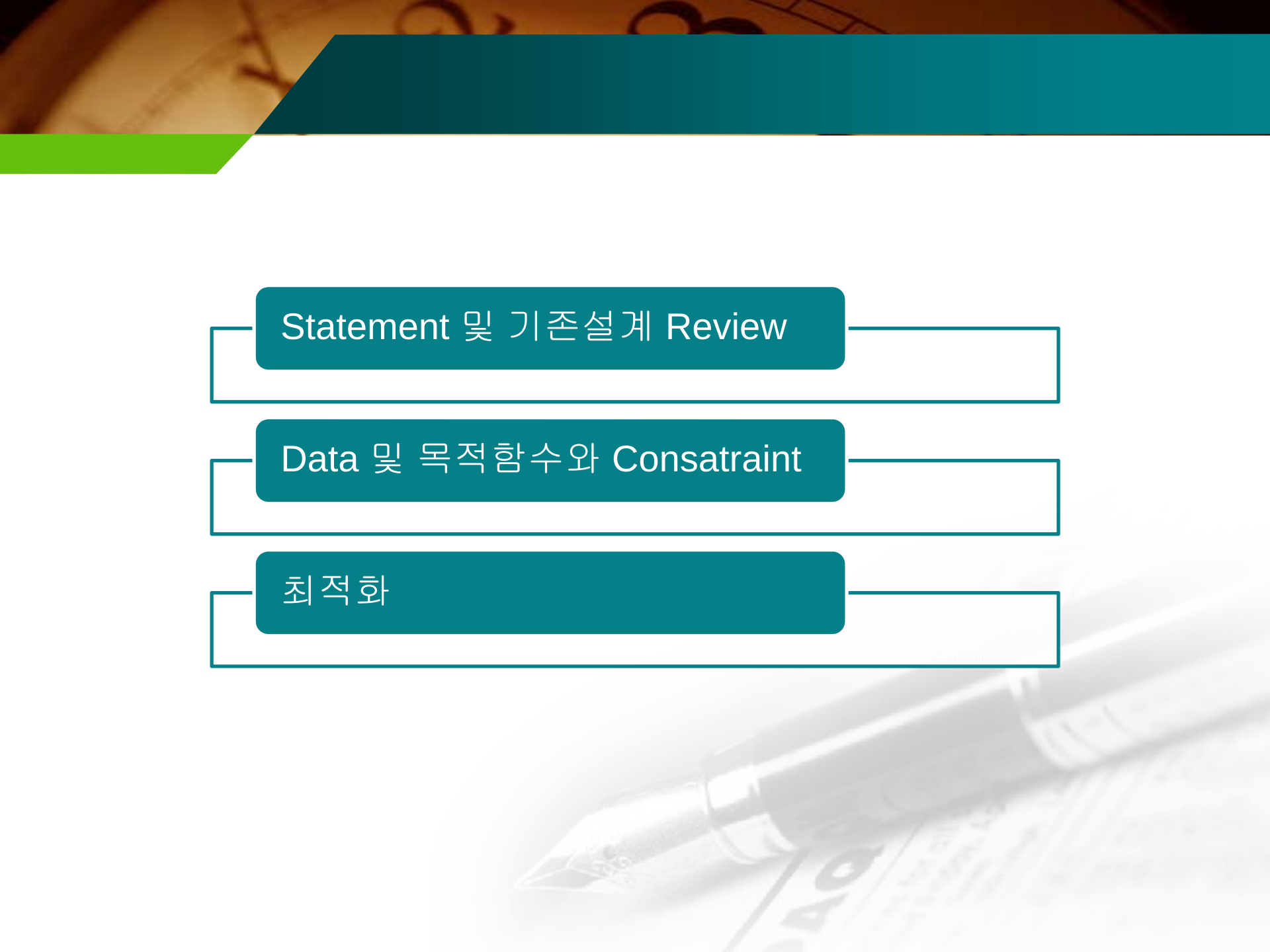


Company
LOGO

청소를 편하게

2007006656 주경훈



Statement 및 기존설계 Review

Data 및 목적함수와 Consatrant

최적화

Statement

걸레의 대의 재료가 될 수 있는 재료는 3가지이다. 대가 사용되는 조건은 스스로 정하고 변수 값은 두 개의 대의 반지름과 두께로 하라. 걸레의 수명은 무한이 되도록 하고 대의 질량을 최소화 할 수 있도록 최적의 변수들을 설계한 후 재료를 선정하고 그 질량을 구해라.



기존 프로젝트

F_2



$$\mu\{(m_1 + m_2)g + F_1 + F_2 \sin \theta\}$$

$$F_1 + F_2 \sin \theta + (m_1 + m_2)g$$

1 번에 작용하는 힘

$$F_1, F_2, \mu\{(m_1 + m_2)g + F_1 + F_2 \sin \theta\}, M$$

$$\sigma_1 = \frac{\sqrt{[\mu\{(m_1 + m_2)g + F_1 + F_2 \sin \theta\}]^2 + F_2^2 \sin^2 \theta + F_1 \sin \theta}}{A_1}$$

$$\sigma_2 = \frac{Mc}{I} \quad I = \frac{\pi R^3 t}{4}$$

$$\therefore \sigma_1 + \sigma_2 \leq \sigma_a$$

$$\frac{\sqrt{[\mu\{(m_1 + m_2)g + F_1 + F_2 \sin \theta\}]^2 + F_2^2 \sin^2 \theta + F_1 \sin \theta}}{A_1} + \frac{Mc}{I} \leq \sigma_a$$

2번에 작용하는 힘

F_2, M

$$\sigma_3 = \frac{\sqrt{[\mu\{(m_1 + m_2)g + F_1 + F_2 \sin \theta\}]^2 + F_2^2 \sin^2 \theta}}{A_2}$$

$$\sigma_4 = \frac{Mc}{I}$$

$$\therefore \sigma_1 + \sigma_2 \leq \sigma_a$$

$$\frac{\sqrt{[\mu\{(m_1 + m_2)g + F_1 + F_2 \sin \theta\}]^2 + F_2^2 \sin^2 \theta}}{A_2} + \frac{Mc}{I} \leq \sigma_a$$

X' 방향 변형

$$\delta = \frac{PL}{AE}$$

가운데 점

$$F_1 \sin \theta + F_2 - \mu \{ (m_1 + m_2)g + F_1 + F_2 \sin \theta \} = P$$

2번이 늘어난 길이 = 1번이 줄어든 길이

$$\frac{PL}{A_2 E_2} = \frac{PL}{A_1 E_1} \implies \text{같은 재질 } E_2 = E_1$$

$A_2 = A_1$ 일 수밖에 없다. $\implies$ 두 값이 매우 작아서 무시할 만함

Y' 방향 변형



$$EIy'''' = -F_1 \cos \theta < x-L >^{-1}$$

$$EIy''' = -F_1 \cos \theta < x-L >^0 + C_1$$

$$EIy'' = -F_1 \cos \theta < x-L >^1 + C_1 x + C_2$$

$$EIy' = -\frac{1}{2} F_1 \cos \theta < x-L >^2 + \frac{1}{2} C_1 x^2 + C_2 x + C_3$$

$$EIy = -\frac{1}{6} F_1 \cos \theta < x-L >^3 + \frac{1}{6} C_1 x^3 + \frac{1}{2} C_2 x^2 + C_3 x + C_4$$

$$\frac{1}{EI} \left(\frac{1}{6} L^3 F_1 \cos \theta \right) \leq y_{\max}$$

Boundary Conditions

$$y(0) = 0$$

$$y(2L) = 0$$

$$M(0) = EIy''(0) = 0$$

$$M(2L) = EIy''(2L) = 0$$

전단응력

1번에 작용하는 전단응력

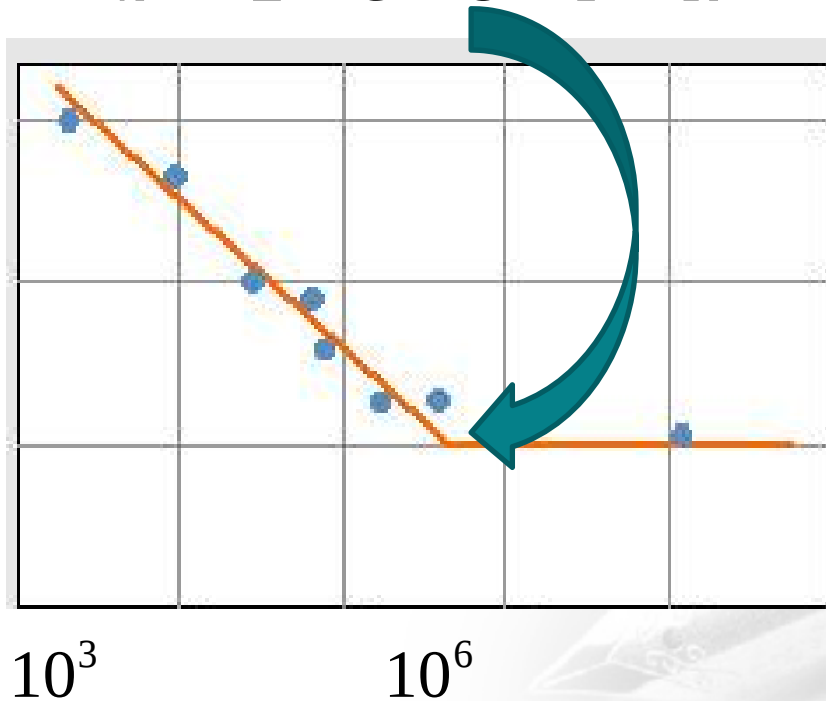
$$\frac{F_1 \cos \theta - \mu \{ (m_1 + m_2)g + F_1 + F_2 \sin \theta \} \sin \theta}{A_1} \leq \tau_a$$

2번에 작용하는 전단응력

$$\frac{F_1 \cos \theta - \mu \{ (m_1 + m_2)g + F_1 + F_2 \sin \theta \} \sin \theta}{A_2} \leq \tau_a$$

$S - N$ Curve

$$S_n = S'_n C_L C_G C_S C_T C_R$$



Steel 물성치

	밀도 (kg / m ³)	σ_a (MPa)	τ_a (MPa)	E(Gpa)
Steel	7860	250	145	200

$$S_n = S_n' C_L C_G C_S C_T C_R$$

$$S_n' = 0.5 S_u \quad (\text{steel})$$

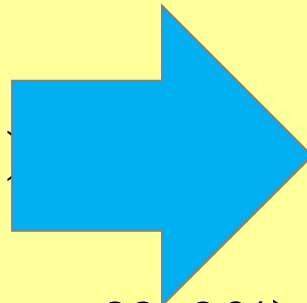
$$C_L = 0.58 \quad (\text{torsion})$$

$$C_G = 0.8 \quad (\text{diameter 관련})$$

$$C_S = 1 \quad (\text{surface factor})$$

$$C_T = 1 \quad (T \leq 840^\circ F)$$

$$C_R = 0.753 \quad (\text{reliability factor } 99.9\%)$$



$$\sigma_a = 75.3 \text{ MPa}$$

$$\tau_a = 25.3309 \text{ MPa}$$

Alloy 2014 – T6 물성치

	밀도 (kg / m ³)	σ_a (MPa)	τ_a (MPa)	E(GPa)
Alloy 2014-T6	2800	400	230	75

$$S_n = S_n' C_L C_G C_S C_T C_R$$

$$S_n' = 0.5 S_u$$

$$C_L = 0.58 \quad (\text{torsion})$$

$$C_G = 0.8 \quad (\text{diameter 관련})$$

$$C_S = 1 \quad (\text{surface factor})$$

$$C_T = 1 \quad (T \leq 840^\circ F)$$

$$C_R = 0.753 \quad (\text{reliability factor } 99.9\%)$$

$$\sigma_a = 120.48 \text{ MPa}$$

$$\tau_a = 40.1801 \text{ MPa}$$

Yellow brass 물성치

	밀도 (kg / m ³)	σ_a (MPa)	τ_a (MPa)	E(GPa)
Yellow brass	8470	410	250	105

$$S_n = S_n' C_L C_G C_S C_T C_R$$

$$S_n' = 0.5 S_u$$

$$C_L = 0.58 \quad (\text{torsion})$$

$$C_G = 0.8 \quad (\text{diameter 관련})$$

$$C_S = 1 \quad (\text{surface factor})$$

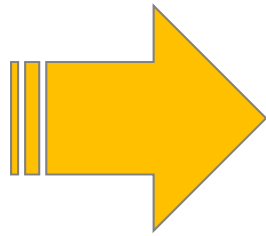
$$C_T = 1 \quad (T \leq 840^\circ F)$$

$$C_R = 0.753 \quad (\text{reliability factor } 99.9\%)$$

$$\sigma_a = 123.492 \text{ MPa}$$

$$\tau_a = 43.674 \text{ MPa}$$

$$m_1 = 2\pi r_1 t_1 L \rho$$



$$m_2 = 2\pi r_2 t_2 L \rho$$

m_1, m_2 가 r, t 와 종속

m_1, m_2 무시

1번

$$\frac{\sqrt{[\mu\{F_1 + F_2 \sin \theta\}]^2 + F_2^2 \sin^2 \theta} + F_1 \sin \theta}{A_1} + \frac{Mc}{I} \leq \sigma_a$$

$$\frac{F_1 \cos \theta - \mu(F_1 + F_2 \sin \theta) \sin \theta}{A_1} \leq \tau_a$$

$$EIy'' = -F_1 \cos \theta \langle x - L \rangle^1 + C_1 x + C_2$$

$$\Rightarrow M = -F_1 \cos \theta \langle x - L \rangle^1 + \frac{F_1 \cos \theta}{2} x$$

$$M(L) = \frac{F_1 \cos \theta}{2} L$$

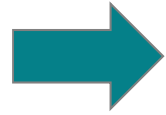
2번

$$\frac{\sqrt{[\mu\{F_1 + F_2 \sin \theta\}]^2 + F_2^2 \sin^2 \theta}}{A_2} + \frac{Mc}{I} \leq \sigma_a$$

$$\frac{F_1 \cos \theta - \mu(F_1 + F_2 \sin \theta) \sin \theta}{A_2} \leq \tau_a$$

Parameters

보통 대의 길이
120~140(cm) 사이



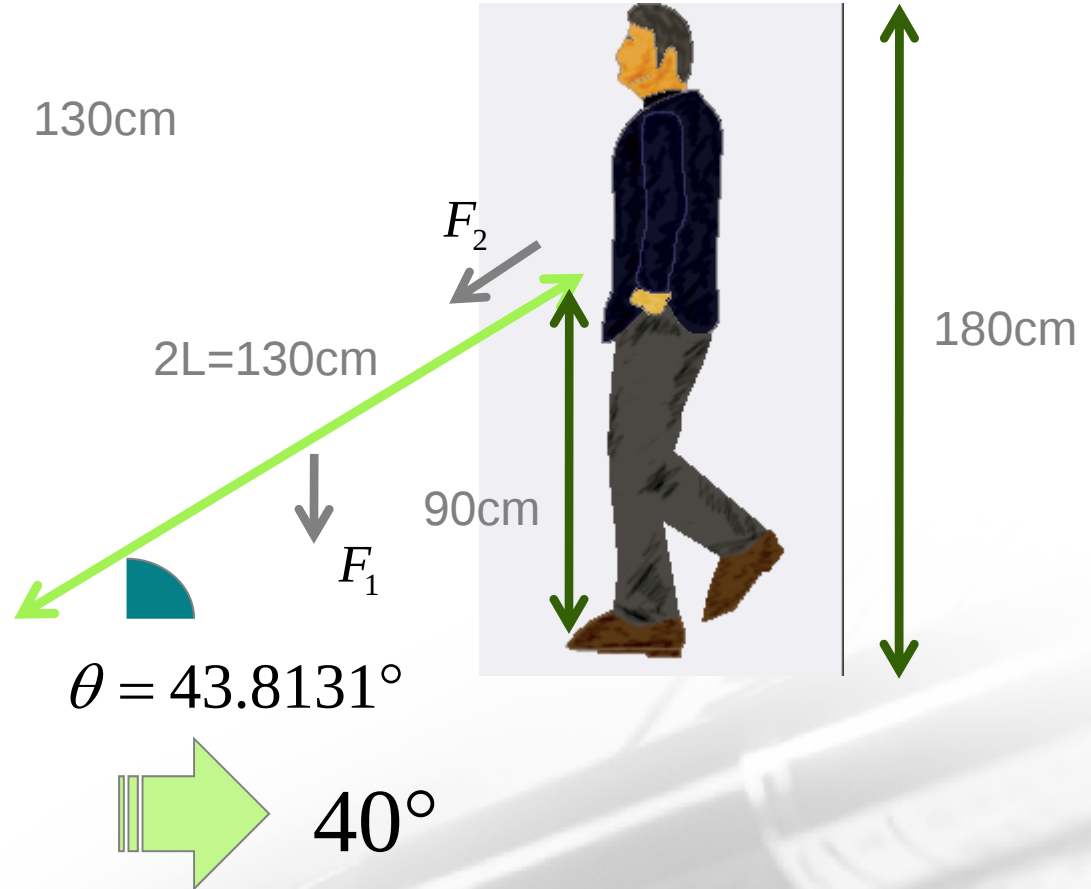
130cm

$$F_1 = 200N$$

$$F_2 = 100N$$

$$g = 9.81m/s^2$$

$$\mu_k = 0.3$$



Design Variables

r_1 t_1

r_2 t_2



r_1 t_1 에 종속적



목적함수

큰 목적함수

$$f = 2\pi(r_1t_1 + r_2t_2)L\rho = m$$

r_1, t_1 구하면 r_2, t_2 알 수 있다.

$\therefore f = 2\pi r_1 t_1 L$ (1번 쪽 이상 대적으므로 더 큰 힘을 받음)

Constraint

$$1: \frac{36.7050}{r_1 t_1} + \frac{63.3983}{r_1^2 t_1} \leq \sigma_a$$

$$2: \frac{16.2730}{r_1 t_1} \leq \tau_a$$

$$3: \frac{16.2445}{r_2 t_2} + \frac{63.3983}{r_2^2 t_2} \leq \sigma_a$$

$$4: \frac{16.2730}{r_2 t_2} \leq \tau_a$$

$$5: \frac{8.0286}{E r_1^3 t_1} \leq y_{\max} (0.001m)$$

$$6: \frac{8.0286}{E r_2^3 t_2} \leq y_{\max}$$

$$7: 0.01 \leq r \leq 0.05(m)$$

$$8: 0.0001 \leq t \leq 0.05(m)$$

Solver(1)

기존 것과 비슷한 결과(여러가지 상황이 다르긴 하지만 나온 결과값은 대충 비슷)

E1	2E+11		시그마	31983294.34	
E2			타우	162309.2692	
E3			y변형량	0.00100098	
	r1	0.02			
	t1	0.005012961			
	f	0.000409258		허용응력(시그마)	75300000
				허용응력(타우)	25330900
				ymax	0.001
0.01	r1	0.02			
0.0001	t1	0.1			

Solver

초기값(1, 1)

E1	2E+11		시그마	75300000	
E2			타우	891336.5806	
E3			y변형량	0.000979409	
	r1	0.047381612			
	t1	0.000385315			
	f	7.45245E-05		허용응력(시그마)	75300000
				허용응력(타우)	25330900
				ymax	0.001
0.01	r1	0.05			
0.0001	t1	0.05			

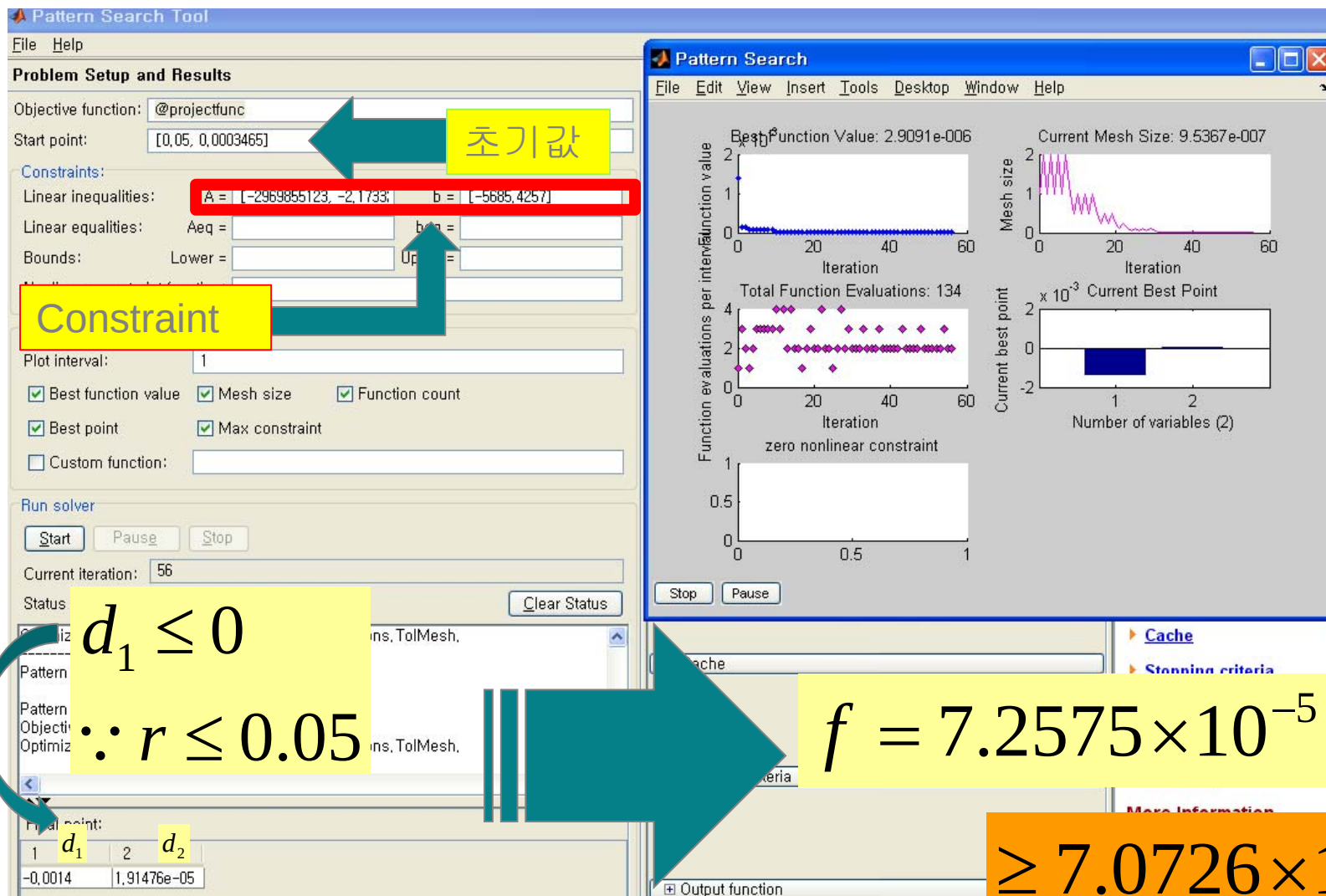
Solver

초기값 (0.1, 0.01), (0.03, 0.07), (0.03, 0.001)

E1	2E+11		시그마	75300000	
E2			타우	939207.5857	
E3			y변형량	0.000926753	
	r1	0.05			
	t1	0.000346526			
	f	7.0726E-05		허용응력(시그마)	75300000
				허용응력(타우)	25330900
				ymax	0.001
0.01	r1	0.05			
0.0001	t1	0.05			

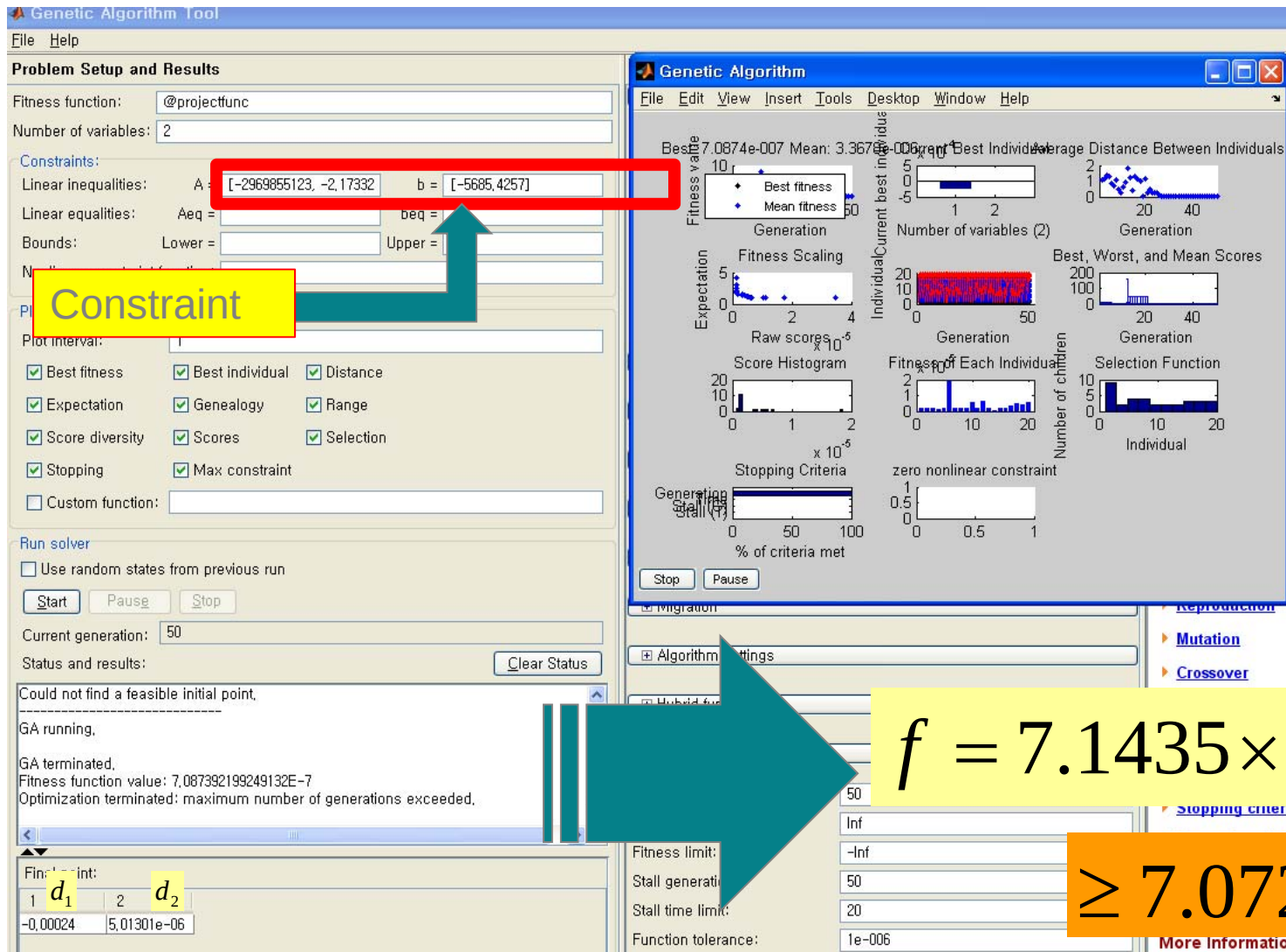
QP

Pattern Search



QP

Genetic Algorithm(너무 불규칙)



Steel

결과값

$$r_1 = 0.05$$

$$t_1 = 0.0003465$$



$$\begin{aligned} m &= 2\pi(r_1 t_1 + r_2 t_2)L\rho \\ &= 1.1103\text{kg} \end{aligned}$$

$$r_2 = 0.0502$$

$$t_2 = 0.0003439$$



Solver(2)

초기값에 관계X

E1	2E+11		시그마	30481095.41	
E2	7.5E+10		타우	380186.9327	
E3	1.05E+11		y변형량	0.001000387	
	r1	0.05			
	t1	0.000856053			
	f	0.00017472		허용응력(시그마)	120480000
				허용응력(타우)	40180000
				ymax	0.001
0.01	r1	0.05			
0.0001	t1	0.05			

Alloy 2014 - T6

결과값

$$r_1 = 0.05$$

$$t_1 = 0.0008566$$



$$\begin{aligned} m &= 2\pi(r_1t_1 + r_2t_2)L\rho \\ &= 0.6107kg \end{aligned}$$

$$r_2 = 0.0504$$

$$t_2 = 0.0002098$$



Solver(3)

초기값(1, 1)

E1	2E+11		시그마	42631752.04	
E2	7.5E+10		타우	531740.5698	
E3	1.05E+11		y변형량	0.000999408	
	r1	0.05			
	t1	0.000612065			
	f	0.000124923		허용응력(시그마)	123492000
				허용응력(타우)	43674000
				ymax	0.001
0.01	r1	0.05			
0.0001	t1	0.05			

Solver(3)

초기값(0.1, 0.001)

E1	2E+11		시그마	42618726.98	
E2	7.5E+10		타우	531578.1098	
E3	1.05E+11		y변형량	0.000999102	
	r1	0.05			
	t1	0.000612252			
	f	0.000124961		허용응력(시그마)	123492000
				허용응력(타우)	43674000
				ymax	0.001
0.01	r1	0.05			
0.0001	t1	0.05			

Solver(3)

초기값(0.03, 0.001)

E1	2E+11		시그마	42667759.75	
E2	7.5E+10		타우	532189.6895	
E3	1.05E+11		y변형량	0.001000252	
	r1	0.05			
	t1	0.000611549			
	f	0.000124817		허용응력(시그마)	123492000
				허용응력(타우)	43674000
				ymax	0.001
0.01	r1	0.05			
0.0001	t1	0.05			

Yellow brass

결과값

$$r_1 = 0.05$$

$$t_1 = 0.0006116$$



$$m = 2\pi(r_1t_1 + r_2t_2)L\rho$$
$$= 1.4149\text{kg}$$

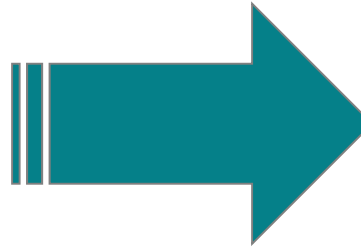
$$r_2 = 0.0504$$

$$t_2 = 0.0002048$$



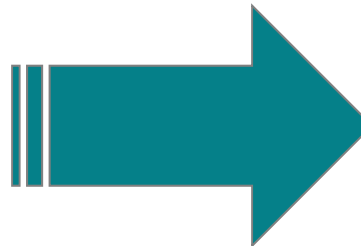
결과값 비교

Steel



1.1103kg

Alloy 2014 – T6



0.6107kg

Yellow brass



1.4149kg

결론

Alloy 2014 – T6

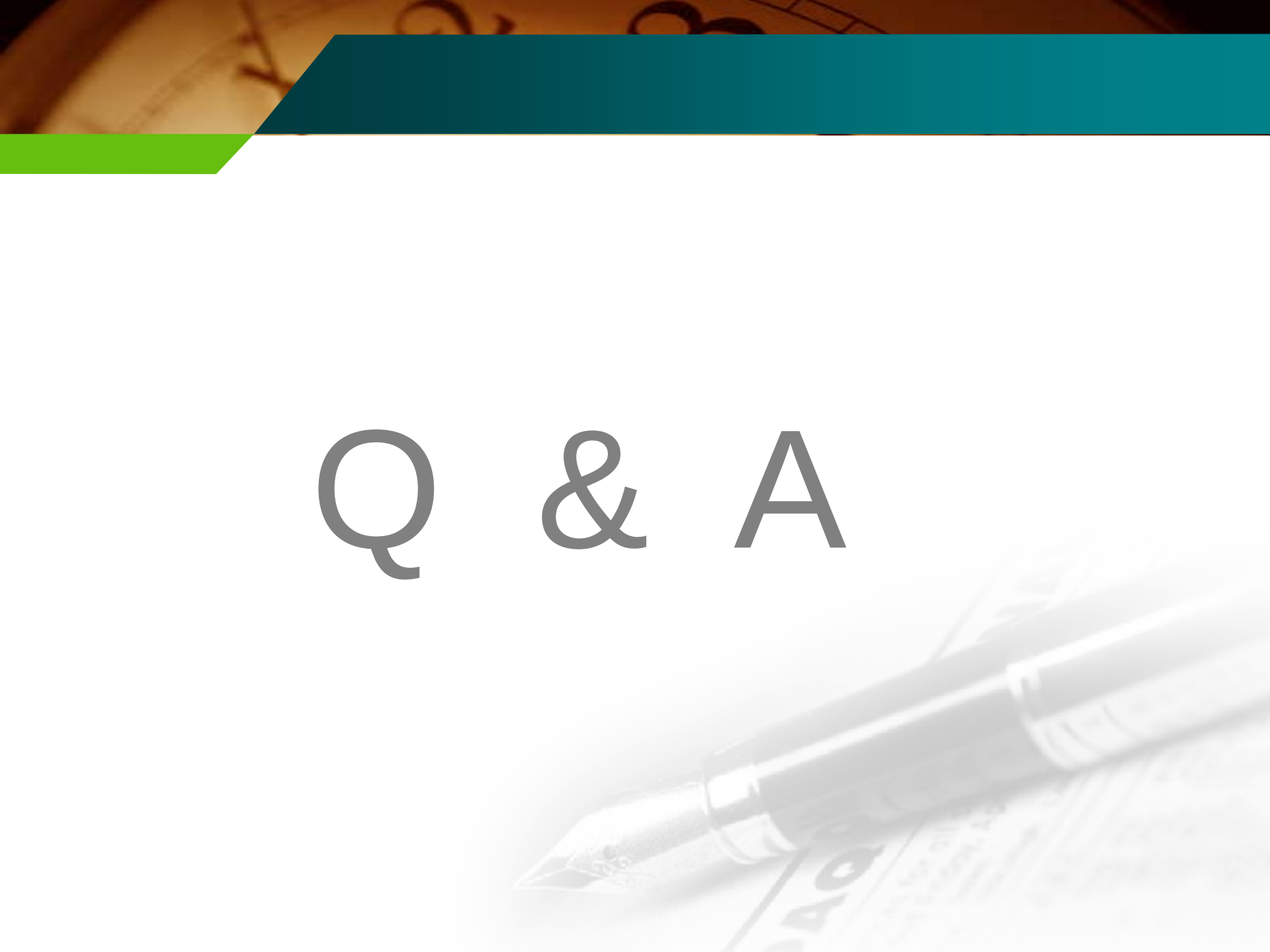
$$r_1 = 0.05m$$

$$t_1 = 0.0008566m$$

$$r_2 = 0.0504m$$

$$t_2 = 0.0002098m$$

0.6107kg



Q & A