
- Mechanics of composite materials and structures
- Joining technologies for composites
- Design of composite structures
- Fatigue and strength of composites





Dr.-techn. Roland Hinterhölzl (University of Applied Sciences Upper Austria) has been heading the Professorship Composite Materials and the study degree program "Lightweight Design and Composite Materials" at the University of Applied Sciences Upper Austria since 2016. From 2010 to 2016 he was head of the numerical simulation department of the Institute for Carbon Composites at the Technical University of Munich. The focus of his work is on process simulation and structural analysis for the automotive and aviation industries. Dr. Hinterhölzl received his doctorate in 2000 at the University of Innsbruck on the simulation of the time-dependent behavior of composite materials, after he had spent several months at the Department of Aerospace Engineering and Engineering Mechanics at the University of Texas at Austin and CRREL (USA). Subsequently, he developed innovative composite components at the aerospace supplier FACC AG and headed the structural analysis department.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Da	1819.03.2021	135/3696	Alzenau	2 Days	1.340,- EUR till 18.02.2021, thereafter 1.590,- EUR	
	2023.09.2021	135/3829	Online ¹	4 Days	790,- EUR till 23.08.2021, thereafter 940,- EUR	

¹ Online Seminar with reduced content







Material Models of Composites for Crash Simulation

Course Description

Increasing demands for weight reduction paralleled by requirements for improved crash performance and stiffness of structures have strongly pushed the development of advanced composites. The use of composite materials today is not limited to niche applications or secondary parts; they are increasingly used for important load carrying structural components in series production.

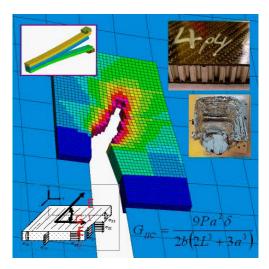
In this one day seminar Prof. Thomas Karall presents the foundations of structural impact and crash analysis of composites with the Finite Element Method. At the beginning of the seminar an overview of current and upcoming industrial applications of composite materials is given. Thereafter concepts for the correct physical modeling of the complex load degradation and failure mechanisms in numerical simulation are presented. The course concentrates on the numerical simulation of the crash behavior of composites and is accompanied with demonstrations using the PAM-CRASH code.

Who should attend?

The course addresses simulation and project engineers, project managers as well as researchers involved in the analysis and design of composite parts and structures.

Course Contents

- Current and upcoming areas of application of composite materials
- Analysis of composite materials
- Available material models and their application
- Modeling methods for plies and laminates
- FEM modeling of composites
- Failure mechanisms and their representation
- PAM-CRASH ply and delamination models
- Necessary material tests
- Examples





Prof. Dr. Thomas Karall (Hof University of Applied Sciences) studied mechanical engineering at the Technical University of Vienna and received his PhD as Assistant Professor at the University of Leoben in the field of fibre-reinforced plastics and the calculation by finite elements. From 2006 to 2010 he was head of department at the Austrian Research Institute for Chemistry and Technology in Vienna in the field of mechanical and thermal testing / fibre composites, and Secretary General of the Austrian Working Group for reinforced plastics. From 2010 to 2015 he worked as Lead Researcher for lightweight design at Virtual Vehicle Research Center in Graz. He was also a lecturer at the Technical University of Graz and lecturer at the FH Joanneum Graz. Since 2015 he has been Professor at the Engineering Department of the Hof University. His areas of work include lightweight design, fibre-reinforced composites and the finite element method.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	16.02.2021	68/3698	Alzenau	1 Day	790,- EUR till 19.01.2021, thereafter 940,- EUR	
	1416.09.2021	68/3756	Online	3 Days	790,- EUR till 17.08.2021, thereafter 940,- EUR	







Material Models of Metals for Crash Simulation

Course Description

Besides an appropriate spatial discretisation of the structure and a profound knowledge of the required load cases, appropriate material modelling is a key ingredient for predictive crash simulations. The load carrying structure of a car today still mainly consists of metallic materials. The materials to be described are diverse.

The seminar deals with the following materials:

- Mild and high strength steels,
- cold formable AHSS and UHSS steels,
- hot formable and quenchable boron steels,
- wrought Al and Mg alloys,
- cast Al and Mg alloys,
- metalic material produced by additive manufacturing.

The objective of this 1-day course is to give the participants an overview of material models of metals used in crash simulation. Within the first chapter the deformation behavior and the failure mechanisms of each material class are explained based on the material structure. In the second chapter phenomenological models for crash simulation of metals are introduced. This includes elasticity, viscoplasticity and failure due to localized necking, ductile normal fracture and ductile shear fracture. In case of crashworthiness simulation the influence of strain rate on the aforementioned properties is of high interest. In the third chapter the tests needed for the characterization of materials are described and the param-

The seminar was extremely well received in our company! Even our colleagues, who had already worked a lot in this area, were able to learn many new things."

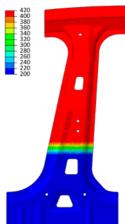
Fabian Wolf - P+Z Engineering GmbH

eter identification for the material models is discussed. The manufacturing process can have a significant impact on the material properties (pre-straining of sheets, paint bake heat treatment,local heating in joining processes etc.). Within the fourth chapter simulation examples are discussed which show the sensitivity of simulation results regarding the identified material parameters. In the final chapter the influence of the discretization on the predictive quality of a crashworthiness model is discussed. This includes both the element size and the type of element (shell vs. solid).

Who should attend?

The course addresses engineers working in the field of crash simulation and heads of simulation departments interested in the important topic of material modelling.

- Course Contents
- Overview of metallic materials used in cars
- Influence of material structure on mechanical behavior
- Phenomenological material models for metals
- Overview of experimental methods for material characterization
- Identification of material parameters from experiments
- Discussion of the sensitivity material parameters





Dr.-Ing. Helmut Gese (MATFEM - Partnerschaft Dr. Gese & Oberhofer) founded the engineering consultancy MATFEM in 1993 (from 1999 the company has been named MATFEM partnership Dr. Gese & Oberhofer). MATFEM offers technical and scientific consultancy services at the intersection of material science and finite element methods. Besides performing FEM analysis projects the area of activity covers experimental and theoretical characterization of materials and the development of new material models for simulation.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Õ	1821.01.2021	70/3796	Online	4 Days	790,- EUR till 21.12.2020, thereafter 940,- EUR	
	07.10.2021	70/3797	Alzenau	1 Day	790,- EUR till 09.09.2021, thereafter 940,- EUR	







Material Models of Plastics and Foams for Crash Simulation

Course Description

Numerical simulation has become a fundamental element in the development of motor vehicles. Today, many important design decisions, especially in the field of crash, are based on simulation results. During the last few years there has been an increase in the use of foams in vehicles. These are, due to their variety and structure, much more complicated regarding the characteristics of the materials than "simple" materials such as steel or aluminum, which can be modelled rather well. Characterization of foam materials is a great challenge for the simulation expert. Although by now there are different modelling approaches available in explicit FEM-programs such as LS-DYNA, PAM-CRASH or RADIOSS, these are, however, often not satisfactory. The application of these special material models requires a sound knowledge and experience.

The seminar provides an overview over plastics and foam materials used in automotive engineering and their phenomenology. On the first day you obtain an introduction into the simulation of elastic and visco-elastic polymers, such as elastomers and elastic polymer foams with volume elements. You are thereby coming to understand the available material models in explicit finite element programs.

On the second day the focus is on the treatment of plastics, such as thermo- and duroplastics through elasto-plasticity with isotropic hardening. Non-associated deformation is going to be discussed as well. The seminar is rounded off with the procedure for simulation of glass-fiber reinforced plastics using both isotropic and anisotropic material laws.

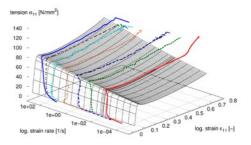
For a demonstration you are going to see examples created with the program LS-DYNA. References to material models in LS-DYNA an PAM-CRASH are going to help you in applying what you will have learnt.

Who should attend?

The seminar addresses experienced CAE engineers and heads of CAE departments with an interest in plastic and foam materials simulation. At least 1-year of experience with FEM-programs such as LS-DYNA, PAM-CRASH or RADIOSS is suggested for participating in this course.

Course Contents

- . Overview of polymer materials used in vehicle construction
- Verification and validation procedure for crash simulation
- Introduction to mechanics of materials
- Simulation of elastic and visco-elastic rubbers and foams with volume elements
- Overview of available material models in explicit finite element codes
- Simulation of elastic-plastic polymers under crash loading for validation
- Simulation of anisotropic materials with application to glass-fiber reinforced plastics





Prof. Dr.-Ing. Stefan Kolling (TH Mittelhessen University of Applied Sciences) is Professor for Mechanics at the TH Mittelhessen University of Applied Sciences (THM). Previously he worked as a simulation engineer at the Mercedes Technology Center in Sindelfingen. He was responsible for methods development in crash simulation. In particular he was involved in the modeling of non-metal materials such as glass, polymers and plastics. Prof. Kolling graduated from the Universities of Saarbrücken and Darmstadt, from where he also received his Ph.D. He is author of numerous publications in the field of material modeling.

ates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
ä	1518.03.2021	37/3760	Online ¹	4 Days	790,- EUR till 15.02.2021, thereafter 940,- EUR	
	2021.09.2021	37/3759	Alzenau	2 Days	1.340,- EUR till 23.08.2021, thereafter 1.590,- EUR	
					¹ Online Seminar with reduced content	179









Modeling of Joints in Crash Simulation

Course Description

For the efficient assembly of components and complete structures many different joining techniques are available. Joints have to ensure that the assembly will fulfill crashworthiness, durability and other requirements. Therefore the best joining technique has to be selected for each application. Modern lightweight design often uses a material mix. Using different materials, like various steel grades, lightweight alloys, plastics or composites for applications for which the individual material is best suited allows for weight savings. The efficient and reliable joining of different materials is even more challenging. Failure of joints can be a reason for collapse of vehicle structures during crash testing. Therefore failure of joints must be precisely predicted in numerical crash simulation applied in the virtual design process of vehicle development.

Course Objectives

The objective of this one day course is to give the participants an overview of failure modelling of different joints (punctiform, linear, planar joints) for crash simulation and also of the characterization tests and methods that are necessary for calibrating the model parameters. Also recommendation for validation tests and simulations of calibrated joint models are given. Examples of typical and used models are shown in all common crash codes.

Who should attend?

The course addresses engineers working in the field of crash simulation and heads of simulation departments interested in the important topic of modelling of joints including failure.

Course Contents

- Overview of modeling techniques for different joining techniques
- Tests and methods for characterization of joints
- Local loading conditions at joints during testing under shear, tension and bending load
- Characteristics of failure behavior
- Failure modeling of
 - Spot welded joints including spot welds in press hardened steels
 - Self-piercing riveted joints
 - Laser welded joints
 - Adhesive joints
- Calibration methods for determination of model parameters
- Validation of calibrated models through testing and simulation



Dr.-Ing. Silke Sommer (Fraunhofer-Institut für Werkstoffmechanik) studied Physics at the RWTH Aachen University and obtained her PhD degree at the Karlsruhe Institute of Technology about modeling of the deformation and failure behaviour of spot welds. She has been working at the Fraunhofer Institute for Mechanics of Materials IWM in Freiburg since 2000 in the field of damage and failure modeling of materials and joints for crash simulation. Since 2013 she is a group leader for joining and joints.

ites	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
Õ	09.03.2021	155/3707	Alzenau	1 Day	790,- EUR till 09.02.2021, thereafter 940,- EUR	
	2730.09.2021	155/3821	Online	4 Days	790,- EUR till 30.08.2021, thereafter 940,- EUR	



Simulation | Engineering Seminar





Introduction to the Python Programming Language

Course Description

Python is a modern programming language that is increasingly used in the field of Scientific Computing. Together with the environment scipy Python is an open source alternative to the commercial software MATLAB. A series of CAE software products, including the Pre-Processor ANSA, the solvers ABAQUS and PAM-CRASH and the Post-Processor META, are already using Python as an integrated scripting language. Python puts the emphasis on well-readable code, so beginners can learn the language very quickly. Nevertheless, Python is a powerful programming language and can also be used for larger projects. Further advantages of Python are the platform independence and the very extensive standard library supplied.

Course Objectives

The seminar provides a comprehensive introduction to the basics of the Python programming language. It also includes an introduction to object-oriented programming. Practical exercises, such as processing text-based files from the CAE world, will be treated. After the seminar, participants will be able to acquaint themselves with the Python interfaces of CAE software products.

Who should attend?

The seminar is aimed at newcomers to the Python language. Experience in other scripting or programming languages would be an advantage but is not a requirement.

Course Contents

- Basic concepts of the Python programming language
 Introduction to the language
 - Data and control structures, functions
- Advanced topics
 - Processing of data
 - Important modules of the Python standard library
 - Examples from scientific computing
 - Modularization in bigger Python projects
- Practical exercises





Dr. André Backes (TECOSIM Technische Simulation GmbH) studied Mathematics at the University of Duisburg. From 2000 to 2006 he was a researcher at the Institute for Mathematics at the Humboldt University in Berlin. His PhD studies at the chair for Numerical Mathematics introduced him to the field of CAE. Since 2006 he works at TECOSIM GmbH in Ruesselsheim and among other topics specialized in NVH. In the area of Virtual Benchmarking he helped developing the TECOSIM-owned process TEC|BENCH where also the Python language was used. In current research projects he investigates the use of Python-based methods for data analysis and machine learning in the CAE process. Since March 2020 he has been working at Tecosim Stuttgart.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
õ	2629.01.2021	161/3730	Online ¹	4 Days	790,- EUR till 29.12.2020, thereafter 940,- EUR	
	0104.02.2021	161/3734	Online ¹	4 Days	790,- EUR till 04.01.2021, thereafter 940,- EUR	
	1718.03.2021	161/3708	Alzenau	2 Days	1.340,- EUR till 17.02.2021, thereafter 1.590,- EUR	
	1617.11.2021	161/3735	Alzenau	2 Days	1.340,- EUR till 19.10.2021, thereafter 1.590,- EUR	
					¹ Online Seminar with reduced content	181







Simulation|Engineering Seminar

page 140



Python based Machine Learning with Automotive Applications

Course Description

The topic of Artificial Intelligence (AI) is currently becoming more and more important, in particular in areas where processes are automated and many data are processed. Especially in automotive area as well in the virtual development process as in the field of testing, numerous applications are conceivable in this context. A part of artificial intelligence is machine learning, which is becoming increasingly important in addition to classical rule-based expert systems. This current development is due to the generation of ever-larger datasets (big data) as well as more powerful computers for their processing.

Especially in the automotive environment, extensive data are generated in the context of simulation or testing, for which an automated analysis is often sought. In addition to the classical interpretation of individual simulation or testing results, the methods of machine learning allow a new view at models and results. Based on the analysis of numerous results (big data), e.g. from parameter studies, it is possible to derive Artificial Intelligence using methods of machine learning, which is then used to evaluate further simulations or tests.

Python is currently the most popular programming language for data analysis and machine learning. The freely available Python library Scikit-Learn provides a user-friendly entry to the relevant procedures. Especially the application of artificial neural networks (Deep Learning) has become very popular lately. The software TensorFlow developed by Google and the Python library Keras based on it provide a beginner-friendly access.

Course Objectives

The seminar gives an introduction to machine learning based on the programming language Python. This includes, as a start, topics of data analysis, preparation and visualization.

In the second step, methods of machine learning are studied using the Python packages Scikit-Learn and Keras or Tensor-Flow. Practical exercises will deepen the topics discussed and discuss possible applications in CAE or testing. An important aspect of data analysis is the extraction of features from CAE or testing data for the use in machine learning. After the seminar participants will be able to tackle the implementation of their own tasks. This also includes evaluating various methods of machine learning regarding their applicability to one's own tasks and to deepen the methods based on the discussed Python packages.

Further Seminars on the Topic Machine Learning & Artificial In<u>telligence</u>

Who should attend?

The seminar addresses participants coming from CAE or testing field who want to take the first steps in machine learning based on their Python knowledge. It is assumed that basic Python knowledge - e.g. as it is conveyed in the carhs.training seminar Introduction to the Python Programming Language of the same trainer - exists.

Course Contents

- Basics of data analysis with Python
 - Data structures
 - Concepts of data preparation
 - Extraction of features for machine learning methods
 - Data visualization
 - The Python packages Numpy, Scipy, Pandas, Matplotlib
- Machine Learning with Python
 - Methods for classification and regression analysis
- The Python Package Scikit-Learn
 - Deep Learning and Neural Networks with Keras, TensorFlow
 - Applications motivated by CAE or testing background
 - Introductory examples
 - Discussion of possible deeper applications
 - Procedure for implementing your own ideas



Dr. André Backes (TECOSIM Technische Simulation GmbH) studied Mathematics at the University of Duisburg. From 2000 to 2006 he was a researcher at the Institute for Mathematics at the Humboldt University in Berlin. His PhD studies at the chair for Numerical Mathematics introduced him to the field of CAE. Since 2006 he works at TECOSIM GmbH in Ruesselsheim and among other topics specialized in NVH. In the area of Virtual Benchmarking he helped developing the TECOSIM-owned process TEC|BENCH where also the Python language was used. In current research projects he investigates the use of Python-based methods for data analysis and machine learning in the CAE process. Since March 2020 he has been working at Tecosim Stuttgart.

Dates	DATE	ID	VENUE	DURATION	PRICE	LANGUAGE
ď	1922.04.2021	185/3736	Online ¹	4 Days	790,- EUR till 22.03.2021, thereafter 940,- EU	
	0405.05.2021	185/3709	Alzenau	2 Days	1.340,- EUR till 06.04.2021, thereafter 1.590,- EUR	
	30.1101.12.2021	185/3737	Alzenau	2 Days	1.340,- EUR till 02.11.2021, thereafter 1.590,- EUR	

2 ¹ Online Seminar with reduced content



SafetyWissen UPDATE

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Important Abbreviations

Α	
AAA	American / Australian
	Automobile Association
AAAM	Association for the
	Advancement of Automotive
	Medicine
AAM	Alliance of Auto
= D A C	Manufacturers
aBAS	Advanced Brake Assist
ACC	System Adaptive Cruise Control
ACEA	Association of European
ACLA	Automobile Manufacturers
ACL	Anterior cruciate ligament
ACN	Automatic Collision
/ 10/11	Notification
ACSF	Automatically Commanded
	Steering Function
ACU	Airbag Control Unit
AD	Automated Driving
ADAC	Allgemeiner Deutscher
	Automobil Club (German
	Automobile Association)
ADAS	Advanced Driver Assistance
	Systems
ADL	Automatic Door Locking
ADOD	Average Depth of
	Deformation
ADR	Australian Design Rules
AE-MDB	Advanced European Mobile
	Deformable Barrier
AEB	Autonomous Emergency
	Braking
AEBS	Autonomous Emergency
A.F.C	Brake System
AES	Autonomous Emergency
AHB	Steering
AHOD	Auto High Beam
AHOD	Average Height of Deformation
AHOF	Average Height of Force
AHR	Active Head Rest
AIS (1)	Abbreviated Injury Scale
AIS (2)	Automotive Industry
, (2)	Standards (India)
AISC	Automotive Industry
	Standards Committee
ANCAP	Australasian New Car
	Assessment Program
AOP	Adult Occupant Protection
	(Euro NCAP)
APF	Abdominal Peak Force
APROSYS	
	SYStems
APSS	Active Pedestrian Safety
	System
ARAI	Automotive Research
	Association of India
ARV	Advanced Rear Visualization
ASCC	Adaptive Speed Cruise
ACIC	Control
ASIC	Application-Specific

	Integrated Circuit
ASIL	Automotive Safety Integrity
	Level (Functional Safety)
ASIS	Adavanced Side Impact
	System
ATD	Anthropomorphic Test
	Device
AZT	Allianz Zentrum Technik
В	
BAS	Brake Assist
BASt	Germany's Federal Highway
	Research Institute
BDA	Bonnet Deployment Actuator
BEV	Battery Electric Vehicle
BIS	Bureau of Indian Standards
BLE	Bonnet Leading Edge
BMVI	German Federal Ministry
	of Transport and Digital
	Infrastructure
BoD	Board of Directors (Euro
	NCAP)
BOS	Beginning of Steer
BRIC	Brain Injury Criterion
BSD	Blind Spot Detection
BST	Blind Spot Technology
BTA	Bumper Test Area
С	
C-IASI	China Insurance Automotive
	Safety Index
C-NCAP	China New Car Assessment
	Programme
C2C	Car-to-Car
CA	Crash Avoidance
CAE	Computer Aided Engineering
CAN	Controller Area Network
CAT	Computer Aided Testing
CATARC	China Automotive
	Technology and Research
	Center
CCD	Charge Coupled Device
CCR	Car to Car-Rear
CDC	Collision Deformation
	Classification
CEA	Comité Européen des
CED	Assurances
CFD	Computational Fluid
CED	Dynamics
CFR	Code of Federal Regulations
CEDD	(USA)
CFRP	Carbon Fiber Reinforced
CID	Plastic Create Increase Deplain a
CIB CLEPA	Crash Imminent Braking
CLEPA	Comité de liaison européen des fabricants d'equipements
	et de pièces automobiles
CMM	Coordinate Measuring
CIVIIVI	Machine
CMOS	Complementary Metal Oxide
CMOS	Semiconductor
CMVR	Central Motor Vehicle Rules
CMVSS	Canadian Motor Vehicle
0111733	Safety Standards
	Surcey Stanuarus

COG	Center of Gravity
	Conselho Nacional de
	Trânsito
COP(1)	Carry over Parts
COP (2)	Child Occupant Protection
COI (2)	(Euro NCAP)
CORD	
COPD	Child Occupant Presence
	Detection
COS	Completion of Steer
CP	Contact Point
CPD	Child Presence Detection
CRABI	Child Restraint Airbag
	Interaction (Child Dummy)
CRS	Child Restraint System
CSMA/CA	Carrier Sense Multiple Access
	/ Collision Avoidance
CSMA/CD	Carrier Sense Multiple Access
CSIVIAYCD	/ Collision Detection
C 11	
CV	Closing Velocity
CVFA	Car to Vulnerable road user
	Farside Adult
CVNA	Car to Vulnerable road user
	Nearside Adult
CVNC	Car to Vulnerable road user
	Nearside Child
D	
DAS	Data Assuriation Custom
	Data Acquisition System
DBS	Dynamic Brake Support
DCU	Domain Control Unit
DGPS	Differential Global Positioning
	System
DLO	Daylight Opening
DOW	Door Opening Warning
DOW	Door Opening Warning Deployable Pedestrian Protection Systems
DOW	Door Opening Warning Deployable Pedestrian Protection Systems
DOW DPPS	Door Opening Warning Deployable Pedestrian
DOW DPPS DSM DT	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring
DOW DPPS DSM DT E	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time
DOW DPPS DSM DT E EBA	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist
DOW DPPS DSM DT E	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking &
DOW DPPS DSM DT EBA EBA EBA	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP)
DOW DPPS DSM DT E EBA	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force
DOW DPPS DSM DT EBA EBA EBA	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution
DOW DPPS DSM DT EBA EBA EBA EBD EBT	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target
DOW DPPS DSM DT EBA EBA EBA	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for
DOW DPPS DSM DT EBA EBA EBA EBD EBT	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target
DOW DPPS DSM DT EBA EBA EBA EBD EBT	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for
DOW DPPS DSM DT EBA EBA EBA EBD EBT ECE	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic
DOW DPPS DSM DT EBA EBA EBA EBD EBT ECE	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council
DOW DPPS DSM DT EBA EBA EBD EBT ECE ECOSOC	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data
DOW DPPS DSM DT EBA EBA EBA EBD ECE ECCSOCC EDM	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management
DOW DPPS DSM DT EBA EBA EBA EBD ECE ECCSOCC EDM ESS	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed
DOW DPPS DSM DT EBA EBA EBA EBD ECE ECCSOCC EDM	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle-
DOW DPPS DSM DT EBA EBA EBD ECE ECC ECSOC EDM EES ECVC	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee
DOW DPPS DSM DT EBA EBA EBD ECE ECC EDM EES EEVC EIF	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force
DOW DPPS DSM DT EBA EBA EBD EBD ECC EDM EDM ECS ECV EIF ELK	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping
DOW DPPS DSM DT EBA EBA EBD ECE ECC EDM EES EEVC EIF	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping Electric SAfety (UNECE/
DOW DPPS DSM DT EBA EBA EBD EBT ECC ECC ECC ECC EDM EES EEVC ELK ELSA	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping ELectric SAfety (UNECE/ WP.29 Working Group)
DOW DPPS DSM DT EBA EBA EBD EBD ECC EDM EDM ECS ECV EIF ELK	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping ELectric SAfety (UNECE/ WP.29 Working Group) Electromagnetic
DOW DPPS DSM DT EBA EBD EBD ECC EDM ECOSOC EDM EES EEVC EIF ELK ELSA EMC	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Euro NCAP Bicyclist Target Economic Commision for Europe (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping ELectric SAfety (UNECE/ WP.29 Working Group) Electromagnetic Compatibility
DOW DPPS DSM DT EBA EBA EBD ECS ECC EDM ECS ECVC EIF ELK ELSA EMC EOU	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Europ (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping ELectric SAfety (UNECE/ WP.29 Working Group) Electromagnetic Compatibility Ease of Use
DOW DPPS DSM DT EBA EBA EBD EBT ECC EDM ECOSOC EDM EIF ELK ELSA EMC EOU EPB	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Europ (ASEAN NCAP) Electronic Brake Force Distribution Europe (United Nations) United Nations Economic and Social Council Engry Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping ELectric SAfety (UNECE/ WP.29 Working Group) Electromagnetic Compatibility Ease of Use Electrical Protection Barrier
DOW DPPS DSM DT EBA EBA EBD ECS ECC EDM ECS ECVC EIF ELK ELSA EMC EOU	Door Opening Warning Deployable Pedestrian Protection Systems Driver Status Monitoring Deployment Time Emergency Brake Assist Effective Braking & Avoidance (ASEAN NCAP) Electronic Brake Force Distribution Europ (United Nations) United Nations Economic and Social Council Engineering Data Management Energy Equivalent Speed European Enhanced Vehicle- Safety Committee Entry Into Force Emergency Lane Keeping ELectric SAfety (UNECE/ WP.29 Working Group) Electromagnetic Compatibility Ease of Use



Important Abbreviations

ERG ES-2 re ESA ESC ESS	Emergency Response Guide Euro SID 2 Rib Extension Emergency Steering Assist Electronic Stability Control Emergency Steering Support
ESV	Enhanced Experimental Vehicles Safety Program / Enhanced Safety of Vehicles Program
ETC ETSC	European Test Consortium European Transport Safety Council
Euro NCAF	
EVPC	Electric Vehicles Post Crash
EVS	Electric Vehicle Safety
EVT	Euro NCAP Vehicle Target
F	
FARS	Fatality Analysis Reporting
	System
FCEV	Fuel Cell Electric Vehicle
FCW	Forward Collision Warning
FCWS	Forward Collision Warning System
FEM	Finite Element Method
FFC	Femur Force Criterion
FIWG	Frontal Impact Working Group (Euro NCAP)
Flex PLI	Flexible Pedestrian Legform Impactor
FMH	Free Motion Headform (FMVSS 201)
FMVSS	Federal Motor Vehicle Safety Standards
FPS	Frontal Protection System
FPSLE	Frontal Protection System Leading Edge
FRG	Floating Rib Guide
FRP	Fiber Reinforced Plastic
FRS	Fitment Rating System (ASEAN NCAP)
FSI	Fluid-Structure-Interaction
FTDMA	Flexible Time Division
	Multiple Access
FW	Full Width
FWDB	Full Width Deformable Barrier
FWRB	Full Width Rigid Barrier
G	
G.S.R.	General Statutory Rules
GAMBIT	Generalized Acceleration Model for Brain Injury
GCS	Threshold Glasgow Coma Scale
GIDAS	German in-Depth Accident
GRSG	Study Groupe de Rapporteurs sur
0.00	la Sécurité Générale (WP.29 - General Safety Provisions)
GRSP	General Salety Provisions) Groupe de Rapporteurs sur la Sécurité Passive (WP.29 - Passive Safety)

GSR GTR GVM GVT GVWR	General Safety Regulation Global Technical Regulation Gross Vehicle Mass Global Vehicle Target Gross Vehicle Weight Rating
H HAD	Highly Automated Driving
HAV	Highly Automated Vehicle
HBM	Human Body Model
HGV	Heavy Goods Vehicle
HIC	Head Injury Criterion
HIT HLDI	Head Impact Time Highway Loss Data Institute
HLLC	High Level Liaison Committee
HMI	Human Machine Interface
HNI	Head Neck Impactor
HOF	Height of Force
HPC HPM	Head Performance Criterion H-Point Manikin
HPS	Head Protection System
HPT	Head Protection Technology
HRC	Time to Head Restraint first
	Contact
HRMD	Head Restraint Measuring Device
HRV	Head Rebound Velocity
HTD	, Hardest to detect
HV	High Voltage
1	
IARV	Injury Assessment Reference
	Value
IBRL	Internal Bumper Reference Line
ICPL	Internal Bumper Reference Line Injury Criteria Protection
ICPL	Line Injury Criteria Protection Level
	Line Injury Criteria Protection Level International Consumer
ICPL ICRT	Line Injury Criteria Protection Level International Consumer Research and Testing
ICPL	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group
ICPL ICRT IG	Line Injury Criteria Protection Level International Consumer Research and Testing
ICPL ICRT IG IHC IHRA	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities
ICPL ICRT IG IHC	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for
ICPL ICRT IG IHC IHRA IIHS	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety
ICPL ICRT IG IHC IHRA	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance
ICPL ICRT IG IHC IHRA IIHS	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de
ICPL ICRT IG IHC IHRA IIHS IIWPG	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports
ICPL ICRT IG IHC IHRA IIHS IIWPG INRETS	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité
ICPL ICRT IG IHC IHRA IIHS IIWPG	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de
ICPL ICRT IG IHC IHRA IIHS IIWPG INRETS	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Instituto Universitario de
ICPL ICRT IG IHC IHRA IIHS IIWPG INRETS	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de
ICPL ICRT IG IHC IHRA IIWPG INRETS INSIA IP	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research
ICPL ICRT IG IHC IHRA IIHS INRETS INSIA IP IRC	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research Council on the Biomechanics
ICPL ICRT IG IHC IHRA IIHS IIWPG INRETS INSIA IP IRC IRCOBI	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research Council on the Biomechanics of Impact
ICPL ICRT IG IHC IHRA IIHS IIWPG INRETS INSIA IP IRC IRCOBI	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research Council on the Biomechanics of Impact Injury Risk Function
ICPL ICRT IG IHC IHRA IIHS IIWPG INRETS INSIA IP IRC IRCOBI	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research Council on the Biomechanics of Impact
ICPL ICRT IG IHC IHRA IIHS IWPG INRETS INSIA IP IRC IRCOBI IRC IRCOBI	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research Council on the Biomechanics of Impact Injury Risk Function Intelligent Speed Assistance Intelligent Speed Management
ICPL IGRT IG IHC IHRA IIHS IWPG INRETS INSIA IP IRC IRCOBI	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research Council on the Biomechanics of Impact Injury Risk Function Intelligent Speed Management International Organization for
ICPL ICRT IG IHC IHRA IIHS IWPG INRETS INSIA IP IRC IRCOBI IRC IRCOBI	Line Injury Criteria Protection Level International Consumer Research and Testing Informal Group Intelligent Headlight Control International Harmonized Research Activities Insurance Institute for Highway Safety International Insurance Whiplash Prevention Group Institut National de Recherche sur les Transports et leur Sécurité Instituto Universitario de Investigación del Automóvil Intersection Point Injury Risk Curve International Research Council on the Biomechanics of Impact Injury Risk Function Intelligent Speed Assistance Intelligent Speed Management

ITC	Inland Transport Committee
i-VISTA	(UNECE) Intelligent Vehicle Integrated
IWVTA	Systems Test Area International Whole Vehicle
	Type Approval
1	
J-MLIT	Japan: Ministry of Land,
	Infrastructure and Transport
JA	Junction Assist
JAMA	Japan Automotive
	Manufacturers Association
JARI	Japan Automobile Research Institute
JASIC	Japan Automobile Standards
	Internationalization Center
JNCAP	Japan New Car Assessment Program
к	
	Kana an Mastan Makinla C. C. :
KMVSS	Korean Motor Vehicle Safety Standards
KNCAP	Korean New Car Assessment
KTH	Program
KIH	Knee - Thigh - Hip
L	
LDWS	Lane Departure Warning
	System
LHD	Left Hand Drive
LIDAR	Light Detection and Ranging
LIN	Local Interconnect Network
LINCAP	Lateral Impact New Car
	Assessment Program (U.S. NCAP)
LKAS	Lane Keeping Assist System
LKD	Lane Keeping Device
LKS	Lane Keeping System
LL	Lower Leg
LNL	Lower Neck Load
LSS	Lane Support System
LTR	Land Transport Rules (New
	Zeeland)
М	
MAIS	Maximum AIS (Abbreviated
	Injury Scale)
MCD	Multi Collision Brake
MCB	
MCL	Medial Collateral Ligament
MDB	Mobile Deformable Barrier
MoD	Motor own Damage
	(Insurance)
MOST	Media Oriented Systems
	Transport
MPDB	Moving Progressive
	Deformable Barrier
MSA	Manual Speed Assist
MST	Motorcyclist Safety
14131	Technology
MTBI	
	Mild Traumatic Brain Injury
MVWG	Motor Vehicle Working
	Group (EU)

Empowering Engineers



SafetyWissen UPDATE

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Important Abbreviations

N	
NASS	National Automotive
	Sampling System
NASS CDS	NASS Crashworthiness Data
	System
NASS GES	NASS General Estimates
	System
NASVA	National Agency for
	Automotive Safety & Victims'
NIGAR	Aid (Japan)
NCAP	New Car Assessment
NCSA	Program
NCSA	National Center for Statistics
	and Analysis (an Office of NHTSA)
NHTSA	National Highway Traffic
NITTSA	Safety Administration (USA)
NIC	Neck Injury Criterion
NISS	New Injury Severity Score
NNT	Number Needed to Treat
NPACS	New Programme for the
	Assessment of Child-restraint
	Systems
NPRM	Notice of Proposed Rule
	Making (USA)
NTSEL	National Traffic Safety and
TTOLL	Environment Laboratory
	(Japan)
~	
<u>о</u> ос	Occipital Condyles
ODB	Offset Deformable Barrier
OICA	Organisation Internationale
UICA	des Constructeurs
	d'Automobiles
OLC	Occupant Load Criterion
OMDB	Oblique Moving Deformable
011100	Barrier
OoP	Out of Position
OSM	Occupant Status Monitoring
Р	
PADI	Procedures for the assembly
I ADI	disassembly and inspection
PAEB	Pedestrian Automatic
I AED	Emergency Braking
PCL	Posterior Cruciate Ligament
PDB (1)	Partnership for
(+)	Dummytechnology and
	Biomechanics
PDB (2)	Progressive Deformable
	Barrier
PDC	Park Distance Control
PDI	Pedestrian Detection
	Impactor
PEAS	Primary Energy Absorbing
	Structure
PLI	Pedestrian Legform Impactor
PMA	Parking and Maneuvering
	Assistant
PMD	Photonic Mixer Device
PMHS	Post Mortem Human
	Subjects
PMTO	Post Mortal Test Object
	,

15	
PNCAP	Primary New Car Assessment Programme
PoC	Point of Collision
PP	Pedestrian Protection
PPA	Pedestrian Protection Airbag
PPAD	Partner Protection
	Assessment Deformation
PSPF	Pubic Symphysis Peak Force
PTS	Poly Trauma Score
PTW	Powered Two Wheeler
R	
Radar	Radio Detection and Ranging
RCAR	Research Council for
NCAN	Automobile Repairs
RCTA	Rear Cross Traffic Alert
REX	Range Extender
RFCRS	Rearward Facing Child
ni cho	Restraint System
RHD	Right Hand Drive
RID	Rear Impact Dummy
RR	Repeatability &
	Reproducibility
c	, ,
S .O	Statutory Order
SA	Safety Assist (Euro NCAP)
SAE	Society of Automotive
JAL	Engineers
SAS	Speed Assistance System
SAT	Safety Assist Technology
SB	Seat Back
SBR	Seat Belt Reminder
SD	Standard Deviation
SEAS	Secondary Energy Absorbing
	Structure
SgRP	Seating Reference Point
SID	Side Impact Dummy
SLD	Speed Limitation Device
SLIF	Speed Limit Information
	Function
SOB	Small Overlap Barrier (IIHS)
SRA	Swedish Road Administration
SRP	Seat Reference Point
SRS	Supplementary Restraint
	System
SSF	Static Stability Factor (U.S.
CCD	NCAP, KNCAP)
SSR	
CT	Speed Sign Recognition
ST	Sensing Time
STNI	Sensing Time Soft Tissue Neck Injury
	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite
STNI SUFEHM	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model
STNI SUFEHM SUV	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle
STNI SUFEHM	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio
STNI SUFEHM SUV	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle
STNI SUFEHM SUV SWR T	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio (Roof Crush)
STNI SUFEHM SWR TA	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio (Roof Crush) Type Approval
STNI SUFEHM SUV SWR T	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio (Roof Crush) Type Approval Technical Committee - Motor
STNI SUFEHM SWR T TA TCMV	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio (Roof Crush) Type Approval Technical Committee - Motor Vehicles (EU)
STNI SUFEHM SWR T TA TCMV TEG	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio (Roof Crush) Type Approval Technical Committee - Motor Vehicles (EU) Technical Evaluation Group
STNI SUFEHM SUV SWR T TA TCMV TEG TF BTA	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio (Roof Crush) Type Approval Technical Committee - Motor Vehicles (EU) Technical Evaluation Group Task Force Bumper Test Area
STNI SUFEHM SWR T TA TCMV TEG	Sensing Time Soft Tissue Neck Injury Strasbourg University Finite Element Head Model Sports Utility Vehicle Strength-to-weight Ratio (Roof Crush) Type Approval Technical Committee - Motor Vehicles (EU) Technical Evaluation Group

THOR	Test Device for Human Occupant Restraint
THUMS	Total Human Model for Safety
TIPT	Thorax Injury Prediction Tool
ToPl	Time of Pedestrian
	Identification
TOR	Takeover Request
TPL	Third Party Liability
	(Insurance)
TREAD	Transportation Recall,
	Enhancement, Accountability
TRL	and Documentation Transport Research
INL	Laboratory (UK)
TRT	Total Reaction/Response
	Time
TSP	Top Safety Pick (IIHS)
TT	Top Tether
TTB	Time to Brake
TTC	Time to Collision
TTD	Time to Decision
TTI	Thoracic Trauma Index
TTS	Time to Steer
U	
U.S. NCAP	United States New Car
	Assessment Program
UBM	Upper Body Mass
UL	Upper Leg
UMTRI	University of Michigan
	Transportation Research
	Institute
LINI	United Nations
UN	United Nations
UN USCAR	The United States Council for
USCAR	The United States Council for Automotive Research
USCAR UUT	The United States Council for
USCAR UUT V	The United States Council for Automotive Research Unit Under Test
USCAR UUT V VAN	The United States Council for Automotive Research Unit Under Test Vehicle Area Network
USCAR UUT VAN VC	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion
USCAR UUT VAN VC VDC	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control
USCAR UUT VAN VC	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian
USCAR UUT VAN VC VDC	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian Safety
USCAR UUT VAN VC VDC VERPS	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian
USCAR UUT VAN VC VDC VERPS VR	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian Safety Virtual Reality Vehicle Research & Test Center (NHTSA)
USCAR UUT VAN VC VDC VERPS VR VRTC VRU	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian Safety Virtual Reality Vehicle Research & Test Center (NHTSA) Vulnerable Road User
USCAR UUT VAN VC VDC VERPS VR VRTC	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian Safety Virtual Reality Vehicle Research & Test Center (NHTSA) Vulnerable Road User Vehicle Safety Score (U.S.
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USCAR UUT VAN VC VDC VERPS VR VRTC VRU VSS WAD (1) WAD (2) WG	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian Safety Virtual Reality Vehicle Research & Test Center (NHTSA) Vulnerable Road User Vehicle Safety Score (U.S. NCAP) Wrap Around Distance Whiplash Associated Disorders Working Group
USCAR UUT VAN VC VDC VERPS VR VRTC VRU VSS VRU VSS VRU VSS VRU VSS WAD (1) WAD (2) WG WP	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Dynamics Control Vehicle Related Pedestrian Safety Virtual Reality Vehicle Research & Test Center (NHTSA) Vulnerable Road User Vehicle Safety Score (U.S. NCAP) Wrap Around Distance Whiplash Associated Disorders Working Group Working Party
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USCAR UUT V VAN VC VDC VERPS VR VRTC VRU VSS WAD (1) WAD (2) WG WP WS WS5F	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian Safety Virtual Reality Vehicle Research & Test Center (NHTSA) Vulnerable Road User Vehicle Safety Score (U.S. NCAP) Wrap Around Distance Whiplash Associated Disorders Working Group Working Party World SID World SID 5th%ile Female Dummy
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USCAR UUT V VAN VC VDC VERPS VR VRTC VRU VSS WAD (1) WAD (2) WG WP WS WS5F	The United States Council for Automotive Research Unit Under Test Vehicle Area Network Viscous Criterion Vehicle Dynamics Control Vehicle Related Pedestrian Safety Virtual Reality Vehicle Research & Test Center (NHTSA) Vulnerable Road User Vehicle Safety Score (U.S. NCAP) Wrap Around Distance Whiplash Associated Disorders Working Group Working Party World SID World SID 5th%ile Female Dummy



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Index

<u>A</u>

Abbreviations 183 ACI 126 Active Safety 129,130 ADR 20 AEB 130 132 143 146 149 150 152 154,155,158,161,162,164 AES 164 Airbag 77,80 ANCAP 32.45.134 aPLI 126.128 Artificial Intelligence 140 ASEAN NCAP 29, 30, 59, 113, 130, 134,157 ASV 132 Automated Driving 129, 135, 137, 139.140 Auto[nom]Mobil 139

В

Bachem, Harald 17, 104 Backes, André 181, 182 Balancing 45 BASt 138 Battery 22 Baumgärtner, Timo 173 Bharat NCAP 30, 71, 157 Biomechanics 168 BioRID 107, 120 Brain Injury Criterion 122 BrIC 122 Brolin, Karin 168 Bumper Test 105

<u>C</u>

CAE Grand Challenge 166 Camera 118 Child Occupant Protection 112 China 13 C-IASI 29,30,157 CMVSS 208 76 C-NCAP 29,30,60,62,63,132,134, 157,161 Commercial Vehicles 17 Compatibility 34,37 Composites 176,177



Crash Imminent Braking 159 Crash-Sensing 85 Crash Simulation 74,177,178,179, 180 Crashworthiness 74 Creamer, John 18,26,137

D

Data Acquisition 117 Data-based Development 141 Driver Assistance 130,140 Dual Rating 45 Duddeck, Fabian 172 Dummy 120,124,125

Ε

eCall 44 Efficiency 175 Eickhoff, Burkhard 84 Ejection Mitigation 63,92 Electric Vehicles 22,25 Emergency Lane Keeping 155,156 Emergency Steering Support 144, 148,154 ES-2 120 ESC 129,130,142,156 Euro NCAP 27,30,32,45,86,96,100, 110,112,157 Euro SID 120 Extrication 44

F

Far Side Occupant 41 FCW 164 Finck, Maren 102, 103 Flex PLI 98 126 FMVSS 18 26 FMVSS 126 142 FMVSS 201 94.95 FMVSS 208 76, 77, 78 FMVSS 214 86,87,88 FMVSS 216a 75 FMVSS 226 92 FMVSS 305 24 Foams 179 Forward Collision Warning 132, 159 Frank. Thomas 109 Frontal Impact 32, 39, 56, 76, 78, 81

Front Crash Prevention 158 Fuel cell 22

G

Gärtner, Torsten 95 Gautrain, Louis 73 Gese, Helmut 178 Global NCAP 30 Golowko, Kai 77,79 Grid Method 100 Groesch, Lothar 85,135 GTR 18 GTR 9 96 GTR 14 86

H

Harzheim, Lothar 174 Head Impact 94,95 Head Restraints 50 HIC 122 Hinterhölzl, Roland 176 HRMD 107 Hübner, Sandro 80 Human Body Models 168 Hybrid III (HIII) 120

I

IIHS 28,30,50,75,86,108,132,134, 157,158 IIWPG 108 India 19 Inhouse Seminars 12 Injury Mechanisms 168 Injury Risk Curves 48 Insurance Tests 105 Interior Development 173 i-VISTA 164

J

JNCAP 29, 30, 64, 66, 96, 132, 134, 157 Joints 180 Justen, Rainer 22

Κ

Karall, Thomas 177 Kinsky, Thomas 18 KMVSS 20,21 KNCAP 29,67,68,70,96,114,132,134



Knee Mapping 38 Kolling, Stefan 179

Kuhn, Andreas 140, 141

L

Lane Departure Warning 132, 155, 165 Lane Keep Assist 155, 162 Latin NCAP 28, 30, 55, 59, 113, 130, 134, 157 Lightweight Design 74, 170

Lohrmann, Hans-Georg 72 Low-Speed Crashes 104

M

Machine Learning 140,182 Material Models 177,178,179 MCL 126 Meißner, Norman 90 Metals 178 MPDB 32,37,60 Müller, Gerd 129 Multi Collision Brake 44 Multi-point Thoracic Injury Criterion 122 MUSE 149

Ν

NCAP 28, 30, 32, 46, 48, 49, 134, 157 New Energy Vehicles 13 NHTSA 26, 138

0

Occupant Protection 84 Occupant to Occupant Protection 42 OLC 34 OMDB 79 Optimization 174 Out-of-Position 77

Ρ

Passive Safety 16 PCL 126 P-Dummy 120 Pedestrian Protection 96,102,126, 128 Plastics 173,179 Pole Side Impact 86

Post Crash 44

Powered Two Wheelers 149 PraxisConference Pedestrian Protection 97 PraxisConference Rear Impact- Seats - Whiplash 107 PraxisConference Safety Assist 136 Product Liability 26,72 Programming 181 Python 181,182

Q

Q-Dummy 113, 120, 124

R

Rating 49.59 RCAR 104,105 Rear Automatic Braking 160 Rear Impact 107 Rear Seat 83.84 Regulations 18, 19, 20 Rescue 44 Rescue Sheet 44 Restraint System 80 Restraint Systems 77,79 Reuter, Ralf 16 Risk 175 Roadmap 2030 27 Robust Design 172 Rollover 132 Roof Crush 51.73.75 Rother, Klemens 175

<u>S</u>

SAE 138 SafetyExpo 14 SafetyTesting 116 SafetyUpDate 15 SafetyWeek 14 Sandner, Volker 37, 38 Scenario-based Development 141 Schnottale, Britta 111 Seat 107 Seat Adjustments 88 Seat Belt Reminder 63 Seats 107 Seeck, Andre 30, 157 Self-Certification 26



Seminar Guide 6 Sensors 85,135 SID 120 Side Impact 40,86,88,90,91 SID-IIs 120 Sine with Dwell 142 Slowly-Increasing-Steer 142 Small Overlap 52,54 Sommer, Silke 180 Static Vehicle Safety Tests 73

<u>T</u>

Table of Contents 8,9 THOR 79,122,125 Top Safety Pick 51 Turn Across Path 154

<u>U</u>

UN R21 94,95 UN R94 20,25 UN R95 21,25,86 UN R100 25 UN R127 96,98 UN R135 21 UN Regulations 18,115 U.S. NCAP 28,30,46,48,49,86,132, 134,157,159,160

V

Validation 141 Vehicle Classification 115 Vehicle Safety Score 49 VRU 143,146

W

Whiplash 62, 106, 107, 109, 110 Wild, Thomas 117 Wolter, Stephanie 90 WorldSID 88, 120, 125

Seminar Calendar 2021



January	February	March
1 Fr New Year	1 Mo Python Programming 2 > p. 181	1 Mo Safety and Crash-Test Regulations p. 18
2 Sa	2 Tu Artificial Intelligence & Machine Learning	2 Tu
3 Su	3 We	3 We
4 Mo	4 Th	4 Th
5 Tu	5 Fr	5 Fr 💦
6 We Epiphany	6 Sa	6 Sa
7 Th	7 Su	7 Su
8 Fr	8 Mo Frontal Restraint Systems- Advanced - p. 79	8 Mo Static Vehicle Safety Tests p. 73
9 Sa	9 Tu Safety and Crash-Test Regulations 18	9 Tu Modeling of Joints in Crash Simulation > p.180
10 Su	10 We Safety of Commercial Vehicles p. 17	10 We Development of Frontal Restraint Systems p. 77
11 Mo	11 Th Occupant Protection in Frontal Crashes	11 Th
12 Tu	12 Fr	12 Fr
13 We	13 Sa	13 Sa
14 Th	14 Su	14 Su
15 Fr	15 Mo	15 Mo Pedestrian Protection p. 102
16 Sa	16 Tu Material Models of Composites 200 p. 177	16 Tu Euro NCAP MPDB Frontal Crash Workshop
17 Su	17 We	17 We Crash-Sensing and Intelligent Restraints
18 Mo Euro NCAP - Compact www.carhs.de	18 Th	18 Th Material Models of Plastics and Foams
19 Tu Material Models of Metals > p. 178	19 Fr	19 Fr Design of Composite Structures - p. 176
20 We	20 Sa	20 Sa
21 Th	21 Su	21 Su
22 Fr	22 Mo Product Liability p. 72	22 Mo
23 Sa	Whipidsh leseng and evaluation 200	23 Tu
24 Su	24 We Ejection Mitigation www.carhs.de	24 We
25 Mo	25 Th Structural Optimization p. 174	25 Th
26 Tu Data Acquisition in Safety Testing > p. 117	26 Fr Introduction to Passive Safety p. 16	26 Fr Head Impact on Vehicle Interiors p. 95
27 We Python Programming p. 181	27 Sa	27 Sa
28 Th Frontal Restraint Systems p. 77	28 Su	28 Su
29 Fr		29 Mo
30 Sa		30 Tu
31 Su		31 We

1 Th 1 Sa Labor Day 1 Tu 2 Fr Good Friday 2 Su 2 We 3 Sa 3 Mo Development, Validation & Safeguarding of AD 3 Th Corpus Christi 4 Su Easter 4 Tu Python based Machine Learning > p. 182 4 Fr 5 Mo Easter 5 We 5 Sa 6 Su 6 Su	
3 Sa 3 Mo Development, Validation & Safeguarding of AD 3 Th Corpus Christi 4 Su Easter 4 Tu Python based Machine Learning 9, 182 4 Fr 5 Mo Easter 5 We 5 Sa 5 Sa 6 Tu 6 Th 6 Su 6 Su	
4 Su Easter 4 Tu Python based Machine Learning >>> 182 4 Fr 5 Mo Easter 5 We 5 Sa 5 Sa 6 Tu 6 Th 6 Su 5 Sa	
S Mo Easter S We 5 Sa 6 Tu 6 Th 6 Su	
6 Tu 6 Th 6 Su	
7 We 7 Fr Child Protection in Front and Side Impacts 111 7 Mo Pedestrian Protection 2 , p.	102
8 Th 8 Sa 8 Tu Product Liability >> 7.7	2
9 Fr 9 Su 9 We 9	
10 Sa 10 Mo 10 Th	
11 Su 11 Fr Worldw. Status of Automated V	/ehicle Policies
12 Mo Crashworthy and Lightweight Car Body 12 We 12 Sa	
13 Tu side Impact p. 90 13 Th Ascension of Christ 13 Su	
14 We Biomechanics & Human Body Models 14 Fr 14 Mo Introduction to Passive Safety	p. 16
15 Th Advances in Sensors for AD 15 Sa 15 Tu Development of Frontal Res	traint Systems
16 Fr 16 Su 16 We Introduction to Passive Safet	
17 Sa 17 Mo 17 Th Head Impact on Vehicle Interio	rs 200 p. 95
18 Tu 18 Fr	
19 Mo NCAP- New Car Assessment Programs 20 p. 30 19 We 19 Sa	
20 Tu 20 Th 20 Su	
21 We 21 Fr 21 Mo Early Design Maturity of Restraint ?	Systems systems p. 80
22 Th Vehicle Safety under Self-Certification 22 Sa 22 Tu Crash Safety of Hybrid and E	
23 Fr Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Electric Vehicles 23 Su Pentecost 23 We Crash Safety Of Hybrid and Safet	ent Programs
	www.carhs.de
25 Su 25 Tu 25 Fr	
26 Mo Introduction to Active Safety of Vehicles 26 We 26 Sa	
27 Tu 27 Th 27 Su	
28 We 28 Fr 28 Mo Artificial Intelligence & Machine Le	earning 2 > p. 140
	www.carhs.de
30 Fr 30 Su 30 We Safety and Crash-Test Regulation	ons 🗾 > p. 18
31 Mo	

Alzenau

Gaimersheim

Hanau

Landsberg a. Lech

Online

Würzburg

Seminar Calendar 2021



vlut	August	September
1 Th Euro NCAP MPDB Workshop > p. 37	1 Su	1 We Crash-Sensing and Intelligent Restraints
2 Fr	2 Mo	2 Th SafetyWeek 2021 p. 14
3 Sa	3 Tu	3 Fr
4 Su	4 We	4 Sa
5 Mo	5 Th	5 Su
6 Tu Crashworthy and Lightweight Car Body Design	6 Fr	6 Mo
7 We PraxisConference Pedestrian Protection	7 Sa	7 Tu Advances in Sensors for Automated Driving
8 Th Side Impact	8 Su	8 We
9 Fr	9 Mo	9 Th
10 Sa	10 Tu	10 Fr
11 Su	11 We	11 Sa
12 Mo	12 Th	12 Su
13 Tu	13 Fr	13 Mo
14 We	14 Sa	14 Tu Knee Mapping Workshop
15 Th Automotive Safety Summit Shanghai	15 Su	15 We
16 Fr	16 Mo	16 Th Material Models of Composites
17 Sa	17 Tu	17 Fr
18 Su	18 We	18 Sa
19 Mo	19 Th	19 Su
20 Tu	20 Fr	20 Mo Material Models of Plastics and Foams
21 We	21 Sa	21 Tu SafetyUpDate
22 Th	22 Su	22 We Whiplash Testing and Evaluation
23 Fr	23 Mo	23 Th Frontal Restraint Systems- Advanced
24 Sa	24 Tu	24 Fr Design of Composite Structures
25 Su	25 We	25 Sa
26 Mo	26 Th	26 Su
27 Tu	27 Fr	27 Mo Modeling of Joints in Crash Simulation
28 We	28 Sa	28 Tu Product Liability
29 Th	29 Su	29 We
30 Fr	30 Mo	30 Th NVH - Background, Practice & Simulation
31 Sa	31 Tu Introduction to Passive Safety	

October	November	December
1 Fr	1 Mo All Saints	1 We Python based Machine Learning p. 182
2 Sa	2 Tu Passenger Cars in Low-Speed Crashes p. 104	2 Th Crashworthy & Lightweight Car Body 74
3 Su German National Holiday	3 We Safety of Commercial Vehicles p. 17	3 Fr
4 Mo Additive Manufacturing Advanced www	4 Th Rear Seat Occupant Protection > p. 84	4 Sa
5 Tu Data Acquisition in Safety Testing p. 117	5 Fr	5 Su
6 We	6 Sa	6 Mo
7 Th Material Models of Metals p. 178	7 Su	7 Tu
8 Fr Head Impact on Vehicle Interiors > p. 95	8 Mo	8 We
9 Sa	9 Tu Safety and Crash-Test Regulations p. 18	9 Th
10 Su	10 We Safety of Hybrid and Electric Vehicles	10 Fr
11 Mo Early Design Maturity of Restraint Systems p. 80		
12 Tu Vehicle Safety under Self-Certification 20 p. 26	12 Fr Introduction to Active Safety of Vehicles > p. 129	12 Su
13 We	13 Sa	13 Mo
14 Th Worldwide Status of Automated Vehicle Policies	14 Su	14 Tu Euro NCAP UpDate 2021 p. 27
15 Fr	15 Mo Euro NCAP MPDB Workshop > p. 37	15 We
16 Sa	16 Tu Python Programming p. 181	16 Th
17 Su	17 We Development, Validation & Safeguarding of AD	17 Fr
18 Mo	18 Th Ejection Mitigation www.carhs.de	18 Sa
19 Tu automotive CAE Grand Challenge p. 166	19 Fr Frontal Restraint Systems p. 77	19 Su
20 We Side Impact > p. 90	20 Sa	20 Mo
21 Th Design & Simulation of Vehicle Vibration	21 Su	21 Tu
22 Fr	22 Mo Design for Durability www.carhs.de	22 We
23 Sa 24 Su	23 Tu Introduction to Passive Safety > p. 16 24 We Structural Optimization > p. 174	23 Th
	Structural Optimization 5, 174	24 Fr Christmas Eve
25 Mo Pedestrian Protection & Low Speed Crash > p.103 26 Tu Artificial Intelligence and Machine Learning > 140		25 Sa Christmas 26 Su Christmas
The and a second and a second se		26 Su Christmas
27 We New Car Assessment Programs p. 30 28 Th	27 Sa 28 Su	27 Mo 28 Tu
28 In 29 Fr		28 IU 29 We
30 Sa	· · · · · · · · · · · · · · · · · · ·	30 Th
30 Sa 31 Su	30 Tu Functional Safety www.carhs.de	31 Fr New Year's Eve
51.50		JTH NEW ICOLUCYC

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