

Motorcycle Cooling Fin Harley-Davidson



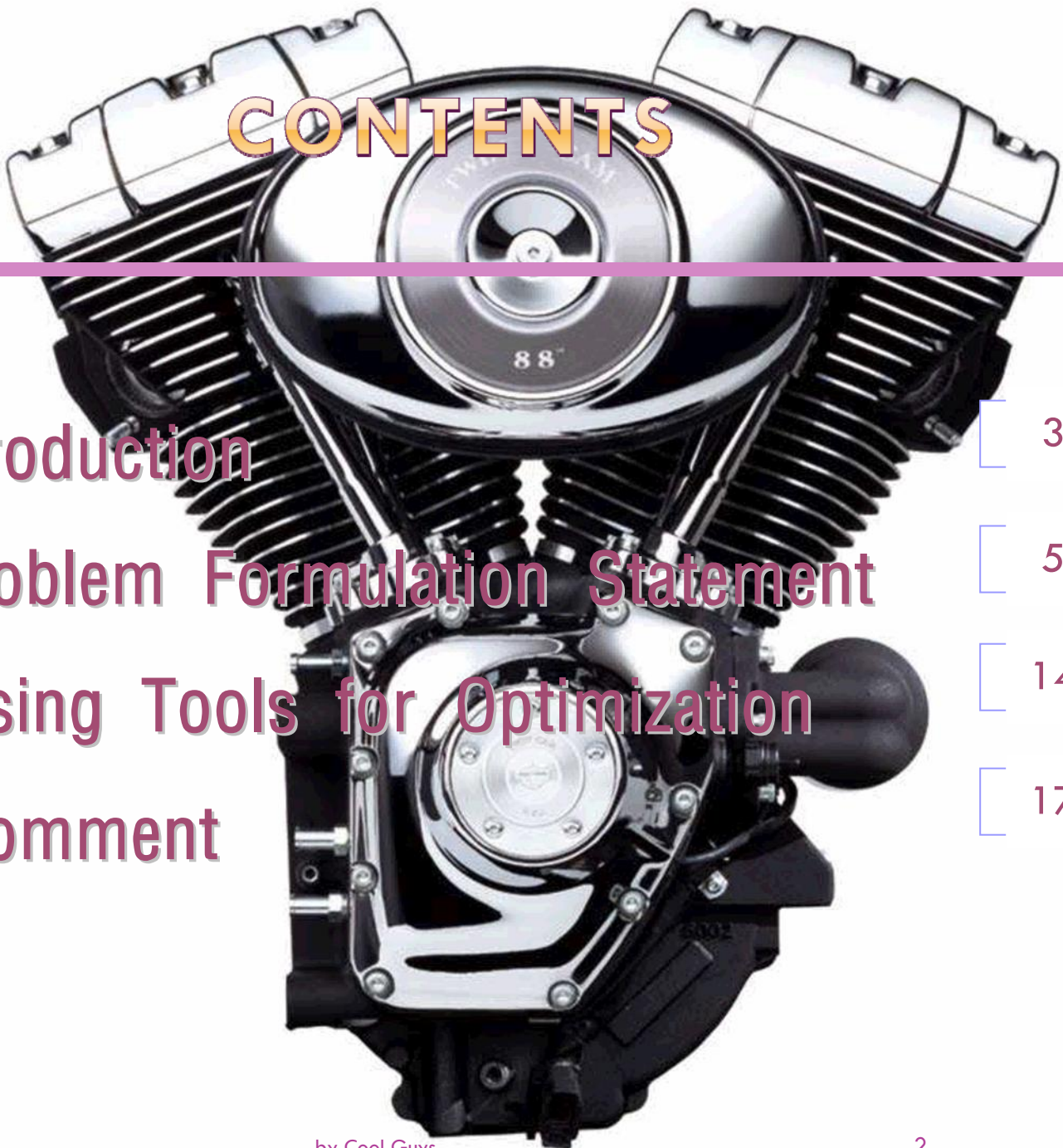
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CONTENTS



I. Introduction

[3]

II. Problem Formulation Statement

[5]

III. Using Tools for Optimization

[14]

IV. Comment

[17]

INTRODUCTION

- V-twin com engine and cooling fin

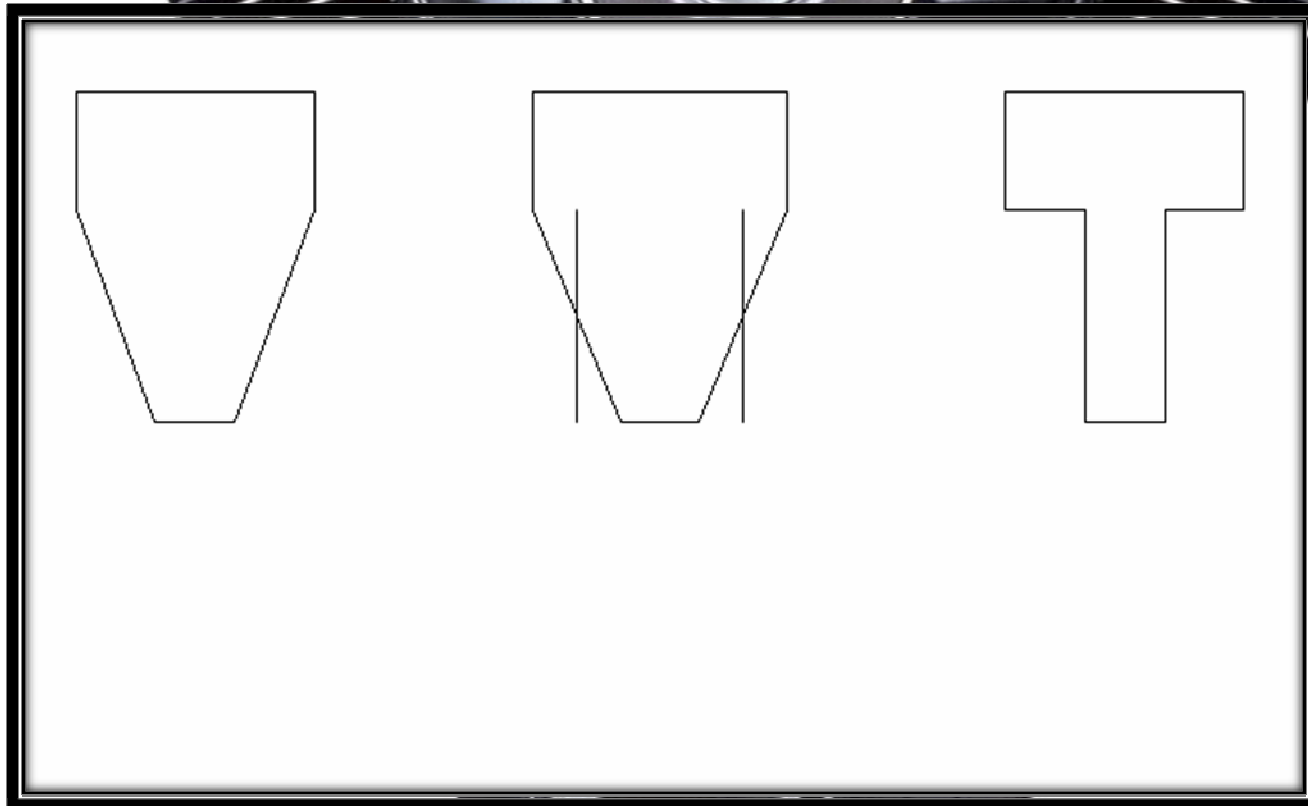


- Displacement 1150 cm^3
- Bore 95.18 mm
- Stroke 101.52 mm
- Torque 115.0 Nm 3000rpm

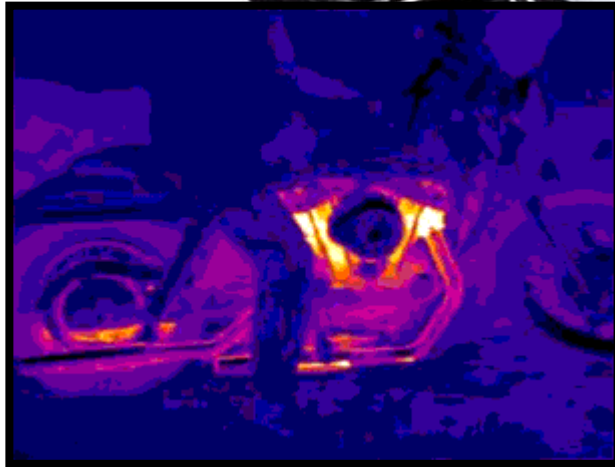
- Heat transfer in engine and fin



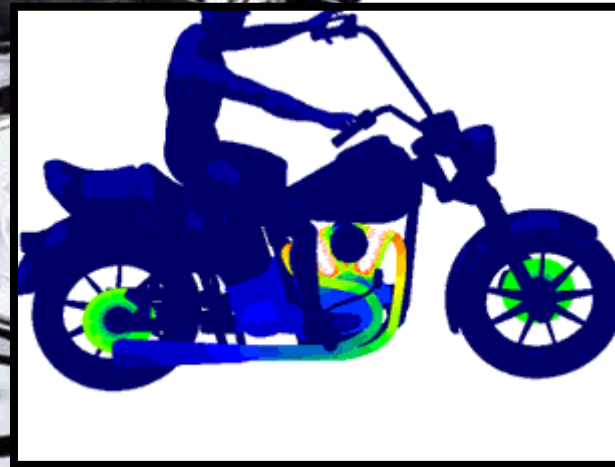
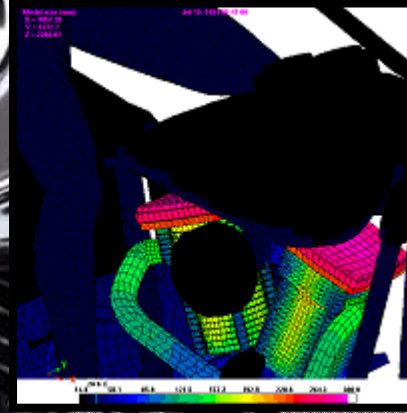
SIMPLIFICATION



REAL & MODELING



Thermal Real Image



Thermal Modeling Image

STEP 1 : PROBLEM STATEMENT

- Design a cooling fin of Harley-Davidson
- Minimize the cost
- Cost directly related to the volume of aluminum
- **Assumption**
 - The number of Fins : 20
 - Fin's efficiency $\geq 95\%$
 - Steady-state
 - One-Dimensional

STEP 2

: DATA AND INFORMATION COLLECTION

- 2024 T-6 Aluminum alloy

Density $\rho = 2770 \text{ kg/m}^3$ at 295K

Allowable stress $\sigma = 400 \text{ MPa}$

Conductive efficient $k = 172 \text{ W/mK}$

- Cylinder

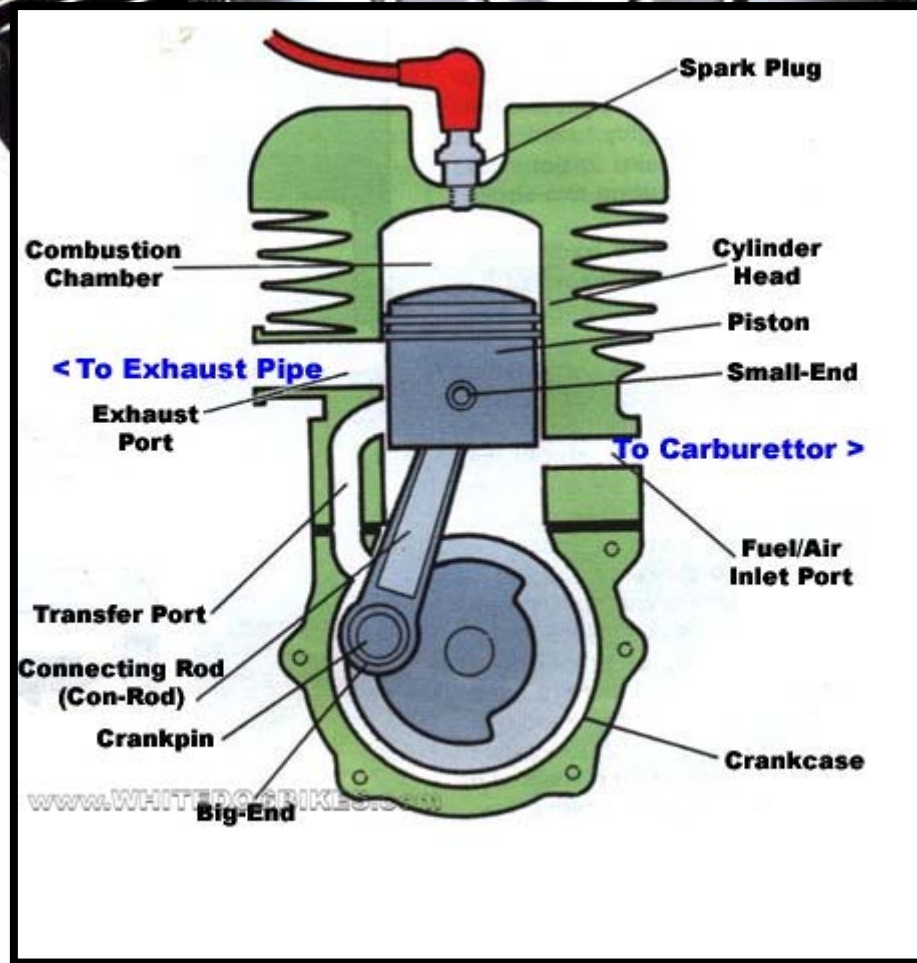
$$A_p = \frac{\pi}{4} B^2, V_d = \frac{\pi}{4} B^2 S$$

B:bore, S:stroke

A_p :area of cylinder, V_d :volume of cylinder

$$Re = \frac{(\dot{m}_a + \dot{m}_g) B}{A_p \mu_g} \quad (\dot{m}_a : \text{mass flow of air}, \dot{m}_g : \text{mass flow of gas})$$

CYLINDER IN ENGINE



STEP 2

: DATA AND INFORMATION COLLECTION

- Convection of gas & air

$$Nu = \frac{h_{\text{gas}} L}{k_g} = f(Re) \quad \text{? Nusselt number}$$

$$\dot{q} = h_{\text{gas}} \Delta T$$

$$\dot{Q} = A \dot{q} = \pi B S \dot{q}$$

$$T_o - T_i = \dot{Q} \frac{\ln(r_o/r_i)}{2\pi k L} \quad \text{? heat transfer at fin}$$

$$Nu = \frac{h_{\text{air}} L}{k} = 0.664 Re^{0.5} Pr^{1/3} \quad (Re < 5 \times 10^5)$$

$$h_{\text{free}} = 1.4 \left(\frac{\Delta T}{L} \right)^{1/4}$$

STEP 2

: DATA AND INFORMATION COLLECTION

- Area of fin & unfin

$$A_{1-fin} = 9 \times 2 \left[(0.184m + 2L + t)^2 - (0.184m)^2 \right]$$

$$A_{1-unfin} = 4 \times 0.184m(0.002m - 9t)$$

$$A_{2-fin} = 11 \times 2 \left[(0.141m + 2L + t)^2 - (0.141m)^2 \right]$$

$$A_{2-unfin} = 4 \times 0.141m(0.018m - 11t)$$

STEP 2

: DATA AND INFORMATION COLLECTION

- Stress at fin

$$\sigma_{fin} \leq \sigma_a$$

$$\sigma_{fin} = \frac{Mc}{I} = \frac{FL(w/2)}{\frac{1}{12}(w+L)^3}$$

M : moment at fin

c : distance from neutral axis

I : moment of inertia

STEP 3 : DESIGN VARIABLES

- ⦿ t : thickness of the fin [m]
- ⦿ L : length of the fin [m]

STEP 4 : COST FUNCTION

total cost = $(A_{fin1} + A_{fin2})t\rho c_{scost}$ (\$)

$$f = (A_{fin1} + A_{fin2})t\rho$$

STEP 5 : CONSTRAINTS

- There are five inequality constraints

$$g_1 : -A_{\text{total}} h(1-L) + Q_{\text{cool}} \leq 0$$

$$g_2 : (L + \frac{1}{2}t) \sqrt{\frac{h}{kt}} - 0.17647 \leq 0$$

$$g_3 : \sigma - \sigma_a \leq 0$$

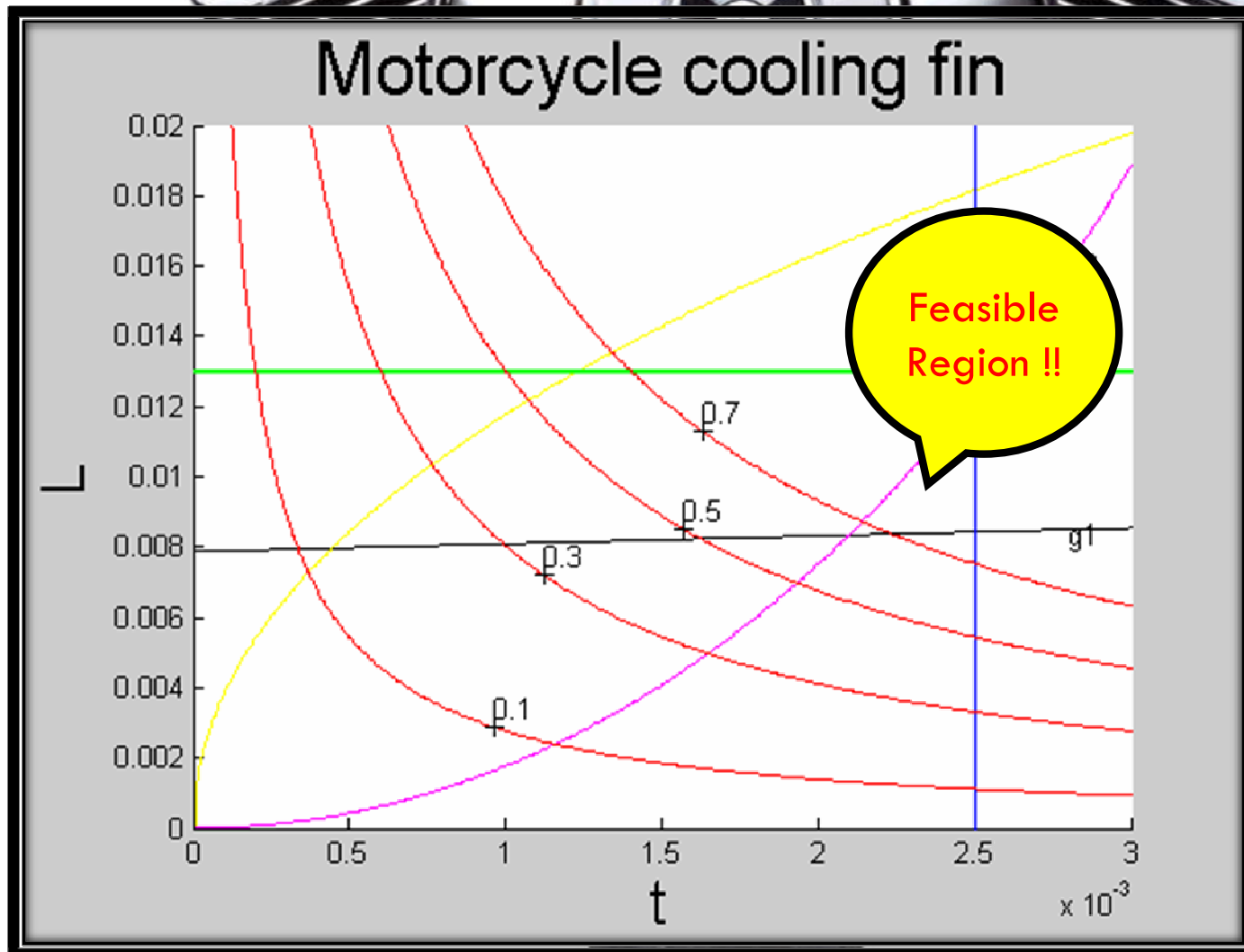
$$g_4 : L - L_a \leq 0$$

$$g_5 : 3t - \frac{h-21t}{21} \leq 0$$

USING MATLAB-SOURCE

```
>> [t,L]=meshgrid(0:0.00001:0.003,0:0.0001:0.02);
a=0.184;
b=0.141;
t1=183.3;
t2=185.5;
ti=25;
h=96.6;
f=2770.+(9.*((a+2.*L).^2-a^2)+11.*((b+2.*L).^2-b^2)).*t;
g1=-((18.*((a+2.*L+t./2).^2-a^2)+0.95+4*a.*(0.092-9.*t))*h*(t1-ti)-(22.*((b+2.*L+t./2).^2-b^2)+0.95+4*b.*(0.118-11.*t))*h*(t2-ti)+1957;
g2=(L+t./2).*sqrt(h./((177.*t))-0.17647;
g3=42379.*L./(((0.184+2.*L).*t.^2)-4000000000;
g4=L-0.013;
g5=4.*t-0.01;
cla reset
axis auto
hold on
xlabel('t','fontsize',20'),ylabel('L','fontsize',20')
title('Motorcycle cooling fin','fontsize',25')
hold on
cv=[0 0.00001];
const1=contour(t,L,g1,cv,'k');
const2=contour(t,L,g2,cv,'y');
const3=contour(t,L,g3,cv,'m');
const4=contour(t,L,g4,cv,'g');
const5=contour(t,L,g5,cv,'b');
fv=[0.1 0.3 0.5 0.7];
fs=contour(t,L,f,fv,'r');
clabel(fs)
text(0.0028,0.016,'g3')
text(0.0028,0.0083,'g1')
>> |
```


USING MATLAB(GRAPH)



USING MATLAB(SOLVER)

- Determine initial value from the graph

```
>> %그래프를 보고 초기값 [0.002,0.008] 로 정함;  
>> x0=[0.002,0.008];  
>> x=fmincon('func',x0,[],[],[],[],[],[],'const')
```

- The value of t & l

```
x =  
  
0.0021    0.0083
```

- Minimum Volume

```
>> f=2770*(9*((a+2+0.0083)^2-a^2)+11*((b+2+0.0083)^2-b^2))*0.0021  
  
f =  
  
0.6514
```

COMMENT & REFERENCE



- Comment

- ① 기존 모델의 형상을 그대로 따라가진 못했지만 편의상 예외적인 경우의 비슷한 값으로 나왔다.
- ② 그래프를 보고 대략적인 온도값을 예측할 수 있었고 MATLAB의 function기능을 이용하여 최소가 되는 값을 찾아볼 수 있었다.
- ③ 대류열전달 계수를 구하는데 있어서 더 엄밀한 기준이 필요하다.
- ④ 충격량에 대한 실험이나 해석이 부족하였다.

- Rederence

- 내연기관공학 /Pulkrabek
- Heat transfer /Yunus A cengel
- 재료역학 /Ferdinand. P Beer
- Internet -<http://nospam.thermodyna1.com/>
- <http://www.totalmotorcycle.com/>
- <http://www.harley-davidson.com/> 드드
- 2004 년도 김동완/ 박상인-김강원, recent 참고