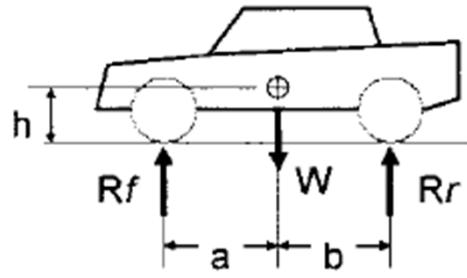


Figure 2.16 (1)

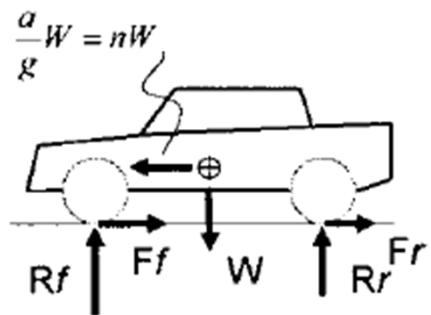
static



$$\begin{cases} 2(R_f + R_r) = W \\ bR_r - aR_f = 0 \rightarrow b\left(\frac{W}{2} - R_f\right) - aR_f = 0 \end{cases}$$

$$\rightarrow \begin{cases} R_f = \left(\frac{b}{a+b}\right)\frac{W}{2} \\ R_r = \left(\frac{a}{a+b}\right)\frac{W}{2} \end{cases}$$

braking



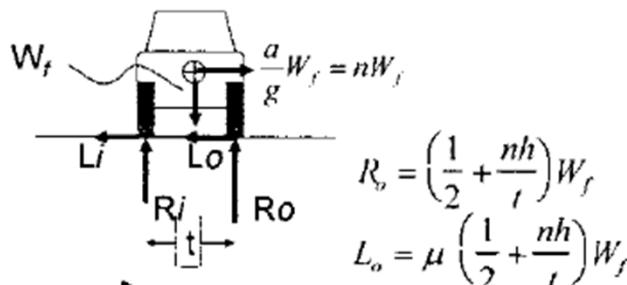
$$\begin{cases} \frac{a}{g}W = nW \\ 2(F_f + F_r) = 2\mu(R_f + R_r) = nW \rightarrow R_r = \frac{nW}{2\mu} - R_f = \left(\frac{n}{\mu} - \frac{b+nh}{a+b}\right)\frac{W}{2} \\ 2R_f(a+b) = nWh + Wb \rightarrow R_f = \left(\frac{b+nh}{a+b}\right)\frac{W}{2} \end{cases}$$

$$\rightarrow \begin{cases} F_f = \mu R_f = \mu\left(\frac{b+nh}{a+b}\right)\frac{W}{2} \\ F_r = \mu R_r = \mu\left(\frac{n}{\mu} - \frac{b+nh}{a+b}\right)\frac{W}{2} \end{cases}$$

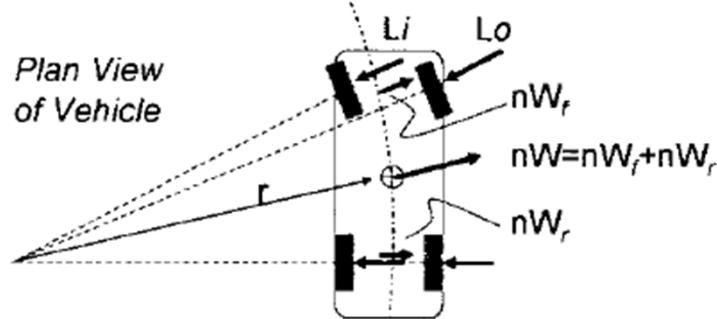
Figure 2.16 (2)

cornering

View of Front Axle

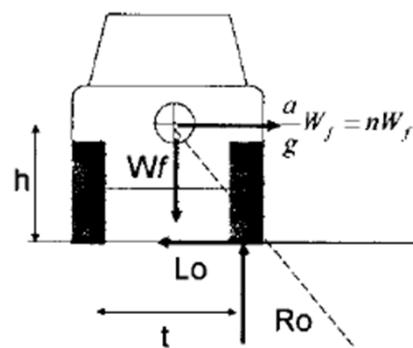


Plan View of Vehicle



Incipient rollover

Vehicle Structure



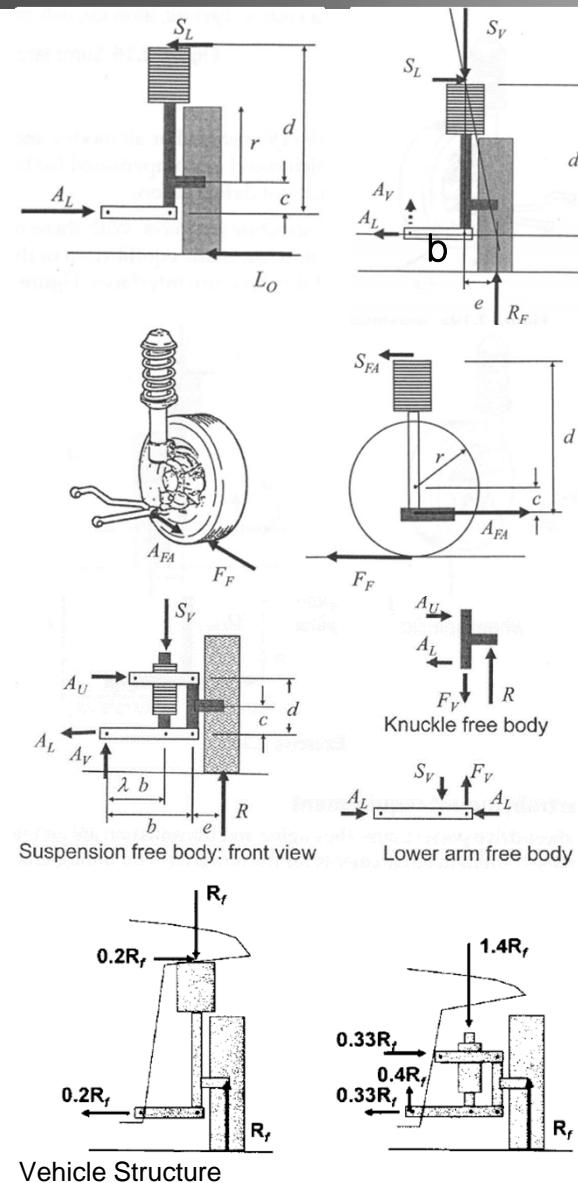
$$\begin{cases} R_i + R_o = W_f \\ L_i + L_o = nW_f \\ L_i = \mu R_i, L_o = \mu R_o \\ \frac{t}{2}(R_o - R_i) - h(L_i + L_o) = 0 \\ \rightarrow \frac{t}{2}(R_o - W_f + R_o) - h(nW_f) = 0 \\ \rightarrow tR_o = \left(\frac{t}{2} + nh\right)W_f \\ \rightarrow R_o = \left(\frac{1}{2} + \frac{nh}{t}\right)W_f \end{cases}$$

$$\begin{cases} R_i = 0, R_o = W_f \\ L_o = nW_f \\ \frac{t}{2}R_o - hL_o = 0 \rightarrow L_o = \frac{t}{2h}R_o \end{cases}$$

$$\rightarrow n = \frac{t}{2h}$$

Exercises - 2

2.5 Struct vs.SLA



Struct

For the maximum lateral tire patch load during rollover mode

$$\begin{aligned} M_{@A_L}: & S_L d - (r - c)L_0 = 0 \\ \rightarrow & S_L = \left(\frac{r - c}{d} \right) L_0 \\ M_{@S_L}: & A_L d - (d + (r - c))L_0 = 0 \\ \rightarrow & A_L = \left(\frac{r - c}{d} + 1 \right) L_0 \end{aligned}$$

For the maximum fore-aft tire patch load during braking mode

$$\begin{aligned} M_{@A_FA}: & F_F(r - c) - dS_{FA} = 0 \\ \rightarrow & S_{FA} = \left(\frac{r - c}{d} \right) F_F \\ M_{@S_{FA}}: & A_{FA}d - (d + (r - c))F_F = 0 \\ \rightarrow & A_{FA} = \left(\frac{r - c}{d} + 1 \right) F_F \end{aligned}$$

For the maximum vertical tire patch load during bump mode

$$\begin{aligned} F_x: & A_L - S_L = 0 \rightarrow S_L = A_L \\ F_y: & R_F - S_V - A_V = 0 \rightarrow S_V = R_F - A_V \\ \text{if } & A_V = 0 (\text{or } S_V \gg A_V), \quad S_V = R_F \end{aligned}$$

SLA

1) S_V

$$F_x: A_U - A_L = 0 \rightarrow A_U = A_L$$

$$F_y: S_V - A_V - R = 0 \rightarrow S_V = R + A_V$$

$$M_{@lowerarm,F_V}: bA_V - (b - \lambda b)S_V = 0 \rightarrow A_V = (1 - \lambda)S_V$$

$$\rightarrow S_V - R = (1 - \lambda)S_V \rightarrow S_V = \frac{1}{\lambda}R$$

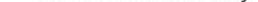
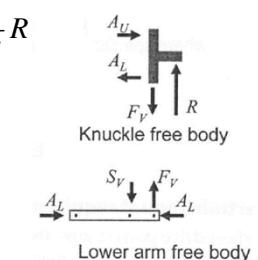
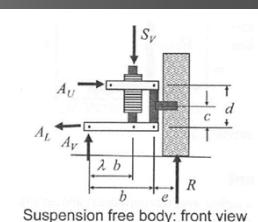
2) A_U

$$M_{@knuckle,F_V}: eR - dA_U = 0 \rightarrow A_U = \frac{e}{d}R$$

3) A_L, A_V

$$A_L = A_U = \frac{e}{d}R$$

$$\begin{aligned} A_V = A_V &= (1 - \lambda)S_V = (1 - \lambda)\frac{1}{\lambda}R \\ &= \left(\frac{1}{\lambda} - 1 \right)R \end{aligned}$$



$\lambda = 0.7$ 인 경우

$$\text{Strut : } S_V = R, \quad \text{SLA : } \frac{1}{\lambda}R = \frac{1}{0.7}R \approx 1.43R$$

SLA가 Struct보다 S_V (spring-shock maximum load)가 1.43배 커서 우수함